IER-499 Final Design of a TEX Variant:

Chlorine to Support NNSA Operations

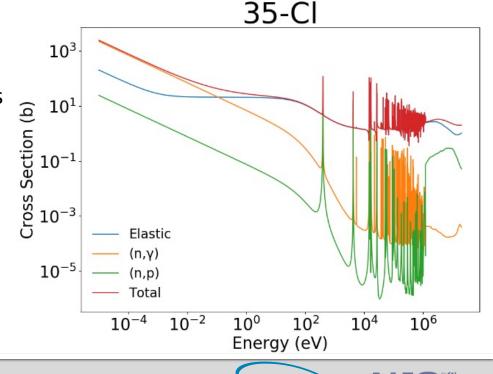
Technical Program Review 2024 February 21,2024 **Eric Aboud**, Ruby Araj, Catherine Percher, Daniel Siefman, Allan Krass, David Heinrichs *Lawrence Livermore National Laboratory*





Need for Chlorine Experiments

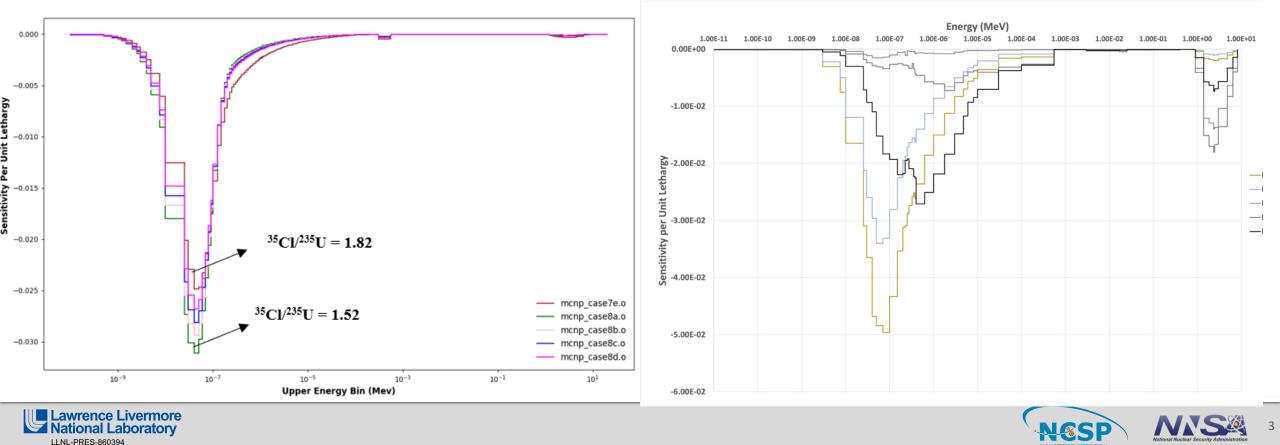
- What are the needs for a chlorine benchmark?
 - Y-12 electrorefining operations which credit ³⁵Cl as a neutron absorber
 - Idaho National Lab / Terrapower for Molten Chlorine Reactor Experiments (MCRE) fuel fabrication
 - Los Alamos National Laboratory for their aqueous plutonium chloride systems
 - ³⁵Cl(n,p) for nuclear data needs
 - The cross section is believed to have a significant uncertainty
 - Interest has been expressed by both domestic and foreign entities
 - IRSN and SRNS has also expressed interest in this benchmark





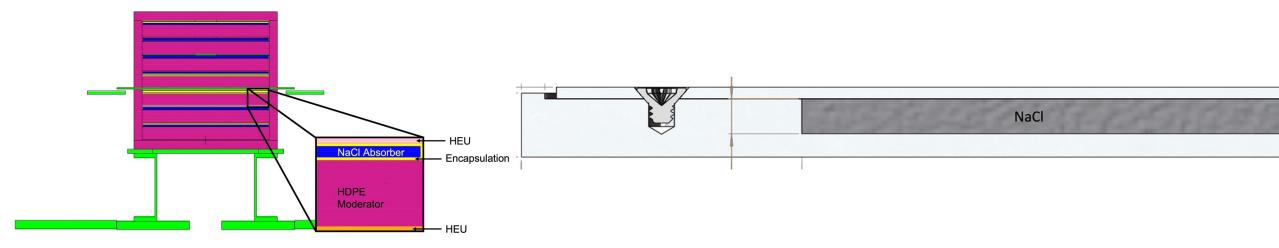
Sensitivity Profiles from Applications

- Sensitivity profiles from Y-12 and INL (MCRE) were used to optimize to and compare
 - Y-12 (left) sensitivity profiles for varying 35Cl/235U ratios (SCALE 238-Group)
 - INL (right) sensitivity profiles for various crit safety upset cases (SCALE 44-Group)



Chlorine Absorber Design

- Many materials and designs were scoped including the use of CPVC and CaCl₂, but ultimately NaCl salts were chosen
- Namely, ≥99.5% pure lab grade sodium chloride salt
- Salt is encapsulated in aluminum and placed like any other solid absorber

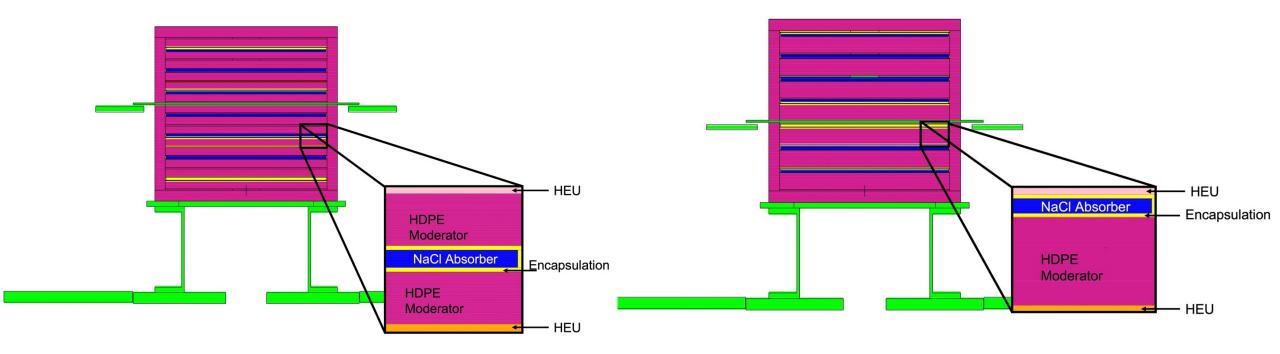






Configurations

• Two types of configurations: Sandwich (left) and Standard (right)

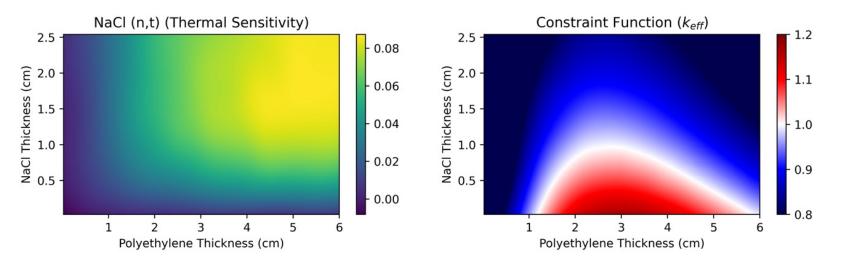






Bayesian Optimization

 Bayesian optimization was used to find critical configurations that matched the sensitivity profiles from Y-12 and INL well



• The G parameter was used as a similarity metric where G=0 is maximally similar

$$G = 1 - \frac{\mathbf{S}_1^T \mathbf{S}_2}{0.5(|\mathbf{S}_1|^2 + |\mathbf{S}_2|^2)}$$





• 3 Standard Configurations:

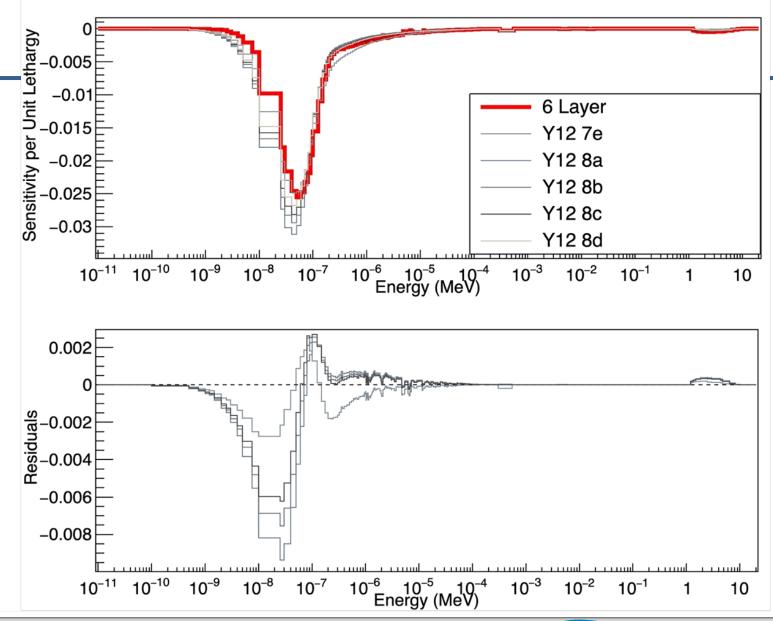
Number of Layers	HDPE Moderator Thickness (in)	NaCl Absorber Thickness (in)	HEU Mass (g)	HDPE Top Reflector Thickness (in)	H/D Ratio
6	27/16	3/16	37,831	1	0.743
8	7/4	1/4	51,222	1	1.0921
18	1/8	3/16	109,331	1	0.7178

Number of Layers	k _{eff}	k _{eff} of Half Stack	Maximum Thermal Capture Sensitivity Amplitude	Minimum G Parameter for Y-12 (case)	Minimum G Parameter for INL	Thermal Fission Fraction (%)	Intermediate Fission Fraction (%)	Fast Fission Fraction (%)
6	1.00025	0.84995	-0.0255	0.009 (7e)	0.211	62.68	25.78	11.55
8	1.00057	0.86737	-0.0327	0.036 (8a)	0.134	62.93	25.50	11.58
18	1.00129	0.73972	-0.0023	0.754 (7e)	0.722	13.66	51.78	34.56

Lawrence Livermore National Laboratory LLNL-PRES-860394



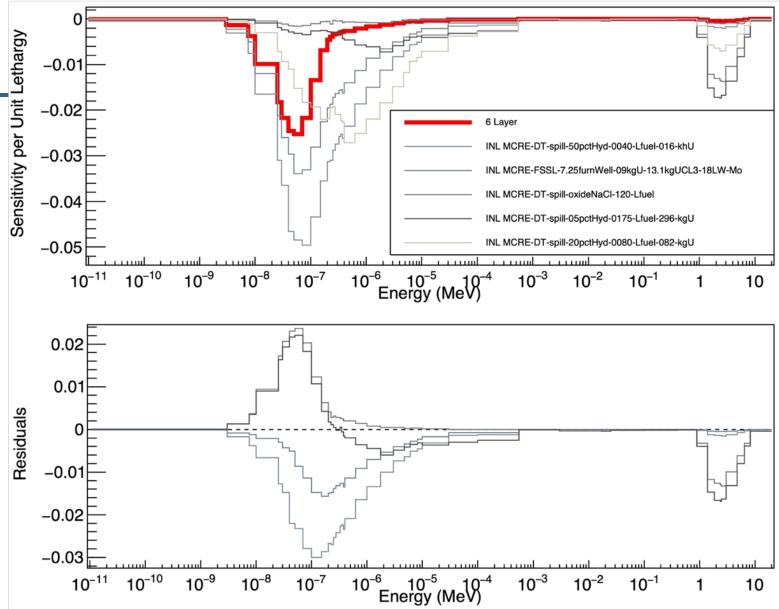
- Compared to Y-12:
- Top is a direct comparison to the sensitivity profiles
- Bottom are 'residuals' that show the difference between the sensitivity profile of the critical configuration and the application case sensitivity profiles



185

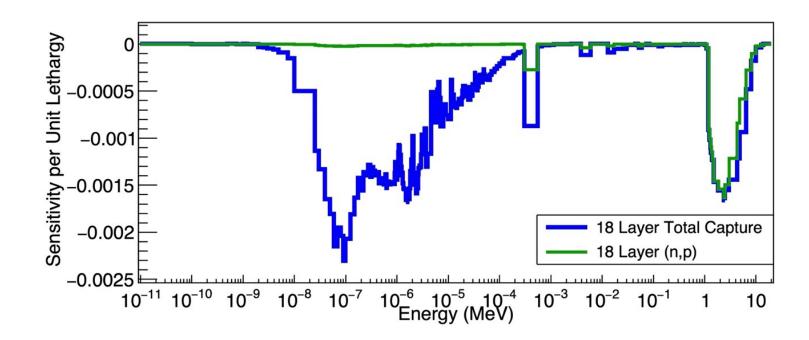


- Compared to INL (MCRE):
- Top is a direct comparison to the sensitivity profiles
- Bottom are 'residuals' that show the difference between the sensitivity profile of the critical configuration and the upset case sensitivity profiles





 How much of the total capture sensitivity profile for the fastest configuration comes from (n,p)?







2 Sandwich Configurations:

•	Number of Layers	HDPE Moderator Thickness (in)	NaCl Absorber Thickness (in)	HEU Mass (g)	HDPE Top Reflector Thickness (in)	H/D Ratio
	6	11/16	3/16	38,594	17/16	0.6388
	8	3/4	1/4	49,552	1	0.9754

Number of Layers	k _{eff}	k _{eff} of Half Stack	Maximum Thermal Capture Sensitivity Amplitude	Minimum G Parameter for Y-12 (case)	Minimum G Parameter for INL	Thermal Fission Fraction (%)	Intermediate Fission Fraction (%)	Fast Fission Fraction (%)
6	1.00094	0.81436	-0.0236	0.009 (7e)	0.206	56.74	31.22	12.04
8	1.00011	0.86381	-0.0246	0.013 (7e)	0.180	58.05	30.19	11.76



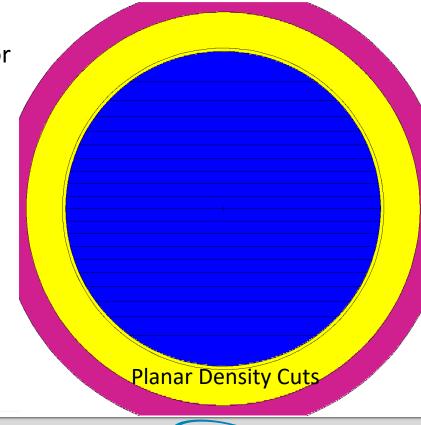


Density Studies

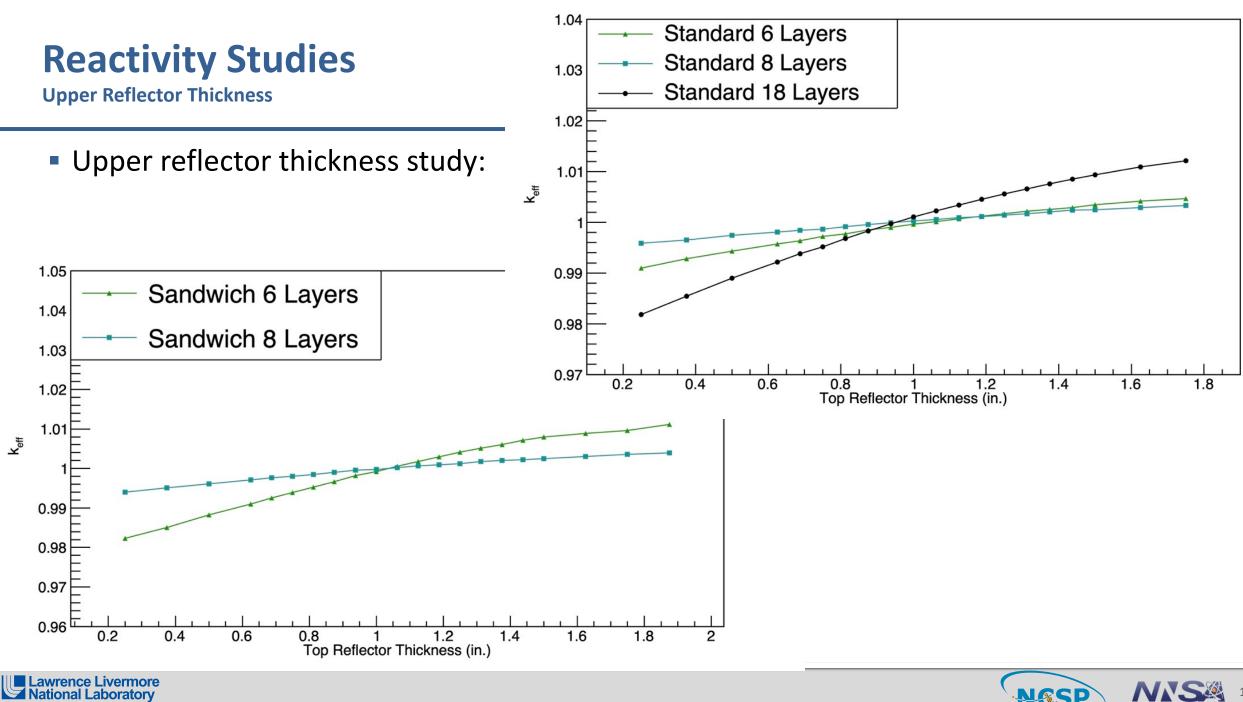
- Design relies on pouring salt into an encapsulation, so we need to know how density variations affect the reactivity of the system
- Total density and planar density were studied:
 - Planar density studies show no large change to multiplication factor

—	Total:	
_	iotal:	

	Standard				
Densities (g/cc)	6 Layer				
(g/cc)	keff	dkeff			
1.217	1.01044	0.00156			
1.25	1.00888	0.00239			
1.3	1.00649	0.00242			
1.35	1.00407	0.00100			
1.375	1.00307	0.00118			
1.4	1.00189	0.00119			
1.425	1.00070	0.00056			
1.4375	1.00014	0.00049			
1.45	0.99965	0.00070			
1.4625	0.99895	0.00045			
1.475	0.99850	0.00116			
1.5	0.99734	0.00439			
1.6	0.99295	0.00635			
1.75	0.98660	0.01038			
2	0.97622	0.00634			
2.16	0.96988	-			







LLNL-PRES-860394



Reactivity Studies

HEU Plate Swaps

Reactivity as a 6 Layer Standard function of mass via 1.005 HEU plate swaps 0.995 Standard 0.99 configurations ۔ ™0.985 ک Similar performed for 0.98 sandwich 0.975 configurations 0.97 0.965 34 37 35 38 39 33 36 Mass (kg)

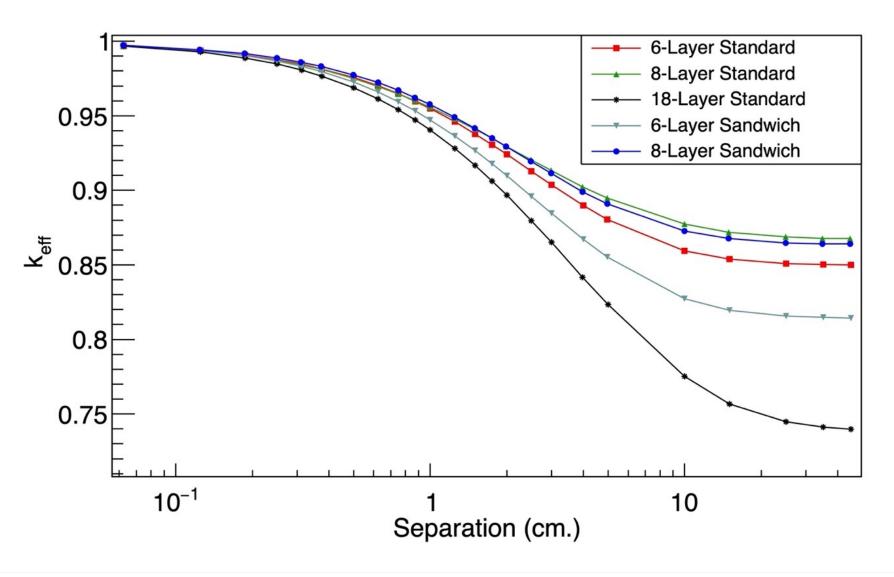




Reactivity Studies

Separation

 Reactivity as a function of separation:







Conclusions

- Final design of TEX with chlorine absorbers was complete
 - 5 configurations were identified, expected to down select to three experimental configurations
 - Great comparison to Y-12 and good comparison to INL sensitivities
 - Fastest configuration touches on the ³⁵Cl(n,p) cross section (continuing to work with Terrapower for faster configurations)
 - Extensive density studies performed to ensure understanding of the salt in the plates
 - Reactivity studies performed to assist with experiment
- Fabrication of the chlorine absorbers is ongoing (with LANL)
- Experiment scheduled to be completed this year





Disclaimer

This document was prepared as an account of work sponsored by an agency of the United States government. Neither the United States government nor Lawrence Livermore National Security, LLC, nor any of their employees makes any warranty, expressed or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States government or Lawrence Livermore National Security, LLC. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States government or Lawrence Livermore National Security, LLC, and shall not be used for advertising or product endorsement purposes.

This work was performed under the auspices of the U.S. Department of Energy by Lawrence Livermore National Laboratory under contract DE-AC52-07NA27344. Lawrence Livermore National Security, LLC

Lawrence Livermore National Laboratory