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Sum-of-Fractions Method

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U.S. DEPARTMENT OF
ENERGY **BATTELLE**

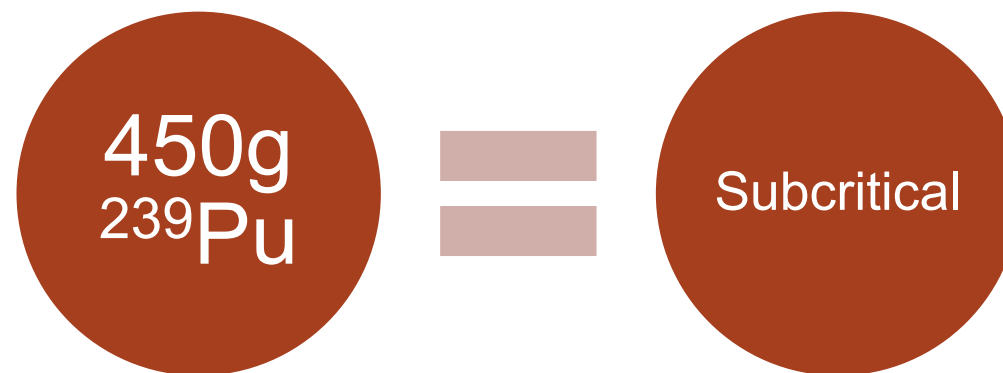
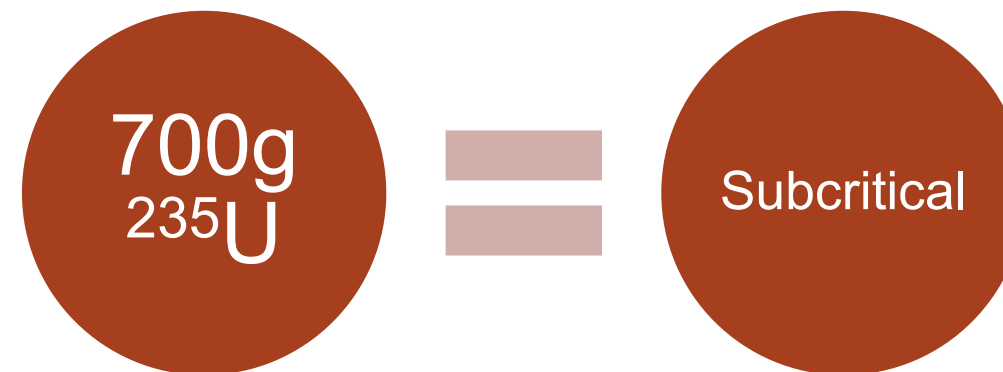
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Purpose

- Addressing the presence of multiple fissionable nuclides in a moderated system
- Validation with benchmarking gaps
 - Calculational margin
 - Margin of subcriticality



Background

- ANSI/ANS-8.15-1981
 - “... the sum of ratios of the mass of each fissile nuclide to its limit does not exceed unity...”
 - Only for water moderated and reflected systems
- Three methods of note were derived from the ANSI/ANS-8.15-1981
 - Rule-of-Fractions
 - ✓ Direct application of ANSI/ANS-8.15-1981
 - Fissile Gram Equivalent
 - ✓ Rule-of-Fractions restricted to a specific moderated and reflected system
 - Sum-of-Fractions (SoF)
 - ✓ Generalization of the Rule-of-Fractions that extends use beyond water moderated and reflected systems

Background (cont.)

- Revision of ANSI/ANS-8.15-2014 removed Rule-of-Fractions
- ANSI/ANS-8.15-2014
 - If mixture is of “...different isotopes of the same material... the subcritical limit for the limiting nuclide should be used...”
 - Or “... the user may calculate their own subcritical limits for mixtures of material ...”
- Work presented here provides a method for calculating subcritical limits using Sum-of-Fractions

Sum-of-Fractions (SoF)

- For a mixture of nuclides i with masses a_i and minimum subcritical mass A_i subcriticality is defined as:

$$\sum_i \frac{a_i}{A_i} \leq 1$$

- The minimum subcritical masses for all the nuclides is based on a system that is more reactive than the specific system evaluated

Method

- Establish a set of mixtures with ^{233}U , ^{235}U , and ^{239}Pu to determine bias, uncertainty in bias (calculational margin), and validation applicability
- Sensitivity analyses performed to determine bias and bias uncertainty
- Validation applicability determined from the upper and lower energy corresponding to the average lethargy causing fission (EALF)

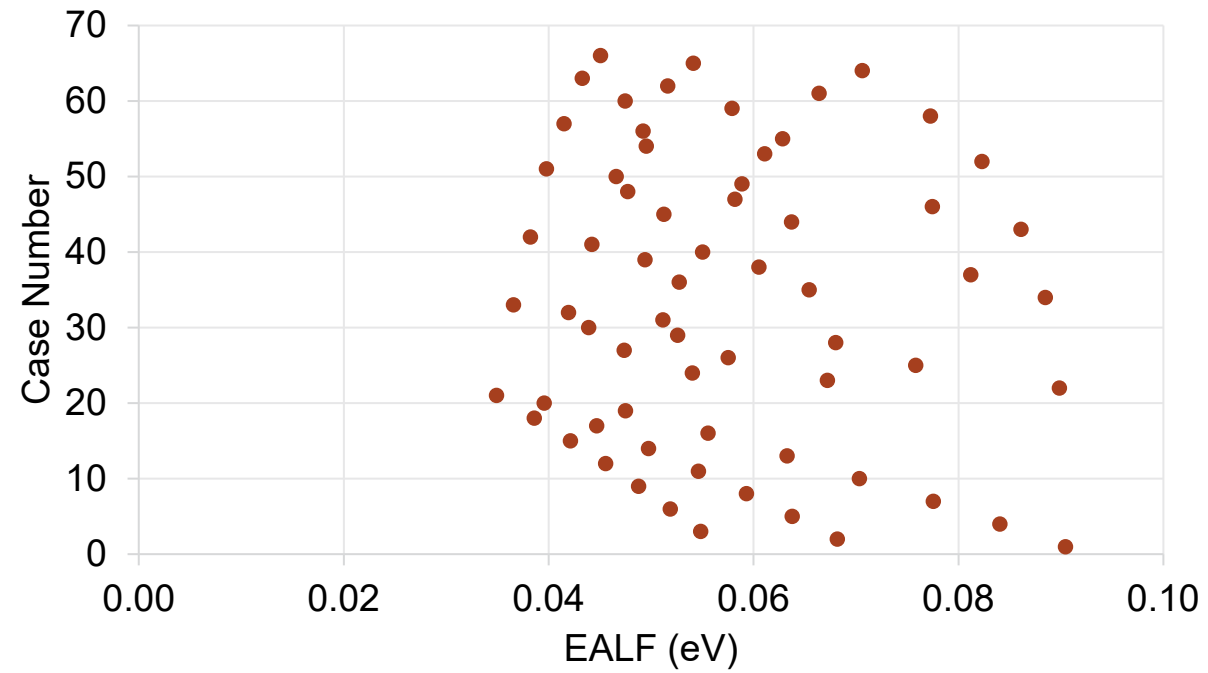
Method (cont.)

- Compute minimum subcritical masses for optimally moderated and fully reflected systems
 - Limited benchmarks to determine bias and bias uncertainty of actinides present in 8.15
 - Use of the ^{233}U , ^{235}U , and ^{239}Pu to establish
- Mixtures containing 5/6 subcritical mass of ^{233}U , ^{235}U , or ^{239}Pu and 1/6 of an 8.15 actinide
- Margin of subcriticality applied to nuclide masses
- Calculations using SCALE 6.2.4

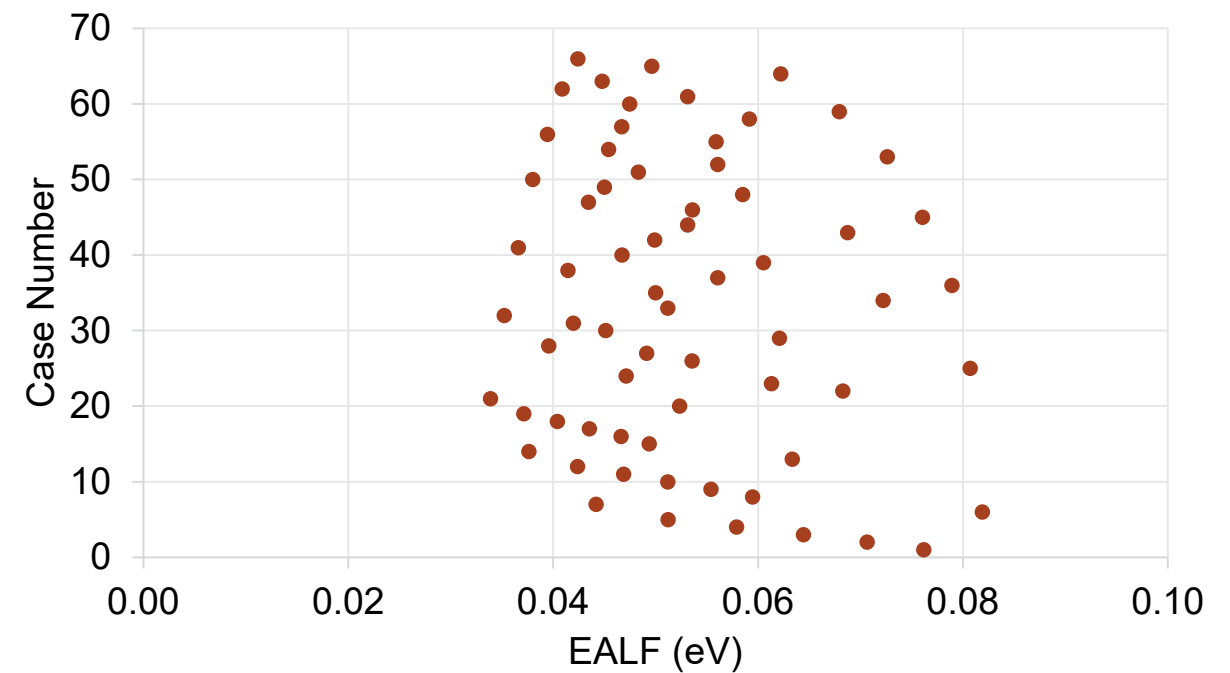
^{233}U , ^{235}U , and ^{239}Pu validation mixtures

- Mixtures used in validation selected to cover moderated systems
- Approximately 30g/L, 50g/L, and 80g/L systems
- All combinations of compositions of 0, 1/6, 1/3, 1/2, 2/3, 5/6, and 1 volume fractions were computed
- EALF range for water system (0.035 - 0.09 eV)
- EALF range for polyethylene system (0.034 - 0.082 eV)

EALF Values for Validation Cases

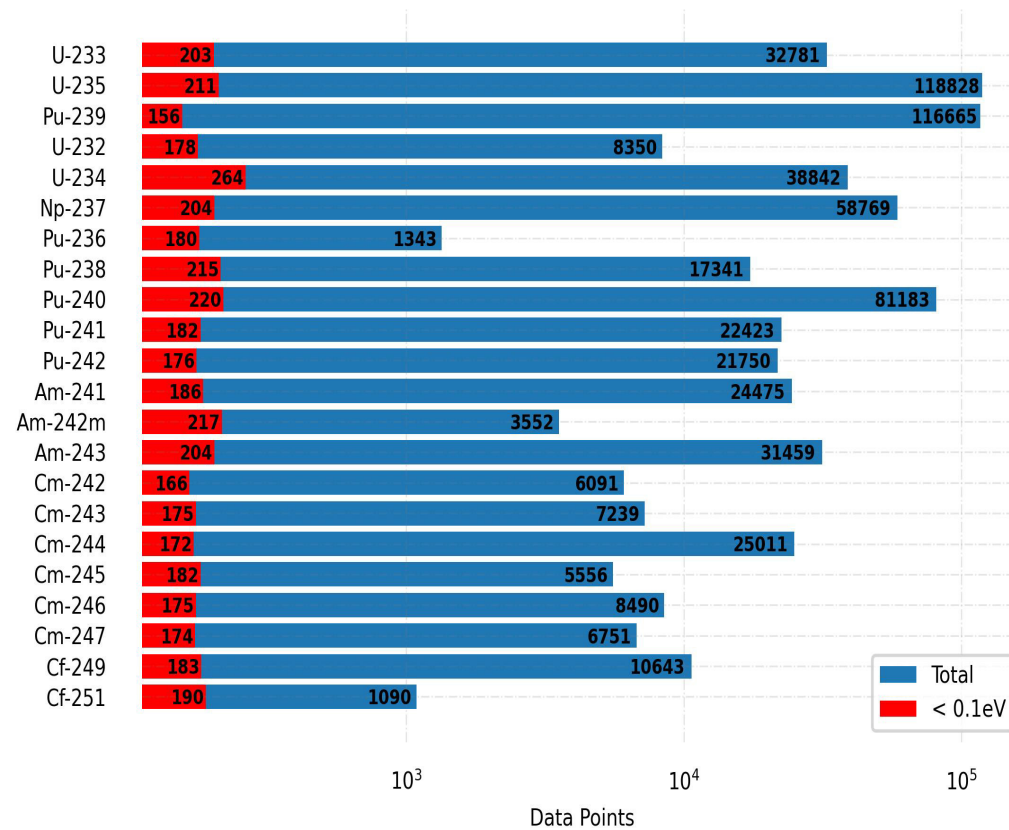


Water Moderated and Reflected

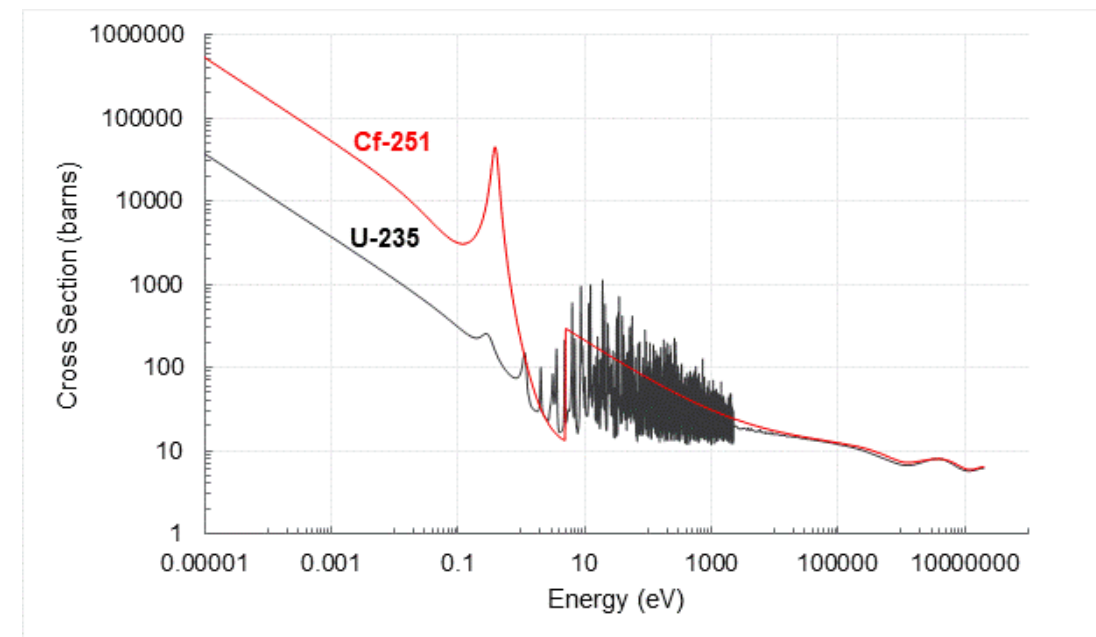


Polyethylene Moderated and Reflected

Available Cross Section Data ENDF/B VII.1

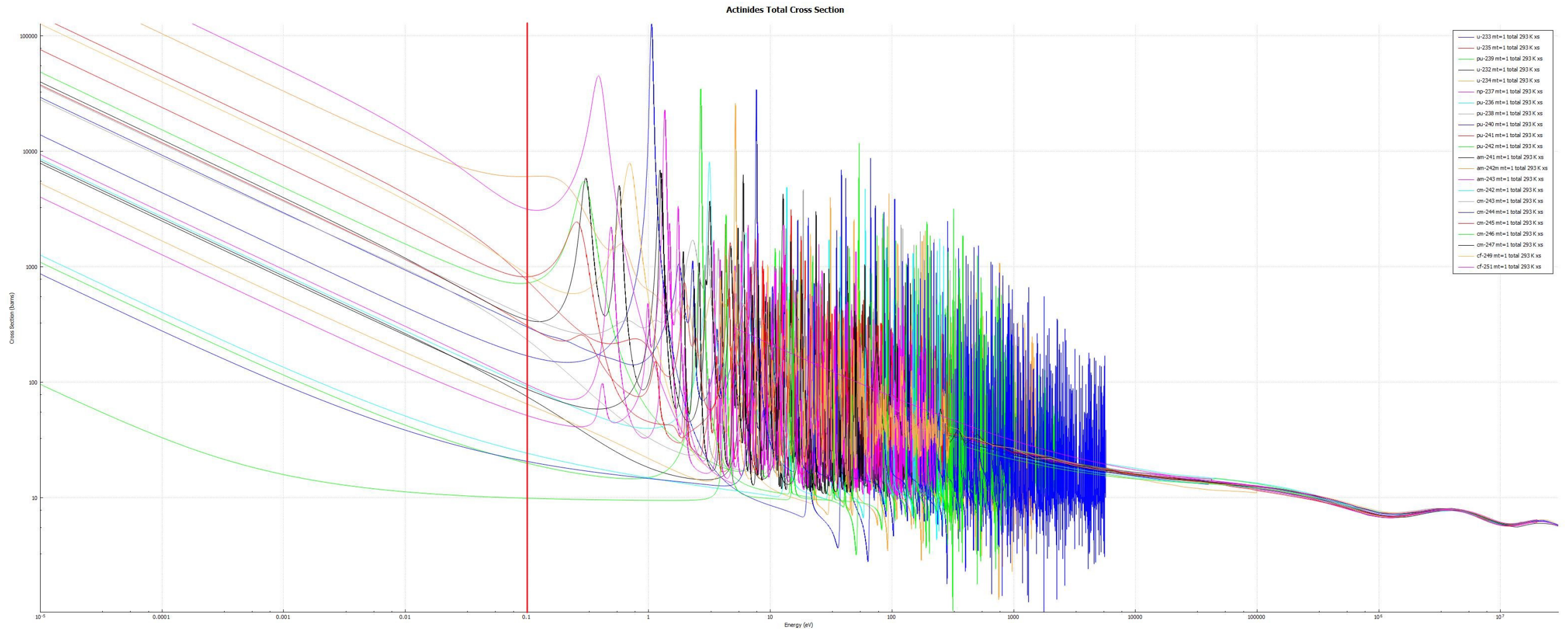


Number of data points for total cross sections



²³⁵U and ²⁵¹Cf total cross sections

Total Cross Section of Nuclides



Sensitivity Study

- TSUNAMI-1D used for generating sensitivity data for application models
 - Sensitivities confirmed by direct perturbation calculations
 - Adequacy of MG 1D method confirmed by comparisons with CE TSUNAMI
- VALID and NEA used as source for benchmarks
 - c_k threshold of 0.8 used
- Calculational margin generated via c_k trending
 - 0.980 for water moderated and reflected systems
 - 0.965 for polyethylene moderated and reflected systems

Minimum Subcritical Masses

Nuclide	Water (g)	Poly (g)	8.15 (g)
U-233	500	250	-
U-235	700	400	-
Pu-239	450	250	-
U-232	3300	2900	1000
U-234	100000	90000	59000
Np-237	47000	44000	35000
Pu-236	1000	600	600
Pu-238	6300	5800	5100
Pu-240	31000	29000	20000
Pu-241	250	100	185
Pu-242	59000	55000	50000
Am-241	56000	52000	24000
Am-242m	21	11	11
Am-243	120000	108000	65000
Cm-242	9800	9000	6000
Cm-243	200	100	90
Cm-244	20000	19000	11000
Cm-245	58	33	23
Cm-246	65000	60000	16000
Cm-247	1100	650	500
Cf-249	58	33	10
Cf-251	27	15	5

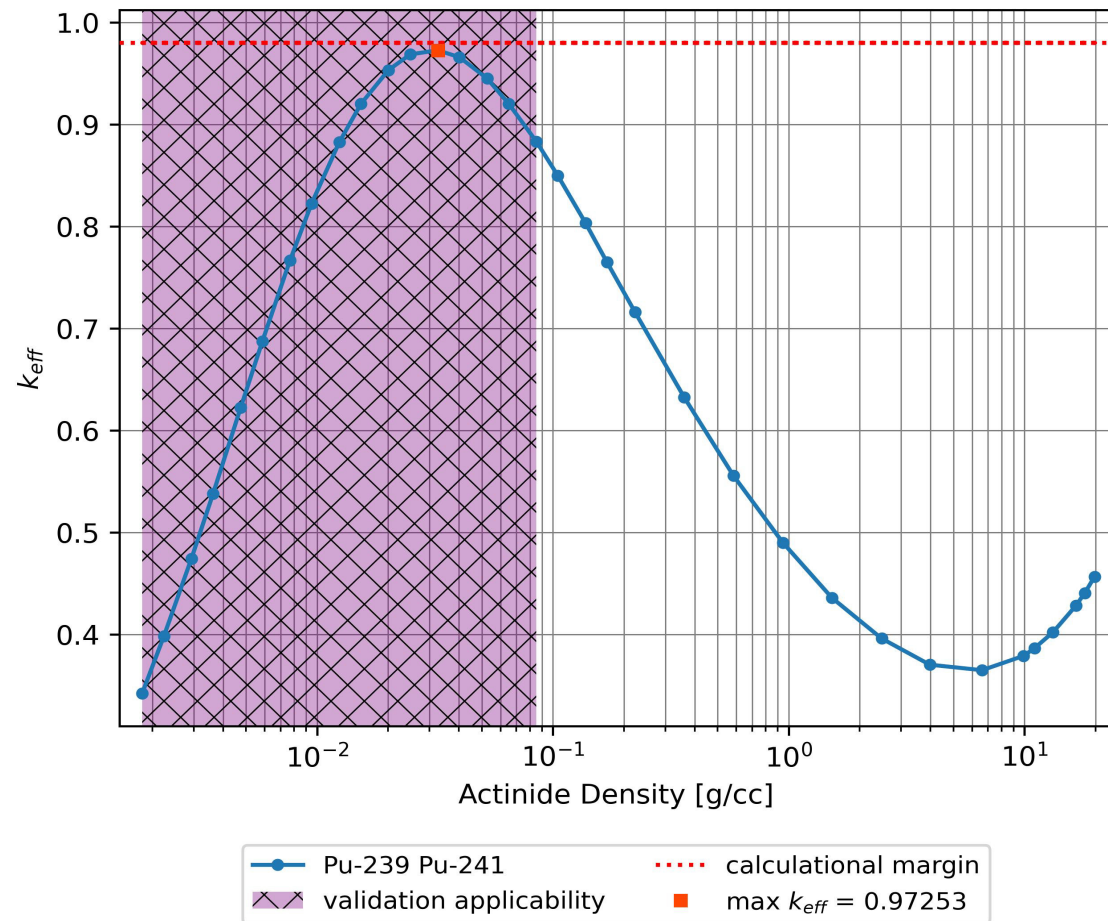
Two Nuclide Mix

Water Moderated and Reflected			
Nuclide	Peak k_{eff}		
	U-233	U-235	Pu-239
U-232	0.94332	0.95189	0.95796
U-234	0.69109	0.67946	0.68568
Np-237	0.68676	0.67217	0.68742
Pu-236	0.96967	0.96872	0.97081
Pu-238	0.66242	0.61224	0.66893
Pu-240	0.68269	0.65830	0.67526
Pu-241	0.97086	0.97123	0.97253
Pu-242	0.75328	0.73399	0.74228
Am-241	0.66117	0.65010	0.65946
Am-242m	0.96814	0.96539	0.96490
Am-243	0.68339	0.67944	0.68780
Cm-242	0.86555	0.88714	0.89897
Cm-243	0.96894	0.96540	0.96855
Cm-244	0.77865	0.81193	0.83088
Cm-245	0.96499	0.96368	0.96333
Cm-246	0.86374	0.87935	0.88773
Cm-247	0.97451	0.97275	0.97582*
Cf-249	0.96597	0.96284	0.96381
Cf-251	0.97096	0.96770	0.96947

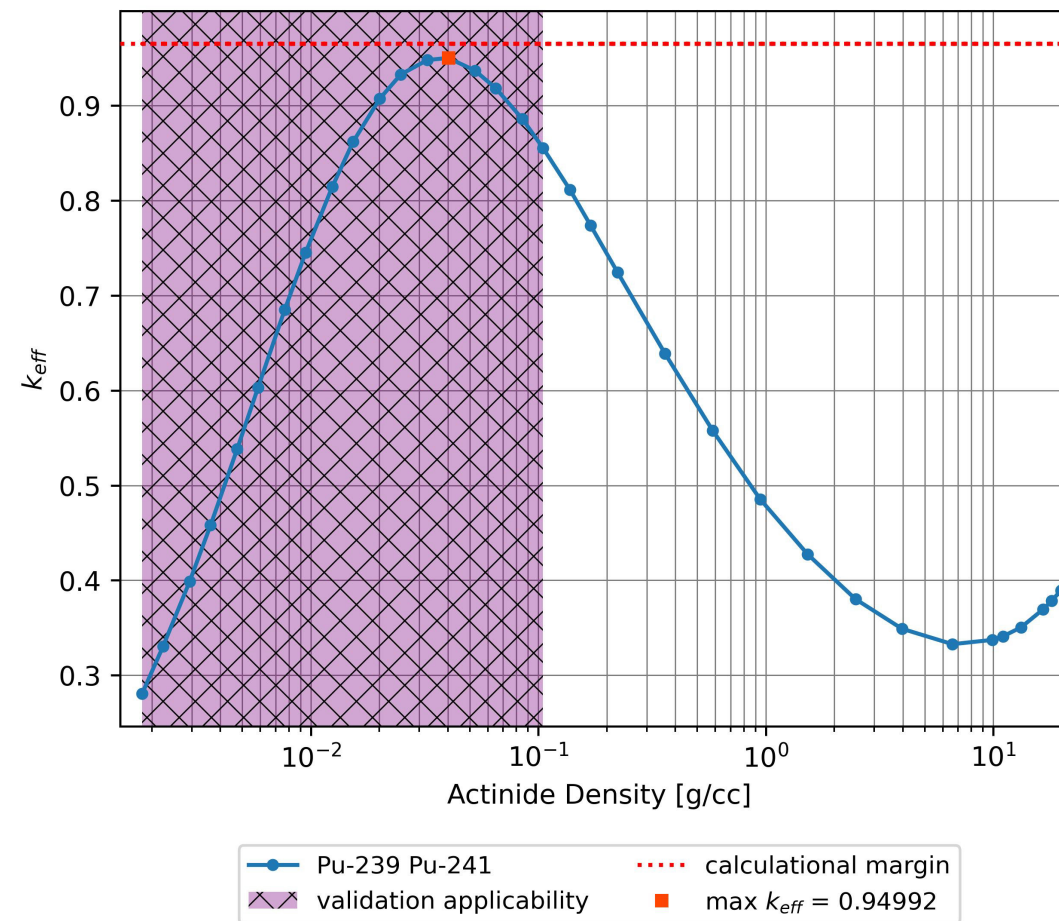
* Max k_{eff}

Polyethylene Moderated and Reflected			
Nuclide	Peak k_{eff}		
	U-233	U-235	Pu-239
U-232	0.91658	0.95326	0.95647
U-234	0.65125	0.64905	0.65243
Np-237	0.65894	0.65255	0.66233
Pu-236	0.93244	0.96100	0.95938
Pu-238	0.63373	0.60226	0.63869
Pu-240	0.64961	0.63653	0.64521
Pu-241	0.91864	0.95049	0.94992
Pu-242	0.70907	0.70673	0.71211
Am-241	0.64059	0.63493	0.64037
Am-242m	0.92694	0.95331	0.95197
Am-243	0.65611	0.65725	0.66339
Cm-242	0.79546	0.85636	0.86932
Cm-243	0.92375	0.95166	0.95109
Cm-244	0.71021	0.75365	0.77373
Cm-245	0.92479	0.95217	0.94976
Cm-246	0.80311	0.85438	0.86153
Cm-247	0.93589	0.96355*	0.96285
Cf-249	0.92555	0.95271	0.95025
Cf-251	0.93112	0.96004	0.95600

^{239}Pu and ^{241}Pu Mix

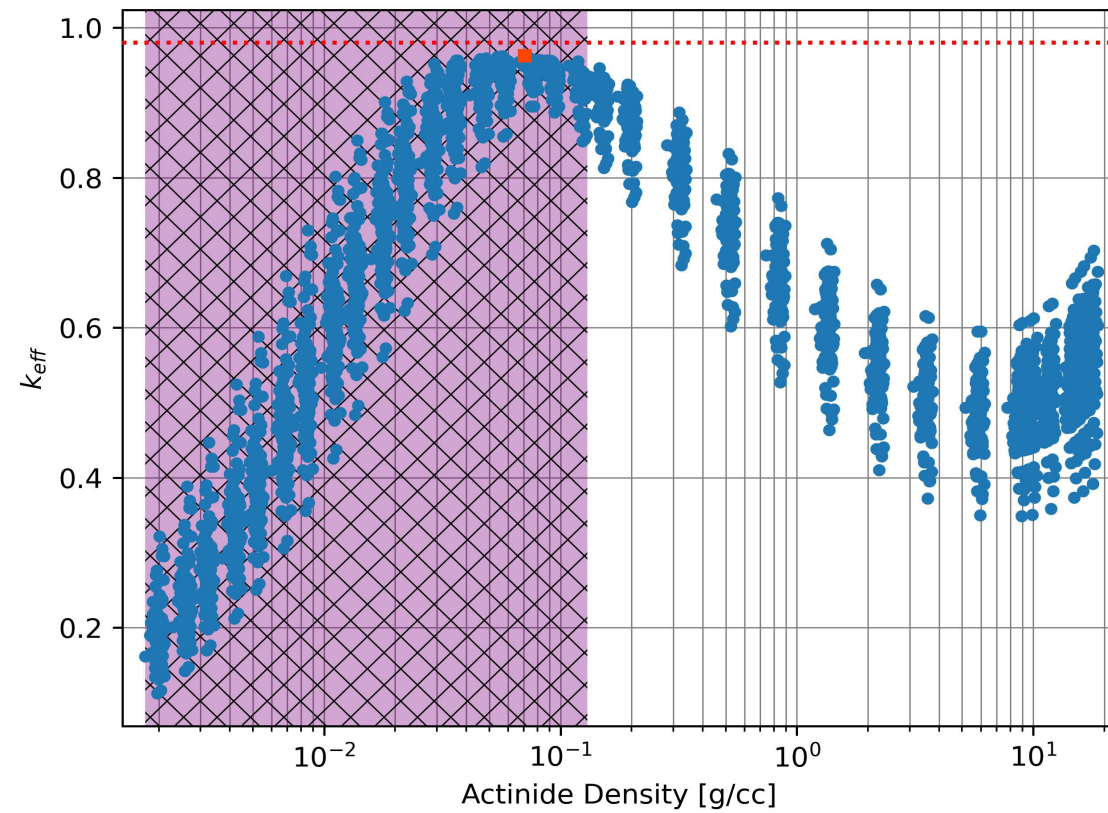


Water Moderated and Reflected



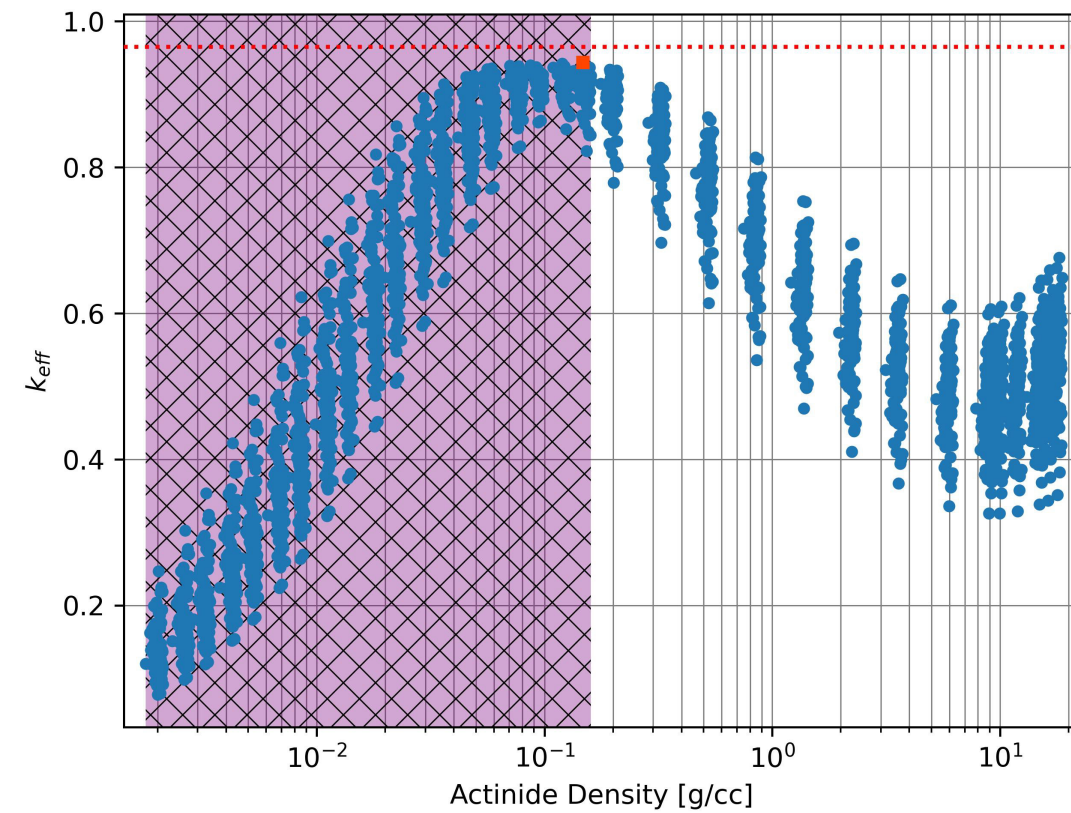
Polyethylene Moderated and Reflected

Random Mix of Fissile Nuclides



● random fissile mixture ⋯ calculational margin
 validation applicability ■ max $k_{eff} = 0.96294$

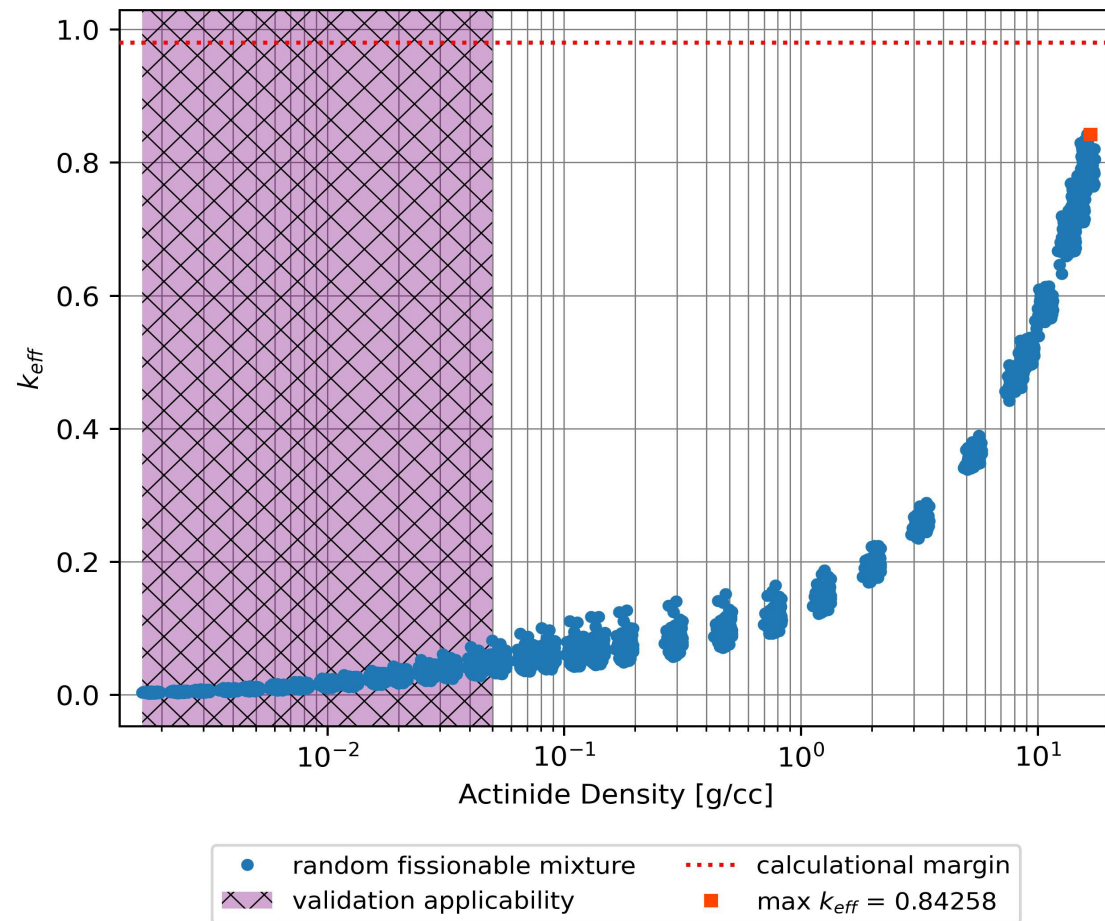
Water Moderated and Reflected



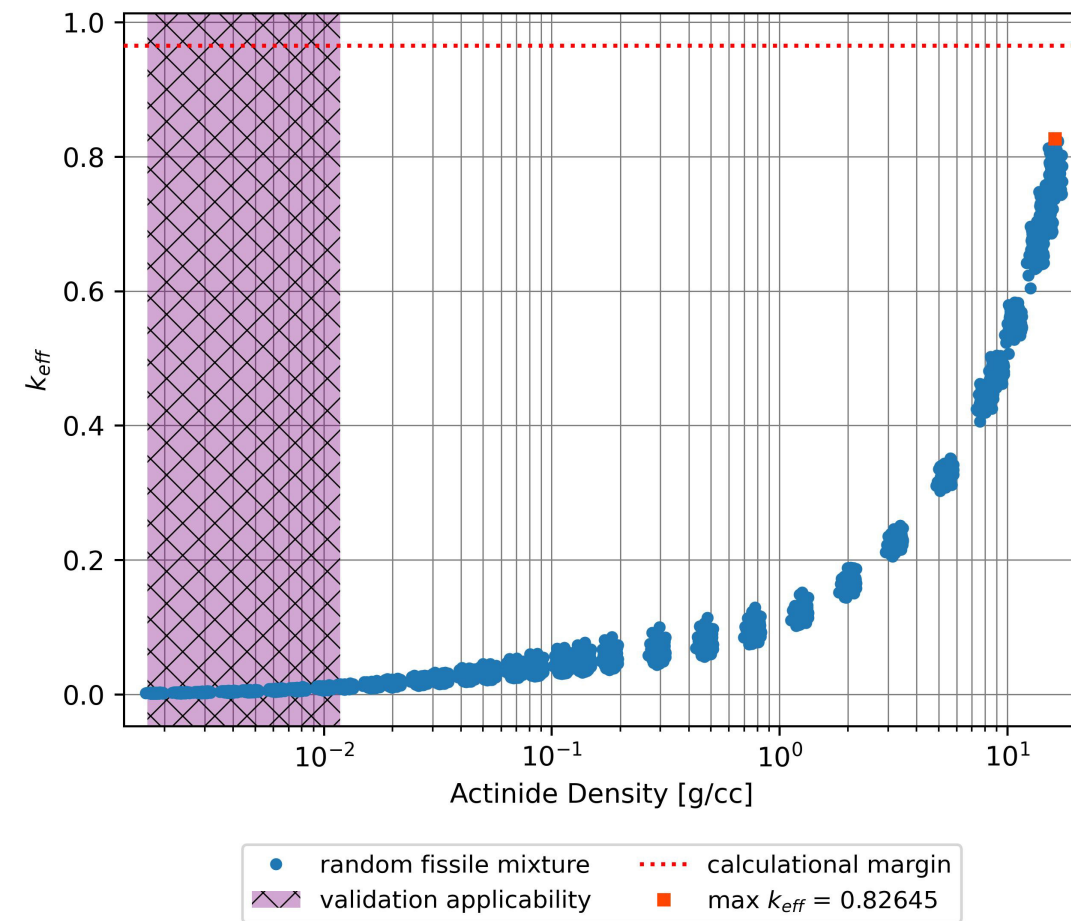
● random fissile mixture ⋯ calculational margin
 validation applicability ■ max $k_{eff} = 0.94367$

Polyethylene Moderated and Reflected

Random Mix of Fissionable Nuclides



Water Moderated and Reflected



Polyethylene Moderated and Reflected

Margin of Subcriticality

- Due to the lack of benchmarks and uncertainties in cross sections a mass penalty is applied via a subcritical factor (Appendix C of ANSI/ANS-8.15)
- Subcritical factors were applied to the ANSI/ANS-8.15 nuclides for water moderated and reflected systems
- Extension of the subcritical factors for nuclides in 8.15 can be made for polyethylene moderated and reflected systems
- Minimum subcritical mass between the computed and 8.15 values is used for each nuclide

Subcritical Masses for Sum-of-Fractions in Water Moderated and Reflected Systems

Nuclide	Computed Mass (g)	factors	Computed w/ factors (g)	ANSI-8.15 (g)	SoF Mass (g)
U-233	500	1	500	--	500
U-235	700	1	700	--	700
Pu-239	450	1	450	--	450
U-232	3300	0.5	1650	1000	1000
U-234	100000	0.5	50000	59000	50000
Np-237	47000	0.7	32900	35000	32900
Pu-236	1000	0.5	500	600	500
Pu-238	6300	0.7	4410	5100	4410
Pu-240	31000	0.7	21700	20000	20000
Pu-241	250	0.7	175	185	175
Pu-242	59000	0.7	41300	50000	41300
Am-241	56000	0.5	28000	24000	24000
Am-242m	21	0.5	10.5	11	10.5
Am-243	120000	0.5	60000	65000	60000
Cm-242	9800	0.5	4900	6000	4900
Cm-243	200	0.5	100	90	90
Cm-244	20000	0.5	10000	11000	10000
Cm-245	58	0.5	29	23	23
Cm-246	65000	0.5	32500	16000	16000
Cm-247	1100	0.5	550	500	500
Cf-249	58	0.5	29	10	10
Cf-251	27	0.5	13.5	5	5

Californium Production

- Subcritical mass using the SoF method:
768 grams
- Subcritical mass using the most reactive fissile mass subcritical limit from Cf-251:
5 grams

Nuclide	Mass (g)	Mass with Margin of Subcriticality (g)
pu-238	1.192114	0.463458
pu-239	0.715268	0.278075
pu-240	663.8882	258.0997
pu-241	2.384228	0.926916
pu-242	99.30309	38.60604
am-241	11.68272	4.541887
am-243	75.69923	29.42958
cm-244	215.7726	83.88588
cm-245	50.66484	19.69696
cm-246	809.6838	314.7806
cm-247	44.70427	17.37967
cf-249	1.072903	0.417112
cf-251	0.238423	0.092692
Total	1977.002	768.5986

Conclusions

- No instances of the use of the SoF method resulted in k_{eff} values exceeding the calculational margin
- When utilizing the SoF include all fissile nuclides
- Provides additional flexibility than ANSI/ANS-8.15 for mixtures
- Extend validation applicability by extending validation

Acknowledgements

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- Team: Andrew Prichard (PNNL-Retired), Travis Greene (ORNL), B.J. Marshall (ORNL), Alex Lang (ORNL)

References

- SCALE Code System, ORNL/TM-2005/39, Version 6.2.4 (April 2020).
- ANSI/ANS-8.15-1981, “Nuclear Criticality Control of Special Actinide Elements,” American Nuclear Society, La Grange Park, IL, 1981.
- ANSI/ANS-8.15-2014, “Nuclear Criticality Control of Special Actinide Elements,” American Nuclear Society, La Grange Park, IL, 2014.



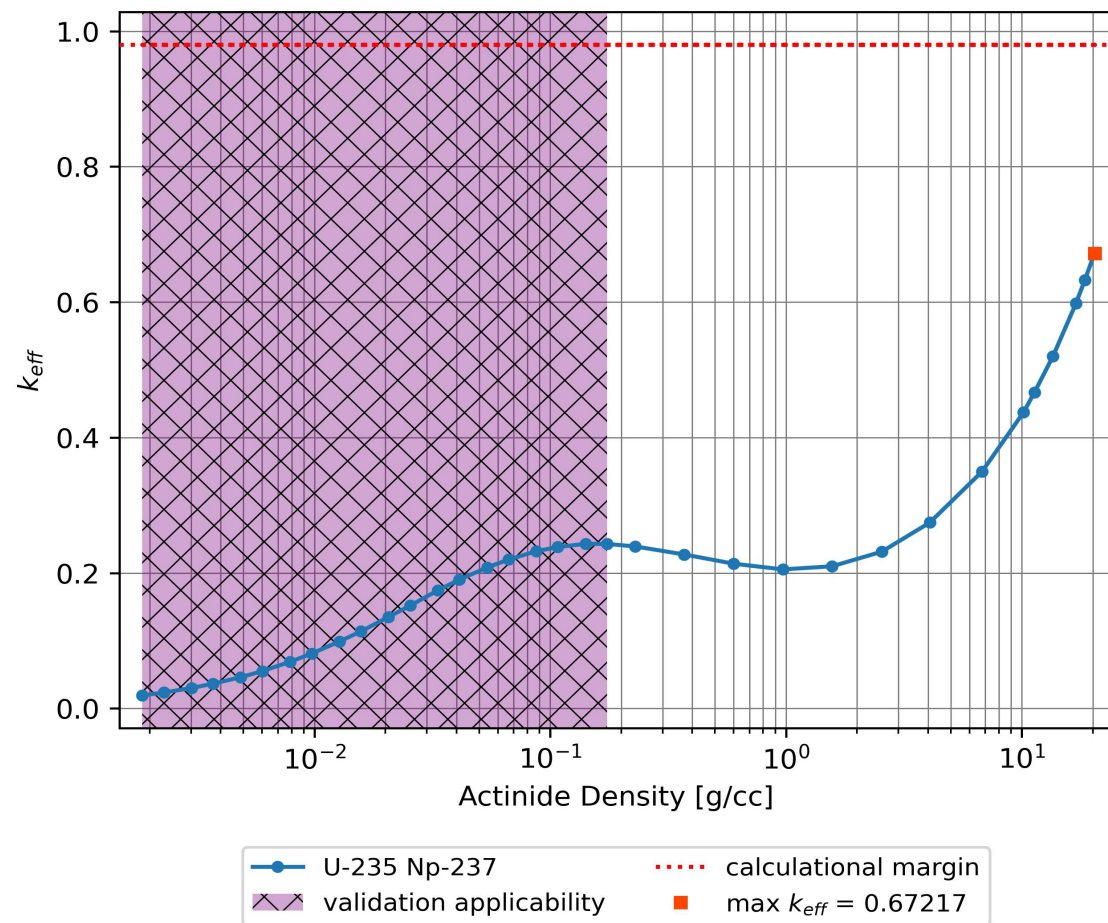
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Thank you

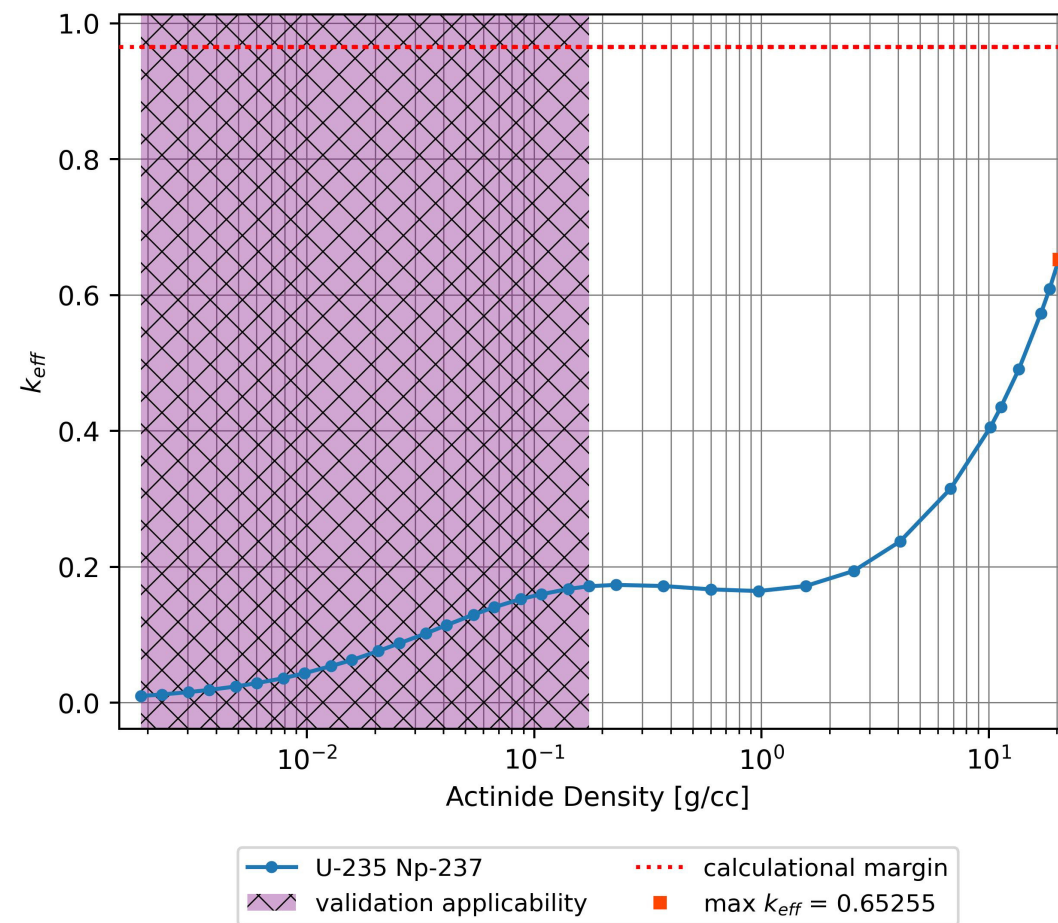
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^{235}U and ^{237}Np Mix

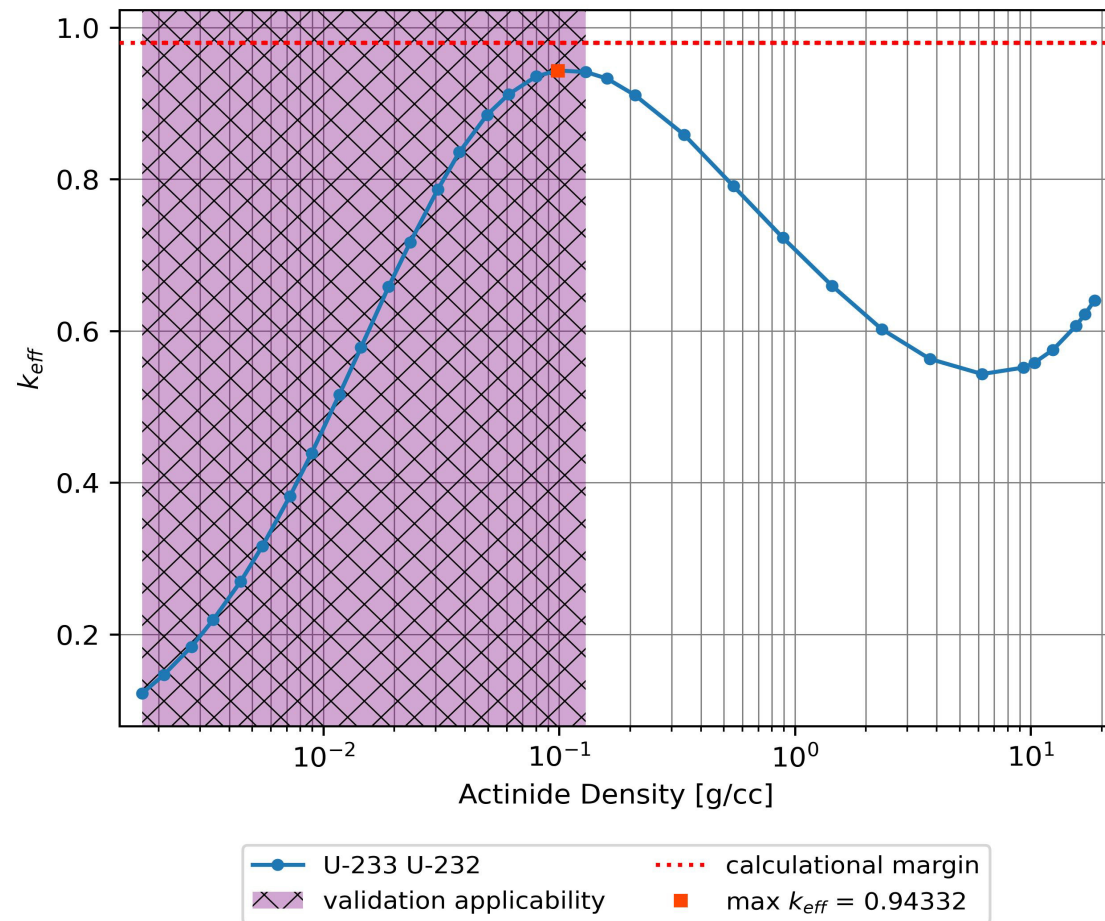


Water Moderated and Reflected

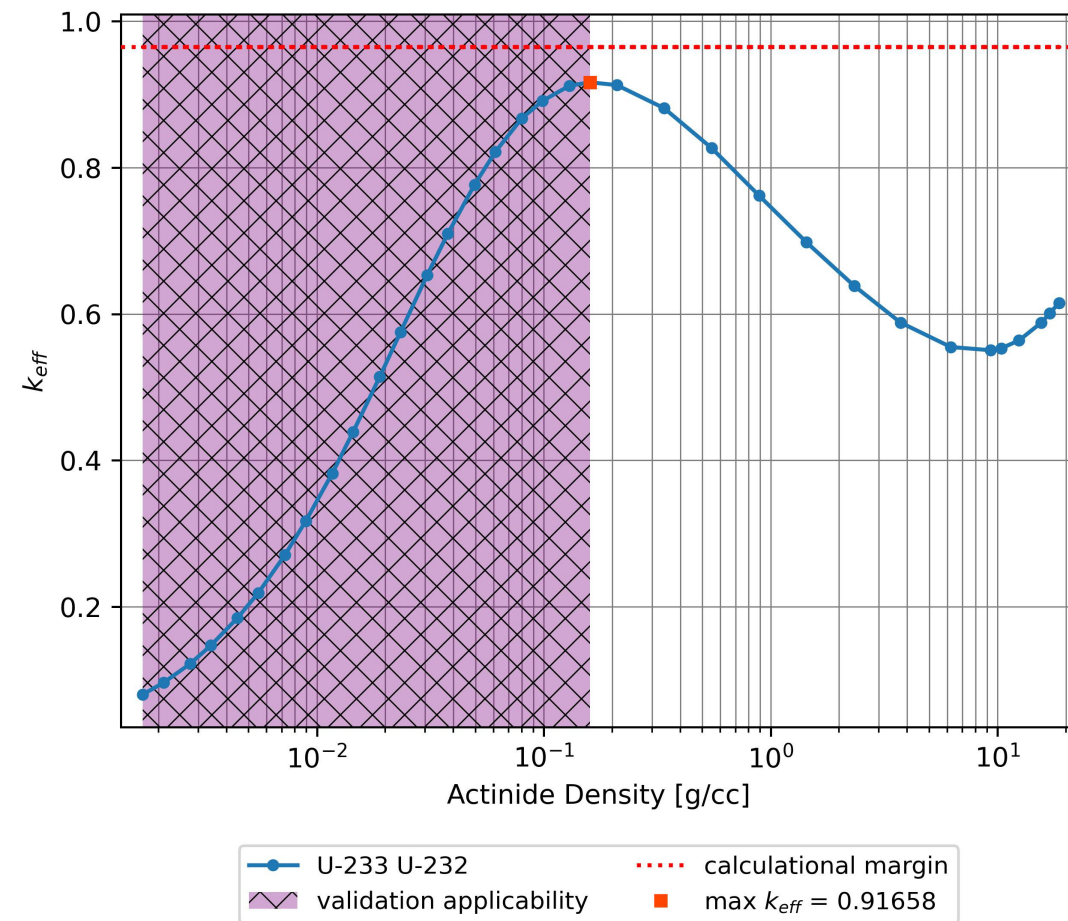


Polyethylene Moderated and Reflected

^{233}U and ^{232}U Mix



Water Moderated and Reflected

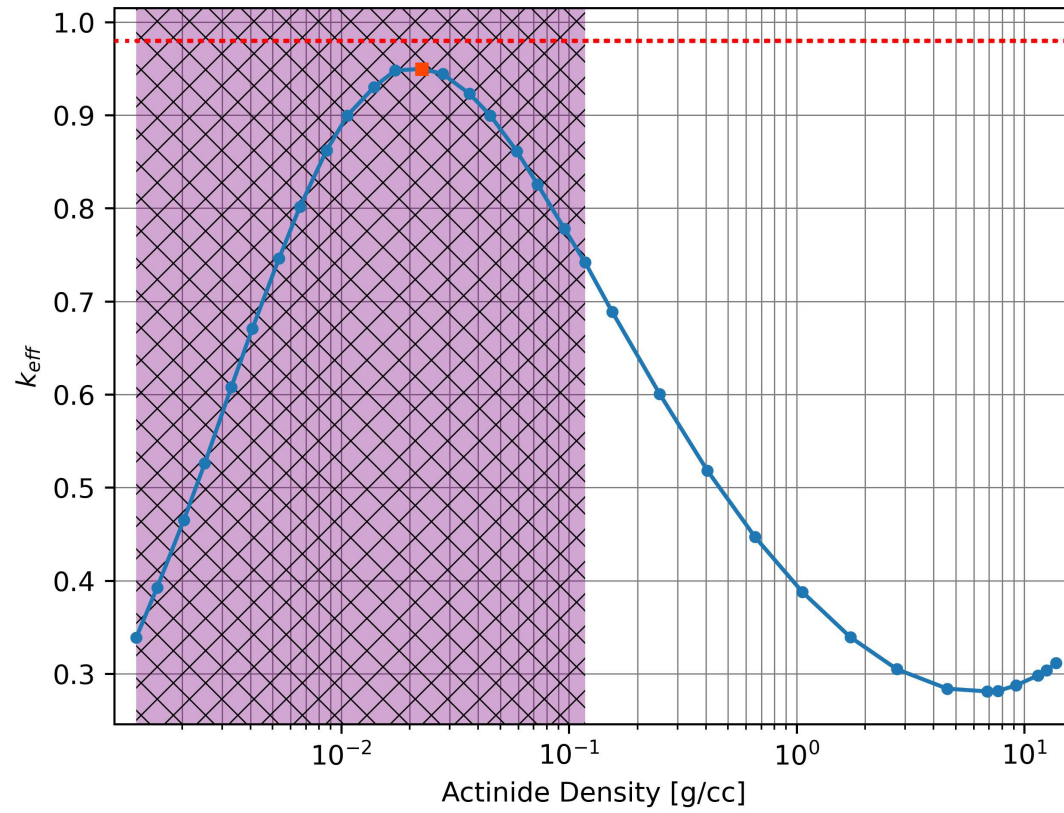


Polyethylene Moderated and Reflected

Subcritical Masses for Sum-of-Fractions in Polyethylene Moderated and Reflected Systems

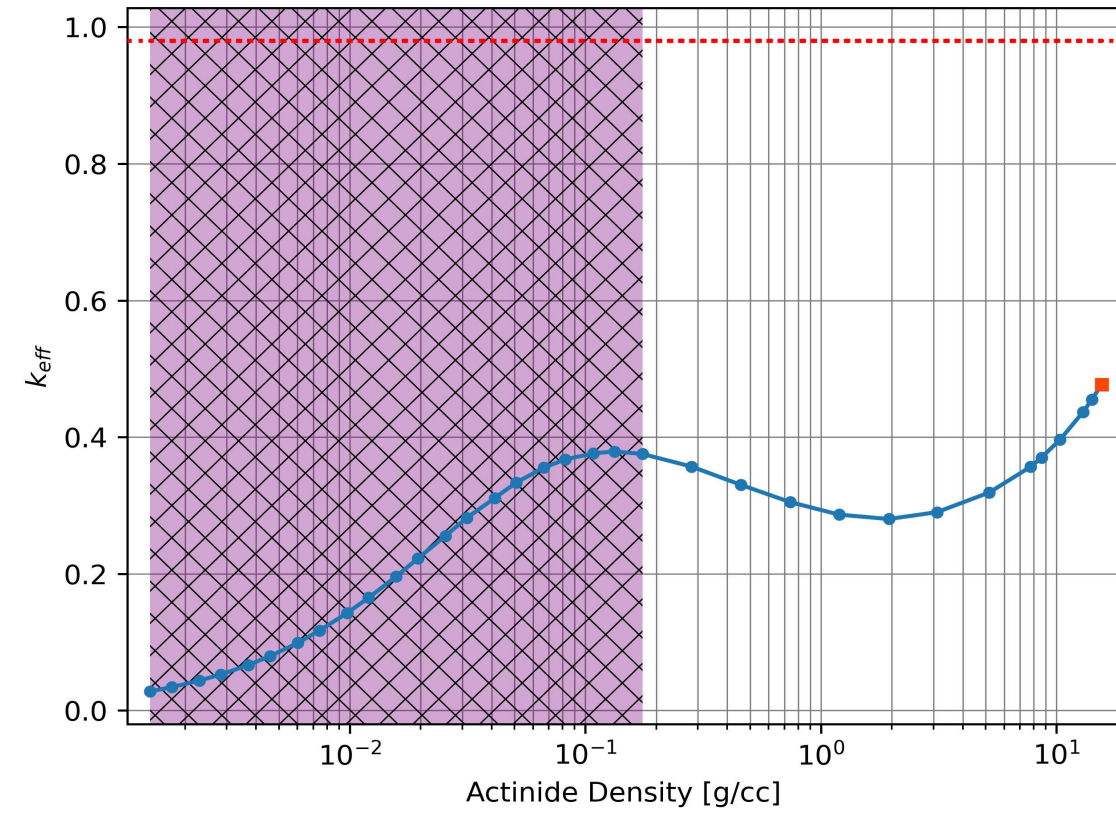
Nuclide	Computed Mass (g)	factors	Computed w/ factors (g)	ANSI 8.15 (g)	SoF Mass (g)
U-233	250	1	250	--	250
U-235	400	1	400	--	400
Pu-239	250	1	250	--	250
U-232	2900	0.5	1450	1000	1000
U-234	90000	0.5	45000	59000	45000
Np-237	44000	0.7	30800	35000	30800
Pu-236	600	0.5	300	600	300
Pu-238	5800	0.7	4060	5100	4060
Pu-240	29000	0.7	20300	20000	20000
Pu-241	100	0.7	70	185	70
Pu-242	55000	0.7	38500	50000	38500
Am-241	52000	0.5	26000	24000	24000
Am-242m	11	0.5	5.5	11	5.5
Am-243	108000	0.5	54000	65000	54000
Cm-242	9000	0.5	4500	6000	4500
Cm-243	100	0.5	50	90	50
Cm-244	19000	0.5	9500	11000	9500
Cm-245	33	0.5	16.5	23	16.5
Cm-246	60000	0.5	30000	16000	16000
Cm-247	650	0.5	325	500	325
Cf-249	33	0.5	16.5	10	10
Cf-251	15	0.5	7.5	5	5

Cf Production



—●— californium process mixture - - - calculational margin
 validation applicability ■ max $k_{eff} = 0.94968$

Fissile only



—●— californium process mixture - - - calculational margin
 validation applicability ■ max $k_{eff} = 0.47716$

Fissile and fissible