

# IER-479/547: Low-Temperature TEX

Surrogate Testing and Reflector Design

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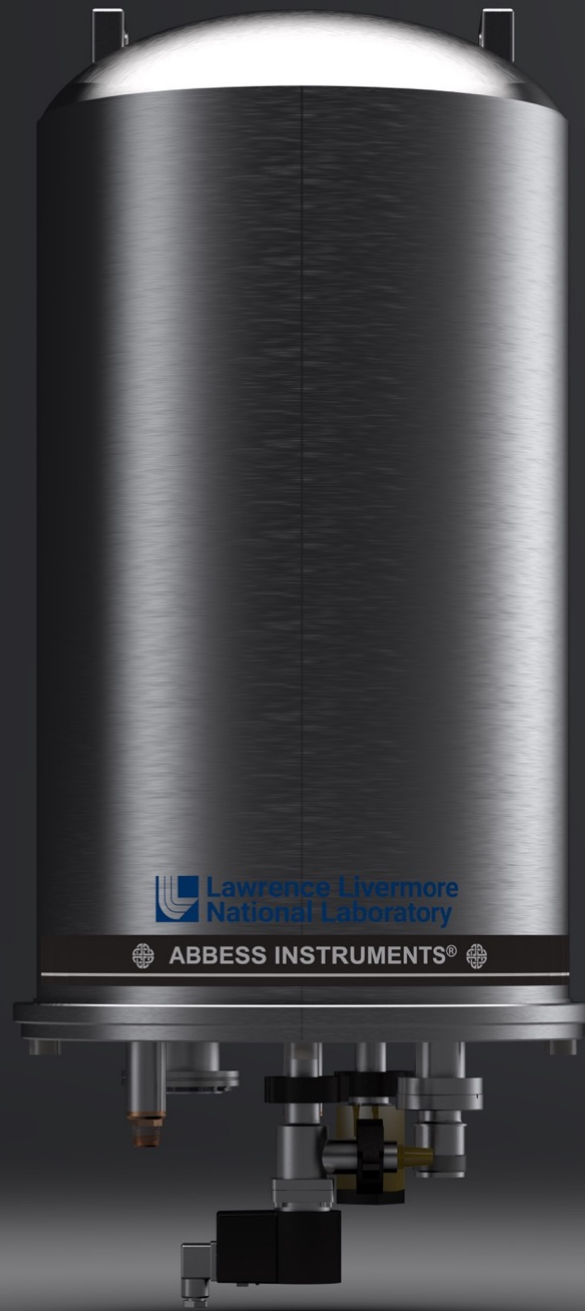
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# Low-Temperature TEX



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# Experimental Configurations

- What goes inside of the chamber?
- 6 proposed configurations spanning from predominantly thermal to fast neutron fission energies
  - 5 require the spindle heatsink
  - 1 requires the non-spindle heatsink

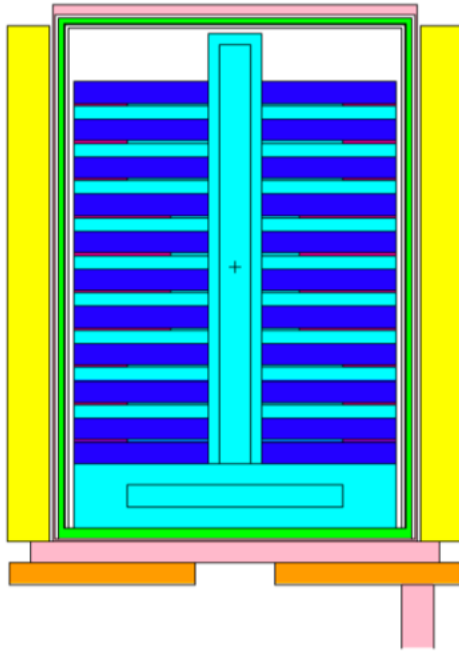
Case	Number HEU Plates	HEU Mass (g)	Moderator Thickness (in)	Spacer Thickness (in)	Annular Reflector Thickness (in)	Cold Critical Temp. (°C)	Multiplication Factor ( $k_{eff}$ )			Fission Fractions		
							Reflected, Cold	Reflected, 20°C <sup>(a)</sup>	Handstack, 20°C <sup>(b)</sup>	Thermal (<0.625 eV)	Intermediate	Fast (>100 keV)
1	26	134,488	-	1/4	2.25	-40	1.00409	1.00360	0.88858	15%	21%	64%
2	19	93,074	1/8	3/8			1.00284	1.00313	0.87854	21%	48%	31%
3	14	68,650	1/4	1/2			1.00236	1.00329	0.88467	30%	48%	22%
4	12	50,610	1/2	1/2			1.00057	1.00629	0.88856	47%	38%	15%
5a	10	43,421	1	5/8	2.00	-30 <sup>(c)</sup>	1.00292	1.01752	0.92108	60%	28%	12%
5b		45,290		7/8	2.50		1.00156	1.01265	0.89957			

(a) Represents the critical configuration reflected at 20°C using the same annular reflector, corresponding to the 80¢ excess reactivity requirement.

(b) Represents the critical configuration unreflected at 20°C using the model described in Section 3.5, corresponding to the handstack limit requirement.

(c) Case 5 is subcritical at less than -30°C, creating a more reactive configuration by increasing the HEU mass would violate the handstack limit.

# Experimental Configurations



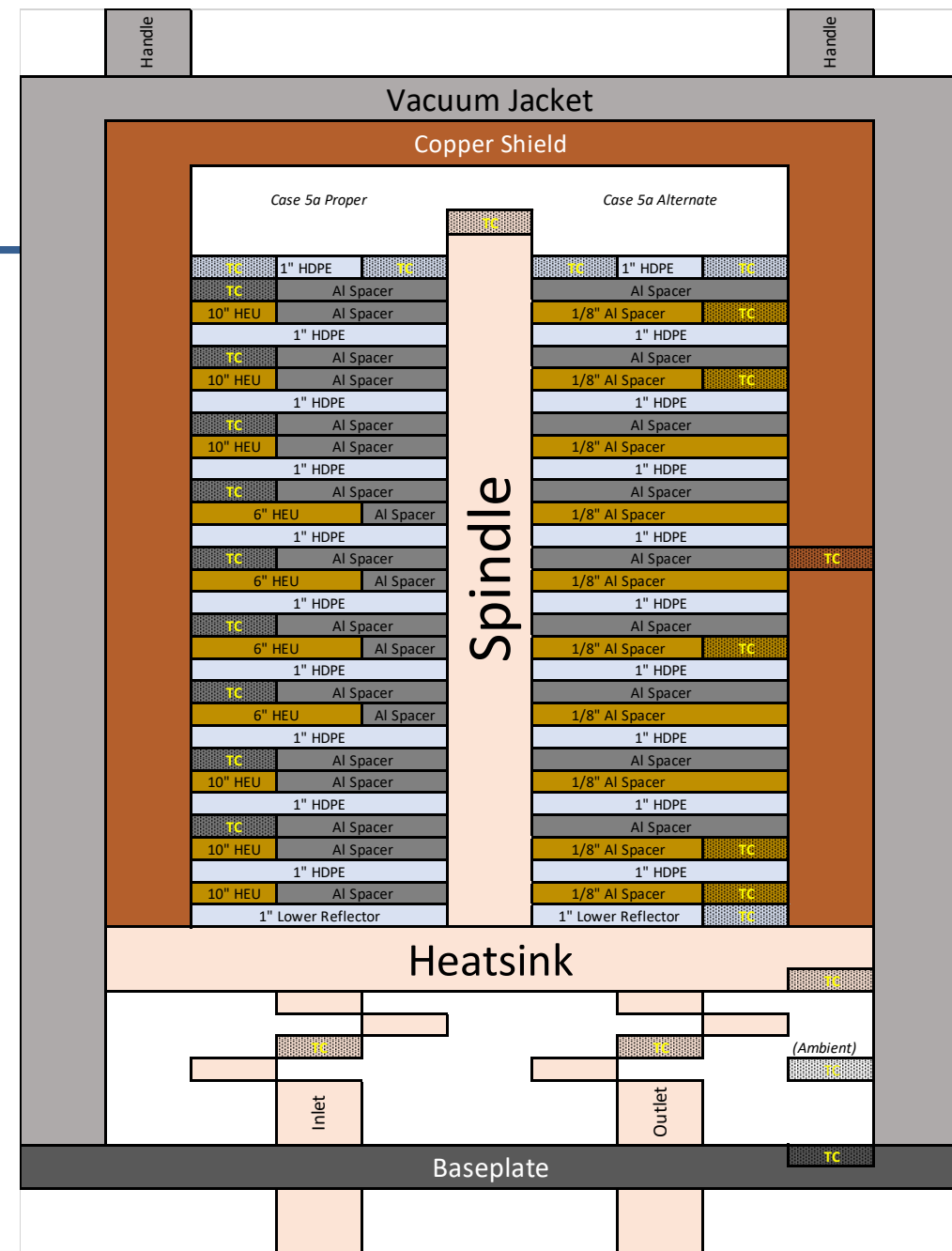
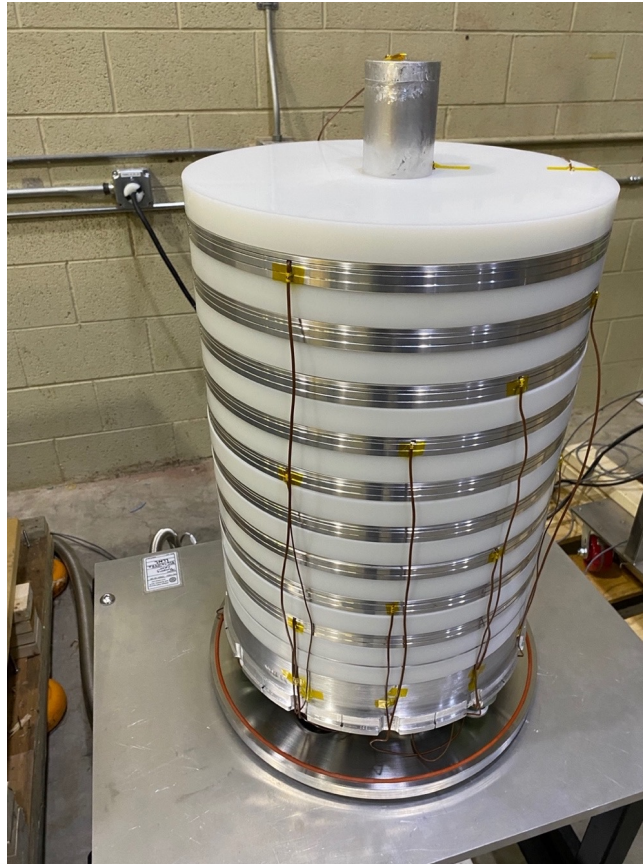
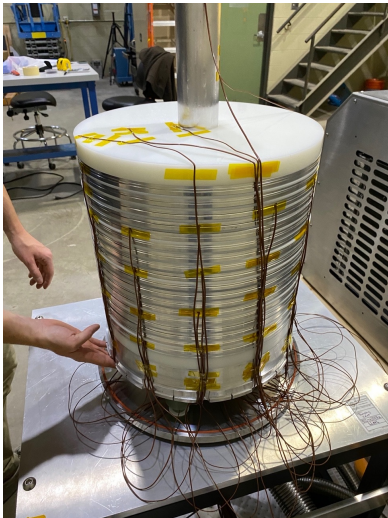
## ■ Case 5a

- 10 Fuel Plates
  - 6x 10" HEU
  - 4x 6" HEU
- 5/8" Aluminum Spacers
- 1" Poly Moderators
- 1" Poly Top and Bottom Reflectors

Case	Number HEU Plates	HEU Mass (g)	Moderator Thickness (in)	Spacer Thickness (in)	Annular Reflector Thickness (in)	Cold Critical Temp. (°C)	Multiplication Factor ( $k_{eff}$ )			Fission Fractions		
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# Thermal Performance Measurements

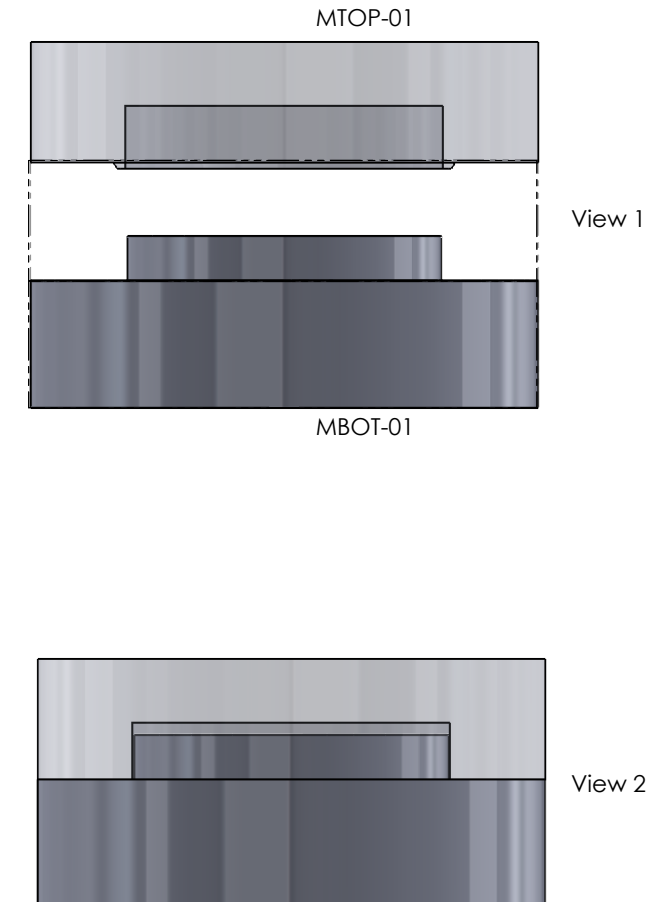
- In order to read the temperatures in the chamber we have 38 thermocouples
- Diagnostic TC's are placed strategically to monitor the temp of the system



# Thermal Considerations

## Case 5 – Aluminum Wire

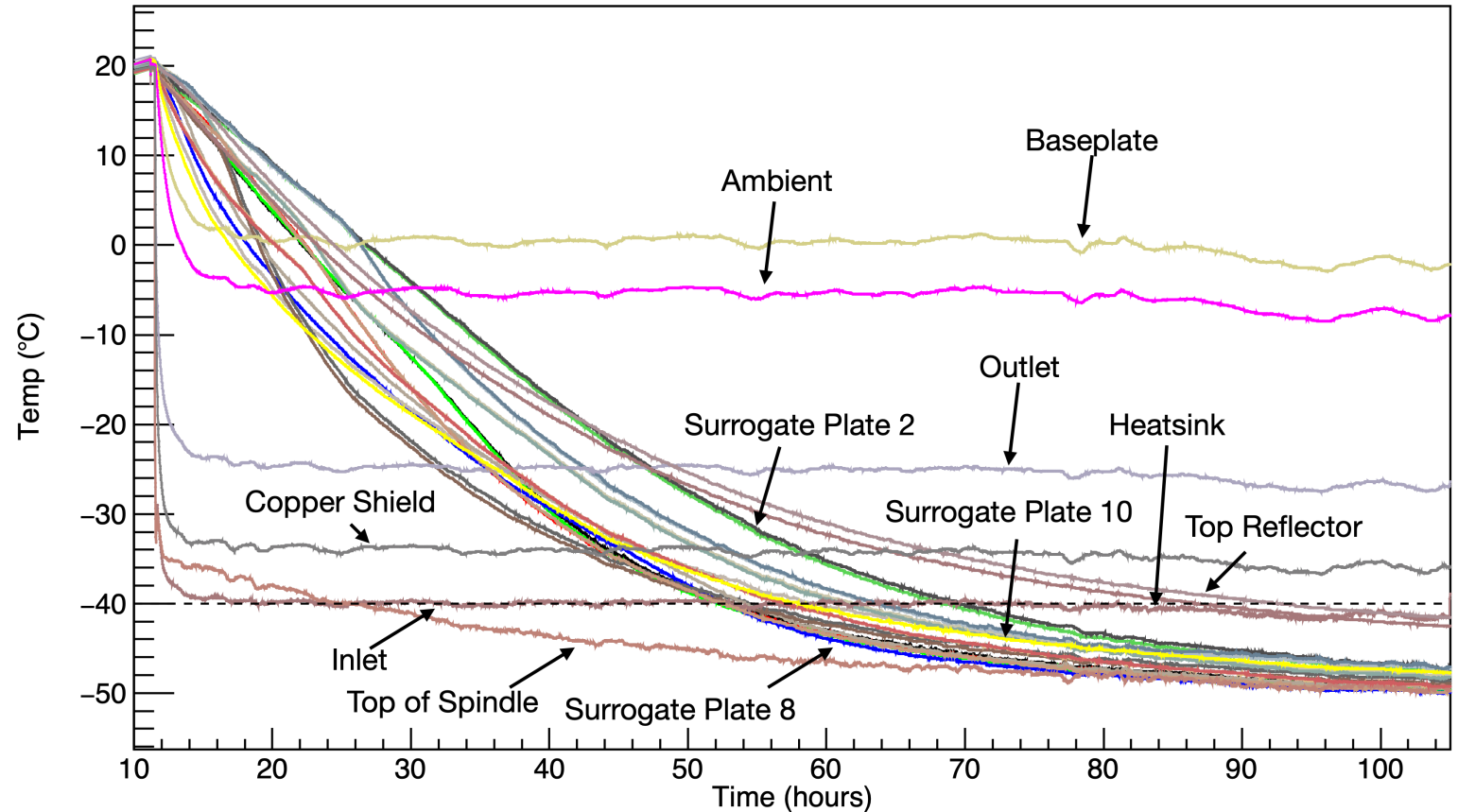
- To improve the thermal contact between the stack and the spindle, aluminum wire was pressed into the gaps
- Since testing, the spacer plates have been redesigned to allow for an aluminum gasket to fit into the gap



# Thermal Performance

## Case 5 – Aluminum Wire

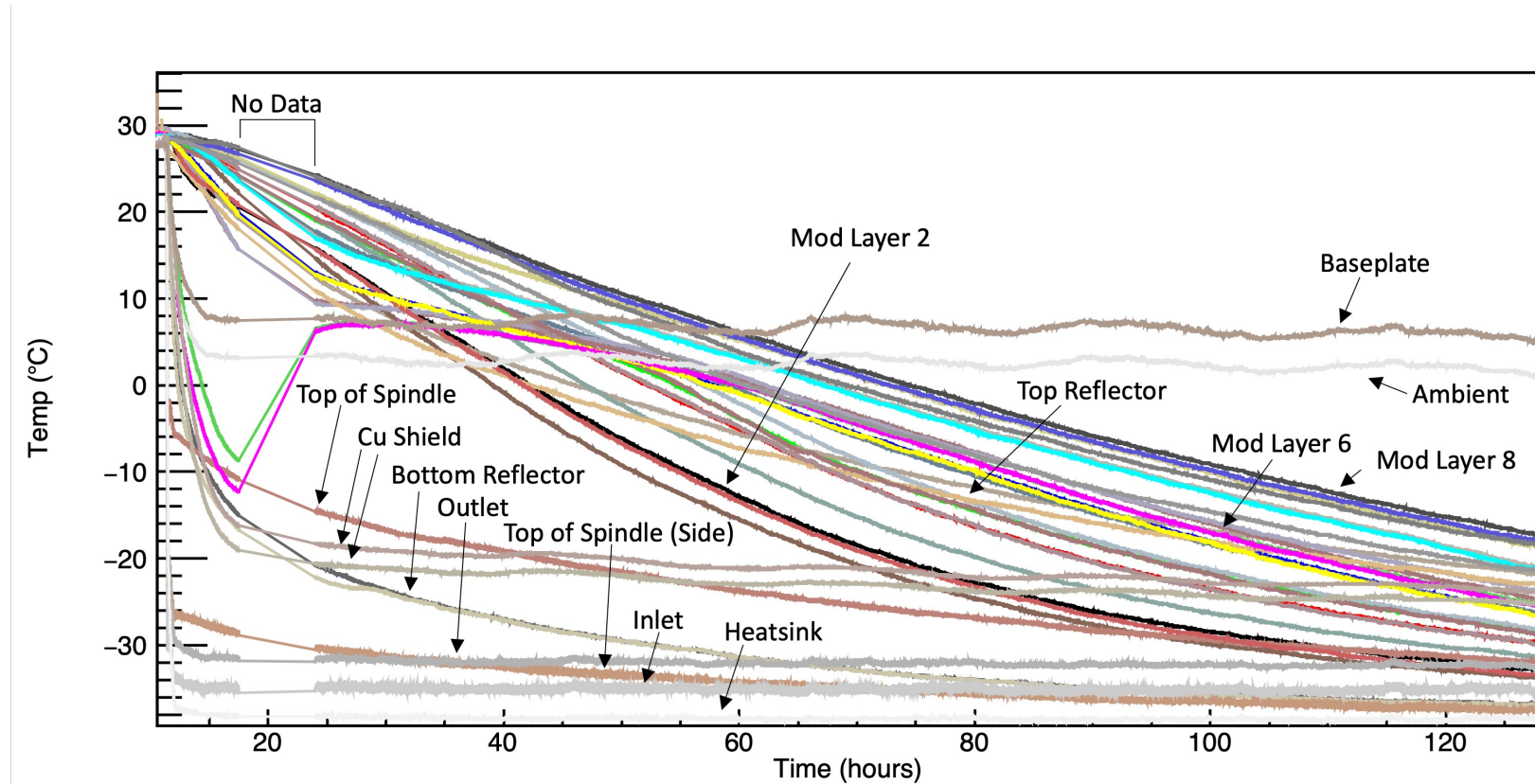
- Cooling to  $40^{\circ}\text{C} \pm 2.5^{\circ}\text{C}$  within 49 hours
- Cooling overshoot (issue with chiller has been fixed)



# Thermal Performance

## Case 5 – Copper Wire

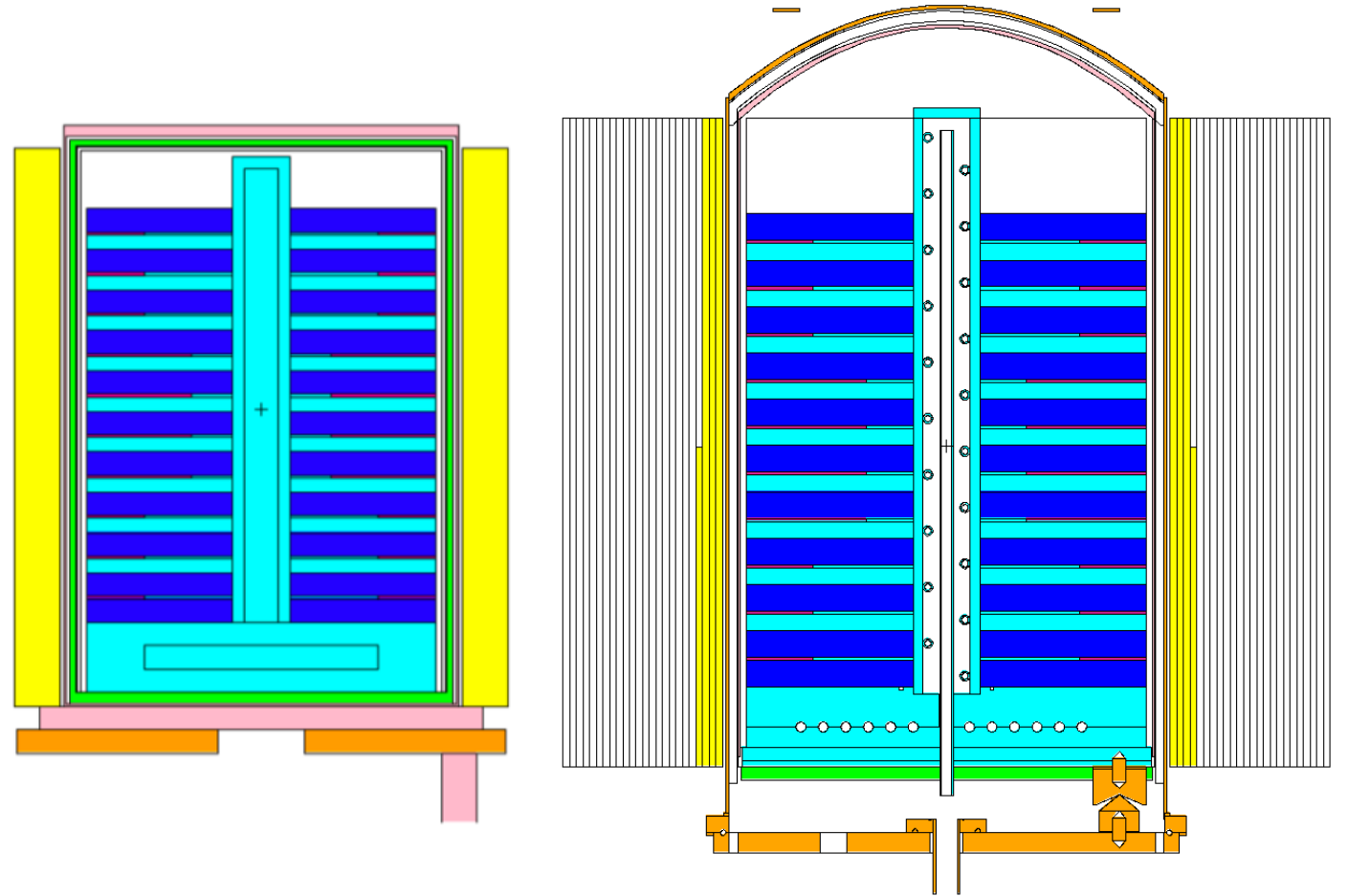
- Similarly, copper wire was tested
- Cooling to  $40^{\circ}\text{C} \pm 2.5^{\circ}\text{C}$  in more than 100 hours
- Aluminum/Copper interfaces form intermetallic compounds that deteriorate conductivity [1]



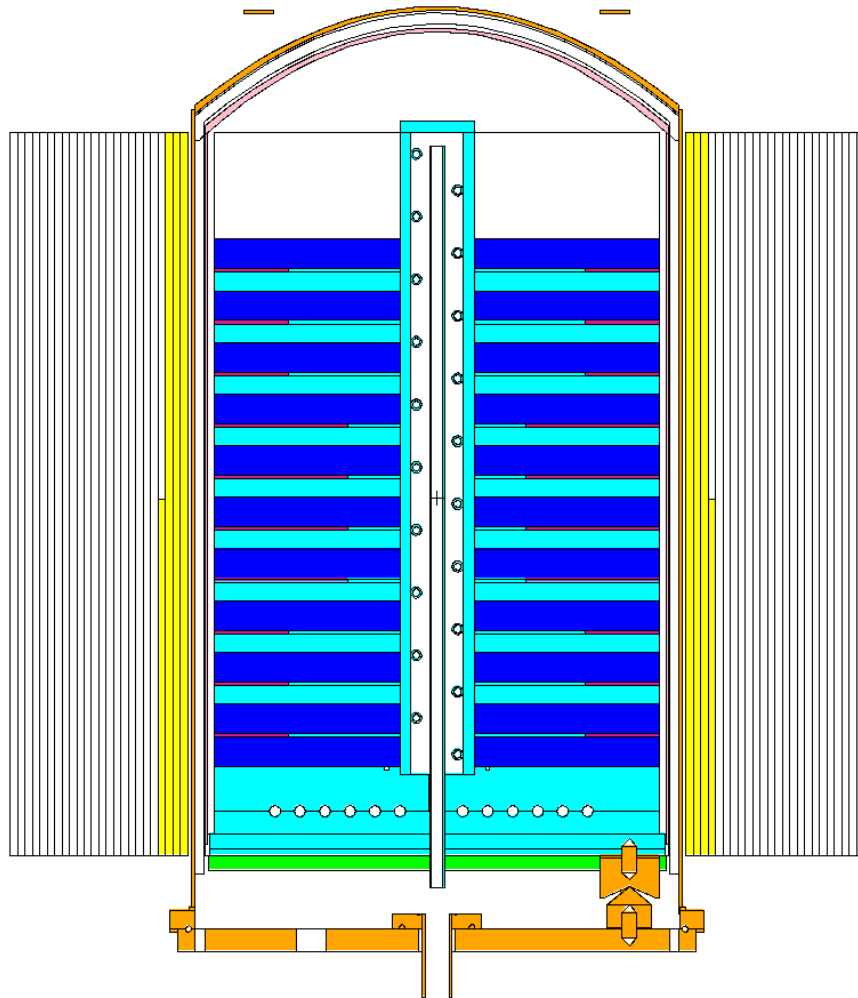


# Reflector Design: The Approach

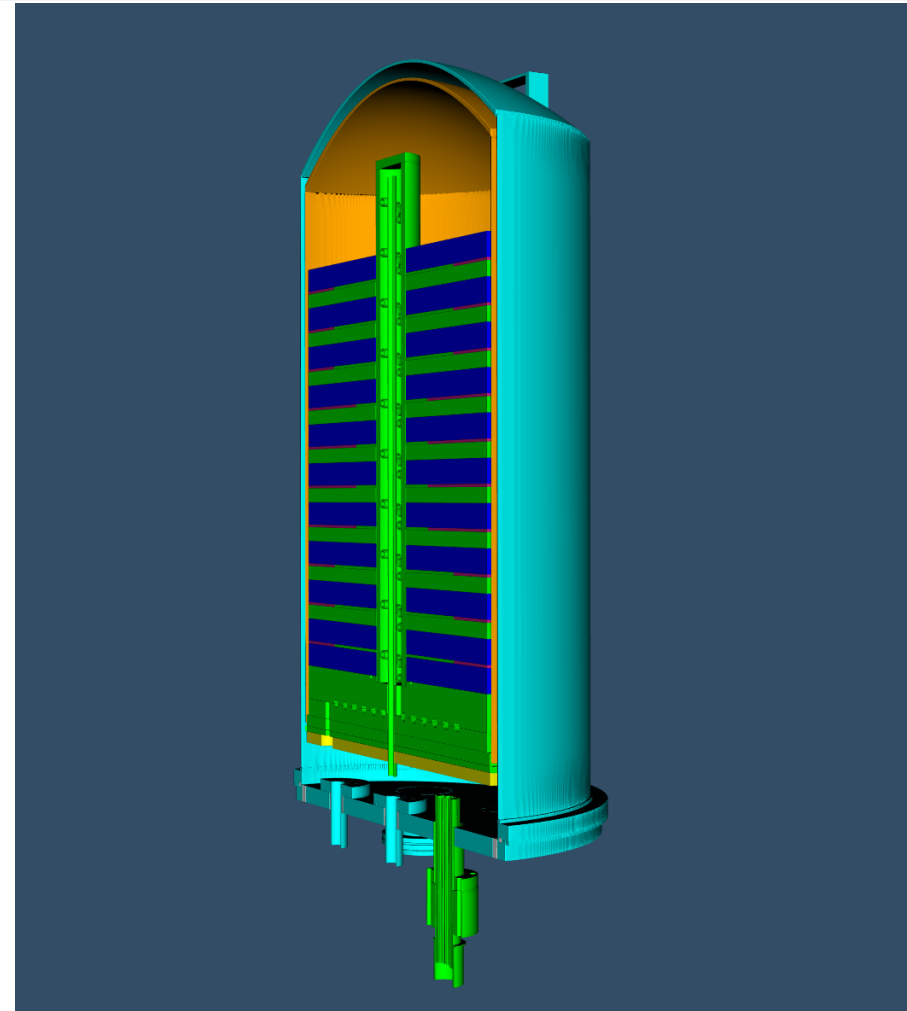
- High fidelity model
- Incrementally map  $k_{\text{eff}}$  to show reactivity worth for each segment of reflector added (both axially and annularly).



# Detailed Assembly Model



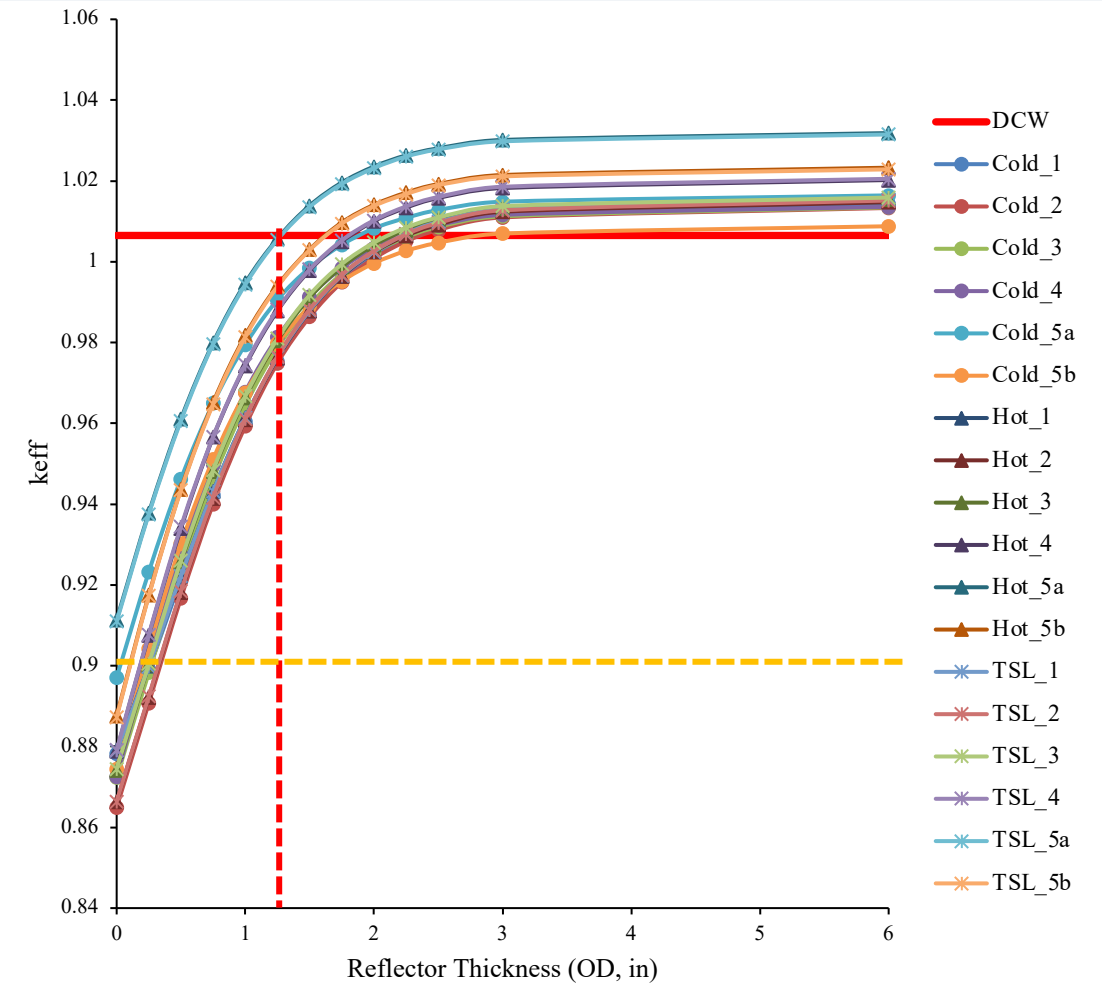
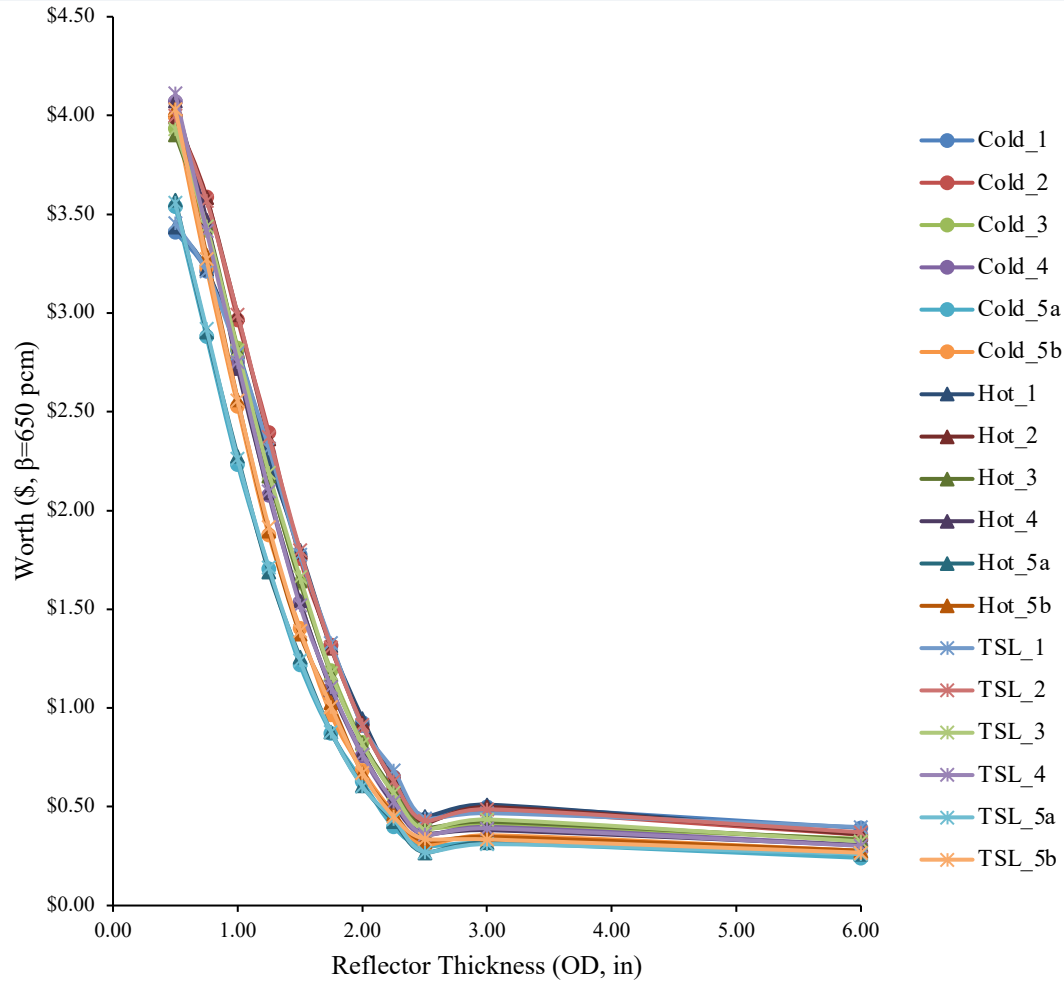
*MCNP Interactive Plotter (YZ)*



*GXView*



# Reflector Calculation Design



# Conclusions

- Progress in surrogate testing
  - A new chiller has been fabricated and testing has resumed
  - Additional tests are being conducted, including:
    - Using formed aluminum gaskets
    - Extended testing with natural uranium
    - Testing with pseudo-spindle
    - Testing with no vacuum
- Reflector Design
  - Results for detailed model are consistent with results presented in CED-2.
  - Calculations provide flexibility in the physical design of the reflectors (e.g. reflector segment widths and heights).
  - Provided initial CAD models of reflector components.



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