

## **BOOK56R**

### *Notes:*

Blank pages: inside page opposite page 1, 3, 4, 21, 126, 152, 153, inside back page opposite page 156

- page 9 has (8.5x11) graph sheet attached
- page 94 has 2 (8.5x11) sheets attached
- page 108 has (8.5x11) sheet attached
- page 122 has 2 big graph sheets (print is light) attached
- page 153/154 has piece of red tape at top

*Scanned by:*

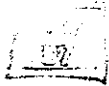
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*RSICC /Oak Ridge National Lab.*

*August 17, 1999*

DRAWER 4  
BACK OF  
DRAWER  
ALL CYLINDERS

**SECRET**



COMPUTATION BOOK



NAME	Number
K-1095 NITRATE EXPERIMENTS —	30

Course .....

Used from 11/7 1949, to ..... 19.....  
EXPERIMENTS 315 →

HARVARD COOPERATIVE SOCIETY  
Cambridge, Massachusetts

**RESTRICTED DATA**

This document contains restricted data as defined in the Atomic Energy Act of 1946.

cylinder areas

Diam.	cm <sup>2</sup> area
9	410.3
10	506.6
12	729.5
15	1140.0

SECRET

Inv. 60

INV. 2

AUG 60

CLASSIFICATION CANCELLED  
DATE 6/3/60  
For the Atomic Energy Commission  
Jack H. Kahner for the  
Chief, Declassification Branch

Inv. 69

This document consists of 156 pages.  
No. 1 of 1 copies, Series A

SECRET

RESTRICTED DATA

This document contains restricted data as defined in the Atomic Energy Act of 1946.

This document consists of 161 pages.  
No. 1 of 1 copies, Series A

correct documentation  
5-25-60

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EXPERIMENT 315

11/7/49

10" AL REACTOR,  $H/K = 242$ , ONE SHELL FILLED WITH  $H_3PO_4$  - NO OTHER TAMPER-

FOX  
CRONIN  
CALLIHAN

TRIP POINTS, #3 - 92+100, #6 - 6.5 x 1000, #7 - OK -  
INSTRUMENT SCALES, #3 3100, #4 116 #5 x 5, #6 x 25.

SOURCE - 8cm above bottom of reactor -  $\approx 15$  cm on scale.

Time	Reading	I	II	I	II	Notes
10:30 A	Filling div from 8H.					
35	#8 Empty at 5.1 cm - filling from #7					
40	H = 9.2 cm	6.25	7.25			
		5.75	7.25			
		6.0	7.25			
48	= 19.5	21.5	24.5	0.28	0.30	#7 empty, filling from 6F.
56	= 22.5	31.0	35.5	0.19	0.20	
11:05	= 24.1	36.0	43.0	0.17	0.17	
		38.0	45.0			{ Checked for NO <sub>2</sub> & PO <sub>4</sub> leaks - blew down sight glass - Response to control rod & source OK
:20	= 25.0	41.0	48.0	0.15	0.15	
:27	= 28.0	72.5	83.0	0.08	0.09	
:32	= 30.5	158.0	184.0	0.04	0.04	stop filling from #6; filling from #5E
45	= 32.2	636	742	0.01	0.01	
		125	137	0.05	0.05	CONTROL ROD IN (VALUE = 2 cm)
:54	32.6	CRITICAL - ROD OUT				
	32.5	SUB CRITICAL				

CRITICAL. SIGHT GLASS AT 32.6 cm.  
Bottom concave 0.9  
Zero - 1.1  
Critical Ht 34.6 cm  
- v<sub>02</sub> 17.582 ✓  
- mass 1.83 + 7.5 kg.  
H/K 240

INVENTORY: #5 - 12.5 cm.  
#6 - 12.5 cm.  
#7 - 9 cm.

6  
11/7/49

Exp. 316  $\frac{H}{X} = 242$

10" Al Reactor 2 shells  $H_3PO_4$  no other reflector.

Henry  
Fox  
Cronin

Source at 8cm from bottom  
Instruments same as 315

	sol'n HT.	#1	#2	c/c	c/c	
3:05 PM	9.3	8.25	4.25			
		8.00	5.00			
3:15	18.7	19.0	13.0	.42	.355	
3:22	21.8	28.5	23.5	.28	.19	stopped from #1
3:30	25.0	62.5	60.5	.13	.075	from #3
3:40	27.1	944	975	.0085	.005	
3:50	27.25	Rod out	barely super critical			
	27.2	Rod out	barely sub critical			

Critical at  $27.225 \pm .025$  cm.

5:00 - Phosphoric acid <sup>boiled over</sup> or <sup>leaked out</sup> and was in lampers tanks - necessary to take shells apart and rinse out tanks and shells.

11-8-49

Shells checked for leaks - none apparent.

Critical - right glass - 27.2  
 Bottom counter 0.9  
 Zero - 1.1  
 CRIT. HT 29.2 a  
 - rod 14.80R ✓  
 - men 1.55 + 4.9 kg  
 $\frac{H}{X} 240$

Exp. 317  $\frac{H}{X}$  242

7

11/8/49  
Fox  
Machlin  
Crown

10" Al Reactor 4 shells  $H_3PO_4$  no other reflector  
Source at 8 cm from bottom  
Instruments Trip Point Starting scale  
#3 90 x 100 x 100  
#4 NG NG  
#5 — X 1  
#6 7 x 1000 x 25  
Photo-multiplicator 3" Smg Ra —  
Process monitor 1000 c/m —

Time	sol'n HT	#1	#2	c/c <sub>1</sub>	c/c <sub>2</sub>	
1:35						
1:40	9.3	3.35 } 3.5 3.50 }	5.25 } 5.5 5.70 }			#8 empty at 5.0 cm Falling from #7
1:48	16.0	11.0	14.0	32	39	#7 empty 18.5"
1:56	18.1	14.5	20.0	24	27.5	
2:05	21.0	31.5	40.0	1.1	1.37	Falling from #6
2:16	23.0	77.0	96.0	.645	.657	
2:25	24.5	347	436	1.001	.0013	Falling from #3

2:35 26.3 critical rod at 14 cm  
super-crit rod at 19.6  
20 sec later it became sub-crit. no other change  
super crit 26.0  
20 sec later it became sub-crit " " "  
This is due to a density effect caused  
by the attack of the  $H_3PO_4$  on the aluminum in-  
creasing rapidly with temp. - a sort of auto-  
catalytic effect. Final temp was near boiling pt.  
of water.

The shells were rinsed outside, dumped in barrel  
and rinsed.

Drum back to previous values

- #8 - DV + 5 cm. ~ 10"
- #7 - 13.5 " " "
- #6 - 13.0 " " "
- #3 - as before - 13.0 approx

Other not used

Height of shell at critical	26.3 cm
Bottom case	0.9
Zero	1.1
Critical HT	28.3 cm
Vol	14.32
mass	1.50 kg + 1.14 kg
	2.64
	H/X 240



8 Cronin  
Fox  
Morfitt  
11/10/49

Exp #318

11/22/42

Trip Points { #3 #6  
92x100 6x1000  
Starting Scales { #3 #4 #5 #6  
2x100 x10 x5 x25

10" Al flat-bottom ("movable" cyl. used in interaction) reactor provided with an <sup>additional</sup> control rod operating horizontally along the diameter of the base. The control rod was built to Hanford specifications. Cylinder otherwise normal & completely water tapered.

Purpose of experiment: To check the effectiveness of the control rod in the proposed Hanford design of their critical mass experimental apparatus. See Hanford feasibility report.

Source @ 7.5 cm from bottom H. Control Rod completely away from reactor. Reading on H.C.R. scale = 69.0 cm.

When the H.C.R. scale reads 0.0 the rod is 15.2 cm past the <sup>of the reactor</sup> outer surface on the other side of the reactor from which the control rod enters.

11-11-49 - Experiment not run on 11-10 because of lack of time

Time	Hgt. Soln.	#1	#2	C/c.	C/c.	Position of rods	Remarks
9:40	9.3 cm	2.5 } 2.25 } 2.25 }	2.5 } 3.0 } 2.25 }			out	background
10:00	12.0 cm	3.25	3.50	.71	.74	out	
		3.00	3.50				
10:14	14.4	4.25	6.50	.54	.40		
		4.25	6.00		.43		
10:20	14.4	4.00	5.75	.57	.45	Hanford C Rod in	other Rod out
		4.50	5.50	.51	.47		
		4.25	5.50	.54	.47	Normal Rod in	Hanford Rod out
10:30	16.2	6.00	9.25	.38	.28	Normal Rod in	HCR out
		7.00	9.50	.33	.27	Normal Rod out	HCR out
		6.25	9.50	.37			
		5.25	8.50	.43	.30	Normal Rod out	HCR IN
10:55	18.3	10.25	18.50	.235	.14	Normal Rod IN	HCR out
		11.00	20.5	.208	.13	NORMAL Rod out	HCR out
		10.0	17.5	.23	.15	Normal Rod out	HCR IN
11:07	19.4	17.5	35	.13	.074	Normal Rod in	HCR out
#402		22.25	42.25	.10	.061	Both Rods out	
		16.0	30.5	.144	.085	Normal Rod out	HCR IN
11:30	20.0	29.0	59.0	.079	.044	Normal Rod out	HCR out
		39.0	76.5	.059	.034	Both Rods out	
		24.5	45.5	.094	.057	Normal Rod out	HCR IN

NOTE: 11/21/49 Cronin says "Normal" Rod was in tamper, in contact with cylinder.

Exp 318 (cont)

Time	Sol'n Ht.	#1	#2	co/c <sub>1</sub>	co/c <sub>2</sub>	Zero = 10 cm Normal Rod	HCR
11:42	20.6	104.5	214.5	.022	.012	IN	out
		43	86.5	.053	.03	IN	IN
		61	122.5	.038	.02	out	IN
12:05	20.5	Critical				at 30 cm	out
		sub-critical				out	out
		Critical at 20.55 ± .05 cm					
12:15	20.8	54.0	112	.042	.023	IN	IN
		111.0	238	.025	.011	OUT	IN
		21.1	167	<del>355</del>	.013	.007	IN
12:30	21.0	Critical				20.5 <sup>(0.6 cm below)</sup> <sub>at 21</sub>	IN
		Critical				27.0 <sub>1 cm above</sub> <sub>at 21</sub>	IN
		Critical at 20.9 ± 0.1 cm					

20.55  
 difference = 0.35 cm = width Hanford Rod in.

Sight glass reads 0.30 cm when solution is at zero in flat bottom reactor

NOTE: Al sheath for horizontal rod introduces a void - 1 7/16" in diameter.

Summary:

<del>Sight glass at critical</del>	<del>1" Hanford Rod at level above reactor bottom</del>	<del>1" Rod in sample</del>
	20.55 cm	20.9
Sight glass at critical	No Rods + void	1" Rod Horizontal
corr =	20.55 cm	20.9 cm
H <sub>c</sub> =	- .30	- .30
V <sub>c</sub> =	20.25 cm ✓	20.60 cm
M <sub>c</sub> = U	10.260 liter	10.438 liter
M <sub>c</sub> = X	+149 Kg +0.18 Kg	+160 Kg +0.18 Kg
	V <sub>c</sub> = 10.26	H/X 240
	M <sub>c</sub> 1.07 kg	
	H/X 240	

Reciprocal Multiplication  
vs

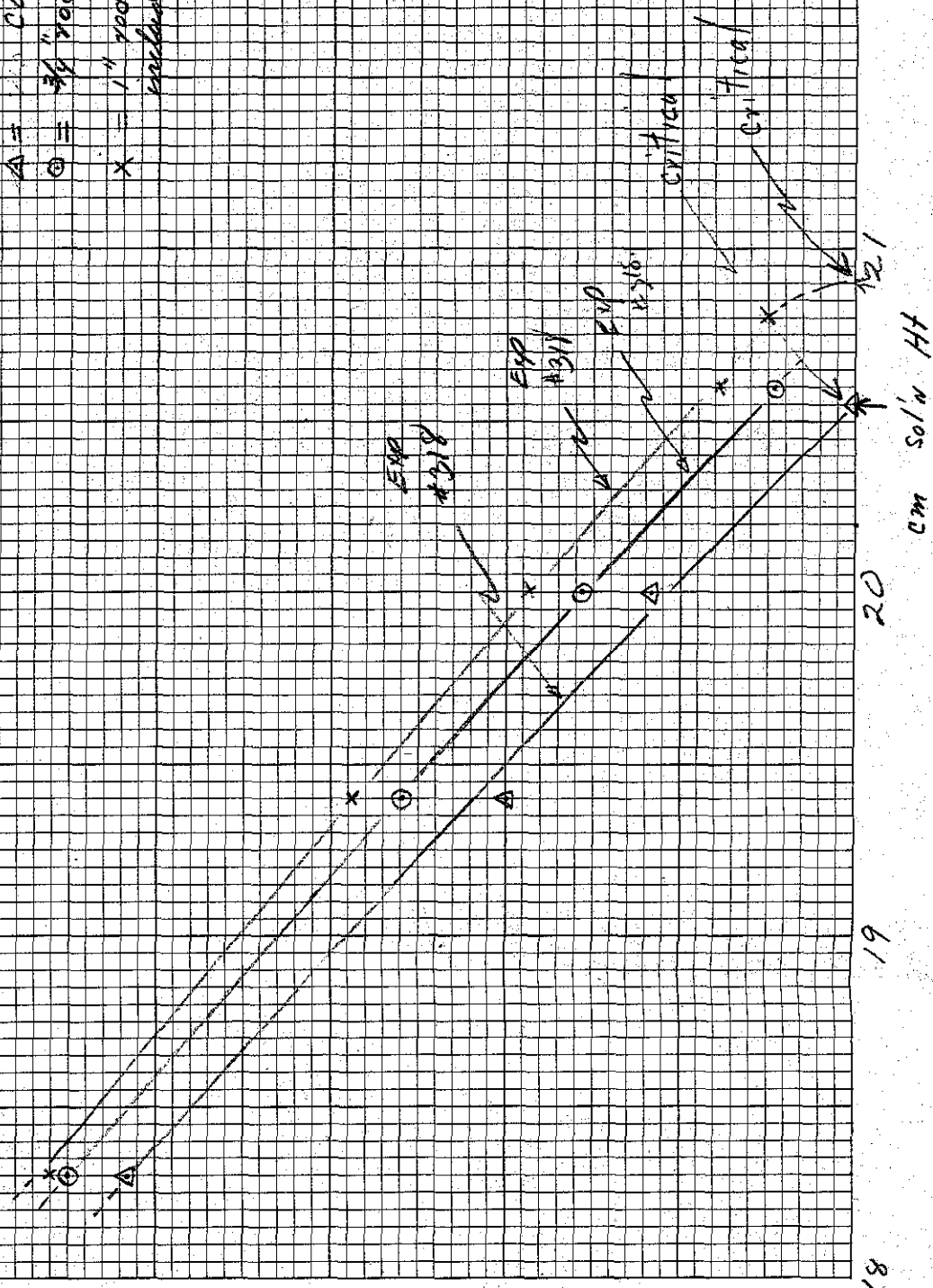
Solution Height Water Top

10" Al Reactor H.M. 100" = 2.40

A = Control rods out

⊙ =  $\frac{3}{4}$ " rod in water reflector vertical

x = 1" rod in water horizontal including  $\frac{1}{16}$ " Al Sheath



.3

$\frac{1}{M}$

.2

.1

18

19

20

20.1

cm sol'n HT

16/11/49

Cromie  
Henry  
Fox

Expt. 319

H/X = 292

10" flat bottom al. reactor Tamped -  
Inst. same as previous Expt.  
Source same

Object: Comparison of values of 1/4" & 1" control rods  
in #2 position, outside reactor. Also effect  
of void below reactor introduced by al  
tube across bottom in the Hanford position

1" control rod in #2 rod position - zeros at 7cm  
Al. tube removed from bottom  
Remainder: Same as #318

11/11/49?

Time	Sol. Ht.	C <sub>1</sub>	C <sub>2</sub>	C <sub>1</sub> /C <sub>2</sub>	Q <sub>1</sub> /Q <sub>2</sub>	Remarks
2:55 PM	9.3 cm	7.0 6.0 6.5	2.5 2.5	1.0	1.0	
3:10 PM	14.6	10.5	7.0	.650	.357	from #6 incl Calibration Marlett i.w.
	17.4	19.5	13.5	.333	.185	
	18.9	36.0	27.5	.180	.091	
	19.9	32.0	24.5	.203	.102	Use #3
	20.4	108.5	95.0	.060	.026	
	20.4	197.0	178.0	.030	.014	Critical

Conclusion: Critical at 20.4<sup>cm</sup> on sight glass

Drainback in #6 to 8.0 from 18.8

in #8 to DV + 8.0

#7 press (#8 overflown)

No rods + no void

20.4 cm

- .30

Hc 20.10 cm

Vc 10.185 V liters

Mc-U 1.141 Kg

Mc-X 1.064 Kg + .07 kgx

H/X 240

Rod in (1" Hanford Control rod along side

20.65

- .30

20.35

10.28 liters

1.07 kgx

H/X 240

Sight glass markings.

11-14-49

Exp. 320

Moshier  
Henry  
Fox  
Cromin

8" AI Flat Bottom Cyl.  $\frac{H}{X}$  242 Completely Water Temped  
no bottom Central Rod  
Source at 19.5 cm  $\approx$  17 cm from bottom.

Instruments	Trip Pt.	Starting Scale
#3	88 x 100	x 100
#4	—	x 10
#5	—	x 2
#6	6.5 x 100	x 25
#7	2 3/4" from tube	

Time	Sol'n #	#1	#2	c/c <sub>1</sub>	c/c <sub>2</sub>	
11:07	14.9	11.5	23.5			#8 MT (air drained back into cyle)
	25.4	13.0	31.0	.88	.75	filling from #7
	33.5					#7 MT
	15.1					draining into #7 18.4 cm
	<del>38.8</del>	13.5	38.5			#6 MT
	18.4					draining into #6
						into #6

	#1	#2	c/c <sub>1</sub>	c/c <sub>2</sub>	HER	outer N.R.	Inner CR	
1:20	13.4	6.0	3.0			OUT	out	out
		6.0	3.0					
11:30	18.1	7.5	4.0	.82	.75	out	out	outer
11-16-49	Exp 320		Instruments		+ Source		Same as 11-14-49	
10:15 A								filling dir. from #8.
:30		4.0						#8 Empty; longer reads. Same low; work added; for 11-14-49
		4.25	2.5					
		5.5	3.0					
		5.0	3.0					
:55	13.4	5.0	3.0					filling from #7.
11:05	22.0	7.5	6.5	0.67	0.46	out	—	out.
15	27.9							Photo multiplier stopped, during counting, emptying soap into dump pan.

Cleaned up ~

12 11/17/49

Exp 320 A.

CRONIN

8" AI Reactor, flat bottom, H/x = 242. Completely water tamped.

MACCLIN  
CALLINAN

To compare control rods as follows: (1) 3/4" in solution - vertical - 2 1/2' eff. length.  
(2) 1" in tamped, vertical - in contact with edge of reactor.

Inst	TRIP POINTS -	Scale	Source at 19.5cm $\approx$ 12cm above bottom
3	85 x 100	100	
4	—	10	
5	—	2	
6	low X100	25	
7	out	—	

		C <sub>1</sub>	C <sub>2</sub>	M <sub>1</sub> <sup>+</sup>	M <sub>2</sub> <sup>-</sup>	ROD 3/4"	POSITIONS 1"	
9:45 A	#							filling from #8; empty filling from #9
10:12	13.4cm	3.25	2.50					
		3.00	2.50					
		3.1	2.3					
27	24.0	5.25	7.5	0.59	0.31	out	out	
34	28.0	8.25	14.25	0.35	0.16	out	out	
	"	6.75	10.25	0.46	0.22	out	in	
	"	6.25	8.25	0.50	0.28	in	out	
	32.15	8.25	13.00	0.38	0.18	in	out	filling from #6.
	"	13.5	26.25	0.23	0.09	out	out	
11:06	"	9.5	18.5	0.33	0.12	out	in	
1:10	36.5	23.0	50.0	0.13	0.05	out	in	
	36.4	very slightly	subcritical			out	out	
23	"	13.5	23.5	0.23	0.10	in	out	
31	"	12.0	23.0	0.26	0.10	in	out	Some drain back through un-closed valve, VOID.
42	36.55	Sub critical				out	out	
55	36.8	CRITICAL.				out	9cm of rod below sub. level.	
12:03 P	39.0	Sub critical-				out	in	
14	39.5	Critical				6cm of rod below sub level	in	
20	39.5	23.25	48.25	0.13	0.05	in	out	
35	43.5*	CRITICAL				in	12cm rod below sub.	
41	43.3*	CRITICAL - Rods out.				in	out	

DRAW INTO 6 TO 39.0 on scale with 3/4" Rod in solution  
Replaced 1" Rod in tamped with 3/4" rod - retained 3/4" rod in sub -  
To compare values of 1" + 3/4" rods in tamped.

Cont pg 14.

\*\* Corrected for rod displacement, estimated



11/17/49

Exp 320A (Cont)

	H	C <sub>1</sub>	C <sub>2</sub>	M <sub>1</sub> <sup>+</sup>	M <sub>2</sub> <sup>+</sup>	Rod #1	Rod #2
1:35P	H=38.5**	CRITICAL				8cm Rod below surface of sol.	in
1:50	=38.2**	CRITICAL				4cm rod below surface.	in
55	=38.0	SLIGHTLY SUPER CRIT.				cut	in
59	=37.7	Sub CRITICAL.				cut	in

Summary:

Rod Position	Sight glass at Criticality	Δ
No Rods	36.7cm	
3/4" Rod in tamper	37.9	1.2 cm
<del>3/4" Rod</del>		
1" Rod in tamper	39.4	2.7
3/4" Rod in Solution	43.3	6.6
1 7/16" Void <sup>vertical</sup> adjacent to reactor in tamper <sub>2.84 Mc out</sub>	37.2	0.5 (see below)
$\frac{2.7}{1.2} = (\frac{1}{3/4})$		

Attached 1 7/16" ~~rod~~ vertical tube to side of reactor - inserting thereby as void in tamper.

2:25	H=37.6	CRITICAL.	10 cm	out
27	=37.35	"	22 cm	out
31	=37.1	Slightly Subcrit.		

Apparently the <sup>greater</sup> void accompanying the 1" rod than the 3/4" ~~rod~~ rod in does not account for the above 2.8 exponent

Drainback - #6 #7 #8 } in 8" Reactor

Summary	no void No rods	3/4" rod in tamper	1" rod in tamper	3/4" rod in sol'n	1 7/16" void vertical
sight glass	36.7	37.9	39.4	43.3	37.2
void	None	none	none	none	none
H <sub>c</sub>	11.90V	12.30V	12.77V	14.04V	12.02V
V <sub>c</sub>	8.9-2.9 Liters	9.22 Liters	9.586 Liters	10.535 Liters	9.05 Liters
M <sub>c</sub> U	1.00004 Kg	1.0327 Kg	1.0736 Kg	1.1799 Kg	1.0137 Kg
M <sub>c</sub> X	0.733 Kg	0.963 Kg	1.000 Kg	1.101 Kg	0.9455 Kg
	H/x 240	H/x 240	M <sub>c</sub> 1.33 H/x 240	1.47 Kg X H/x 240	<del>1.0137</del> 1.26 Kg H/x 240
* Rod #1	-	3/4" rod in solution			
Rod #2	-	3/4" rod in tamper	(Z <sub>rod</sub> = 20.5cm on scale)		
**	Corrected for rod displacement				



11/18/49.

Crosin  
Henry

Source used in previous experiments replaced with  
 Source (Po-Bc) PB-131 originally 9.58 c of Po or  $19.3 \times 10^6$  n/sec  
 present value approx  $\frac{3.0}{1.79} \times 10^6$  n/sec

Source zero is 7.3 cm on scale in Control Rm.

Hanford control Rod in position - note rod and/or Al tube holding it  
 is easily distorted - <sup>was</sup> necessary to use emery cloth to re-fit  
 rods

11/21/49

EXPERIMENT 321.

CRONIN

8" Al REACTOR, flat bottom, water tamped. H/E = 242.

HENRY  
CALLIHAN.

CONTROL RODS: ① 1" Rod HORIZONTAL UNDER REACTOR, Al tube in contact with water.  
② 3/4" Rod IN SOLUTION. 2 1/4" off center.  
③ 3/4" " " TAMPER. in contact with reactor.

NOTE: Al shell for horizontal rod introduces 1 1/16" void below reactor.

INSTRUMENT	TRIP POINTS	SCALES
3	88 x 100	100
4	No	10
5	No	2
6	6 x 1000	25
7	No	-

SOURCE AT 19.5 cm on scale = 12 cm from reactor bottom.

10:55 A  
11:25

Filling Dk from #8; #8 Empty; filling from #6

	C <sub>1</sub>	C <sub>2</sub>	M <sub>1</sub>	M <sub>2</sub>	1" Rods	3/4" in sol	3/4" in temp.	
H = 12.8	8.0	6.0			out	out	out.	
	6.5	5.5						
	7.5	7.5						
	7.3	6.3						
11:38	20.1	10.5	12.0	0.70	0.52	out	out	out
50	24.7	15.0	21.0	0.49	0.29	-	-	-
56	28.6	21.5	36.5	0.34	0.17	✓	✓	✓
		20.5	37.0	0.36	0.17	in	-	✓
12:11 P	34.0	60.0	121.5	0.12	0.05	out	out	out.
13	37.0	52.0	103.5	0.14	0.06	in	out	out
17		39.5	81.0	0.18	0.08	out	out	in
27	36.0	61.5	130.0	0.12	0.05	✓	✓	in
31		106.5	227.5	0.07	0.03	in	out	out
37		153.0	333.5	0.05	0.02	out	-	✓
1:31		107.5	233	0.07	0.03	-	✓	in
46	35.7					in	-	out
55						out	-	45cm on scale
2:02	37.2					in	✓	12cm below level of out.
2:07						out	✓	5cm above level
						out	✓	7cm below level
	37.45					out	✓	in
2:23		223	490.5	0.03	0.01	✓	✓	in
3:07	37.65					out	out	in
4:07	38.05					✓	-	✓
5:04	38.2					✓	at level	✓
3:00	34.7					✓	out.	out
06	36.65					✓	-	✓

#6 empty; filling for 7

Exp. 321 (cont).

SUMMARY: CRITICAL -	No Rods	1" HORIZONTAL ROD	3/4" VERTICAL ROD IN TAMPER	(No)
at Sight Glass =	36.7 cm	37.1 cm	38.1 cm	
$V_c$ =	<del>8.727</del> <sup>8.93</sup> Liters	9.064	9.2697	
$U_{MC}$ =	1.00000 Kg U	1.015 Kg U	1.038 Kg U	
$X_{MC}$ =	0.933 Kg X	0.947 Kg X	0.968 Kg X	
No zero on bottom connection.	++			
CRITICAL VOL.	11.002 ✓	12.032 ✓	12.312 ✓	12.35 ✓
MASS	1.24 + 20 Bq H/X 240	1.21 Bq 12.1 Bq 12.6 Kg X H/X 240	1.24 Bq 1.29 Kg X H/X 240	

INVENTORY:	#	Length	Location
	6	19.0 cm	in 8" reactor
	7	22.5 cm	in 8" Reactor
	8	5.5 cm + DV	
		5.4 cm	in 15" reactor
		6.4 "	" " "
		1.6 "	" " "

taken on same day

Sample	%U	% X	\$p_{H_2}\$
B-4	9.604		
A-8	9.669 <del>9.669</del>		
C-5	9.655		
D-4	9.588		
E-7	9.566		
F-1	9.680		
G-1	9.646		
H-1	9.641		

total average 77.049  
 average 9.631 93.28 1.163  
 (= 0.0899 g<sup>27</sup>/g)  
 (= 0.1045 g<sup>27</sup>/cc)

$\frac{H}{X} = 239$  corrected for new analysis and displacement

~~gms/cc =  $\frac{4120}{\dots}$  gms/cc~~

Area of 8" cyl. = 248.3 in<sup>2</sup>  
 10" cyl = 506.7  
 15" cyl = 1140.0

bottom correct in lit for fixed cyl (3" section)  
 1.45 cm  
 0.93  
~~0.05~~ 0.41

Crown  
Fax  
Herbit

Experiment # 322 A

11/23/49 19

15" reactor - flat bottom. Unamped H/K 242

Normal Controlled set up. (3/4" rod in solution)

Source @ 7 cm from bottom

Instruments	Scales	Trips @
3	100	75 & 100
4	10	—
5	2	—
6	100/100	6 x 1000

9:30 Dead Vol. Filled from #8

9:48 Filled to 10 cm on scale Cylinder about 3 cm higher than usual

Time	Hgt.	C <sub>1</sub>	C <sub>2</sub>	1/4 <sub>1</sub>	1/4 <sub>2</sub>	Remarks
9:54	10.0	27.5	(26.0)			845 MT
		28,27	27,25			
		(25) 26	25,27			
10:24	15.1	74 71	49	.38	.53	from #2
10:45	16.5	95	70	.295	.37	from #3
11:02	18.0	132	97	.212	.27	#3 MT
11:18	19.9	225	176, 180	.124, .115	.146	from #7
11:32	21.4	423 <del>300</del>	378	.066	.067	" "
	Red in	352	294	.080	.088	
	Red with 3mm by #1 counter, 3mm by #2 counter					
	22.3(?)	1082	1011			
11:58	22.3	928	863	.030	.030	
	Red in	544	519	.047	.50	
	Red with 4 mm, 4 cm					
12:18	21.5	431	387	.065	.068	
	Draw back to 19.8					lunch & change of apparatus.
2:26		228	173	.123	.150	
2:45	19.2	20.1	212	163		
2:50	21.7	794	740	.035	.035	
3:20	21.9	837	755	.033	.037	Stopped #4

No conclusions could be drawn due to apparatus difficulties. from air lines in apparatus. Experiment unsuccessful.

Zero correction = 2.1 cm

20 Carmin.  
Fox  
Mort. H.

11/25/49

Experiment \* 322 B Continuation of 322 A

15" Reactor Flat Bottom H/X = 2402 UNTAMPERED.

Normal Control Rod set up. (one 3/4" rod in solen)  
Source 7cm from bottom.

Instruments	Scale	Trip @
3	X100	85
4	X10	No
5	X2	No
6	X25/100	6 x 1000
7		No.

Time	Solen. Hgt	C <sub>1</sub>	C <sub>2</sub>	1/M <sub>1</sub>	1/M <sub>2</sub>	Remarks
7:30-10:20	Brought up to 12.7 cm using #7 & #8	40, 41, 41	43, 44, 43	1.0	1.0	# AT #7 almost AT
10:25	16.3	82	88	.50	.49	# 6 AT
10:30	19.1	159	172	.25	.22	from #4
10:37	21.2	—	—	—	—	Stopped #4
10:45	21.0	312	421	.130	.103	from #3
10:55	22.25	522	1163	.065	.057	Est. cont/22.0
	Red in	520	740	.077	.058	

Red works between 3.5 x 4. mm.  
23.65 Critical with rod @ 15cm  
23.95 Subcritical with rod out.

Conclusion: Critical @ 23.0<sup>cm</sup> on sight glass.

→ N.B. ZERO OF SIGHT GLASS UNKNOWN AT PRESENT.

Inventory (!)

	#1	#2	#3	#4	#5	#6	#7	#8	#9
Hgt. in terms of 15% off line	off line	off line	> 4cm	74cm	(?)	> 6	> 3.6	—	(?)

Summary:  
Zero correction -2.1 cm  
Sight glass 23.0  
zero correction -2.1  
Bottom center —  
CRITICAL HT 21.3 cm ✓  
- Vol. 23.8  
- mass 24.3 g  
- 2.49 kg  
H/X 240

EXPERIMENT 323

11/25/49

15" Al Reactor, H/x = 242, Tamped.  
(Flat Bottomed Reactor).

Fox  
CRONIN  
HENRY  
CALLIHAN.

Inst	TRM Pts	Inst Scales
3	85x100	100
4	N6	#2
5	N-	1
6	6x1000	25
7	-	-

Source 3cm above bottom = 13.3 on scale.  
Control Rods - #1 - 3/4" dia in sub - 2 1/4" off center -  
#2 - 3/4" " " H<sub>2</sub>O - contact with reactor.

Time	H =	C <sub>1</sub>		C <sub>2</sub>		CONTROL RODS		Notes
		1	2	1	2	#1	#2	
1:22 P	6.35 cm	7.0	6.0	6.5	7.0	out	out	
		7.5	7.0	7.0	6.7			
1:32	8.9	8.5	8.5	.82	.79			from #6 Both Rods out
1:42	11.6	16.5	22.0	.42	.31			Stopped #6 Both Rods out
1:55	12.7	26.0	40.5	.27	.16			Both Rods out sub from #4
2:05	13.6	55.0	93.5	.127	.071			
		51.5	91.0	.135	.073	#2 CR in	#1 out.	
		42.5	66.0	.165	.10	#1 CR in	#2 out.	stopped #4
2:20	<del>14.0</del> 14.3	125.0	220.0	.055	.03	#1 CR in	#2 out	start #3
		Critical				#1 CR out	#2 CR at 14cm above bottom	
	<del>14.5</del> 14.5	Critical				#2 CR in	#1 Rod 8.5 cm from bottom	
2:45	14.5	270	390	.033	.017	#1 CR in	#2 out	
	14.7	Critical				#1 CR in	#2 rod 3cm from bottom	
3:09	14.2	sub critical				Both Rods out.		

Sight glass reading	Both Rods out		#2 out	#1 out
	#1 in	#2 rod in	#1 in	#2 rod in
Summary reading	14.25	14.6 cm	14.6 cm	14.4 cm
Zero correction	-2.1	-2.1	-2.1	-2.1
Bottom correction	-0.4	-0.4	-0.4	-0.4
CRITIC. HT	12.15	12.5	12.3	12.7 cm
	12.6 cm	12.9 cm	12.7 cm	13.07 cm
	13.9	14.25	14.07	14.5
	13.85	14.2	14.5	
Vol.	1.40 kg	1.43 kg	1.46 kg	1.46 kg
miss.	1.45 kg	1.48 kg	1.47 kg	1.47 kg
	H/x 240	H/x 240	H/x 240	H/x 240

[Zero correction - 2.1 cm]

Ex 324.

Callahan  
Foy  
Henry  
Crosin

Same as Ex 323 except - a 1 7/16" Al tube air filled on a diameter at the base of reactor. <sup>also</sup> with Cadmium

	#1	#2	c/c <sub>1</sub>	c/c <sub>2</sub>	
3:36	13.6	48	80.5	.146	.08 Both Rods out.
3:47	14.5	Critical - with #1 Rod 10.5 cm from bottom of Reactor			
3:50	14.4	Barely Super-critical Both Rods out			
	14.0	Critical at 14.35 ± 0.05 cm. ← INSERTED Cd INTO AL TUBE			
4:05	14.6	Sub Critical with 1" Cd rod in 1 7/16" Al tube on diameter of reactor. other rods out			
	14.7	Critical - with #1 CR 8 cm from bottom. #2 out			

Summary - 1 7/16" void 1 7/16" Al tube with 1" Cd Rod  
sight glass 14.35 14.65

Drain back same as Ex 323.

Zero correction - 2.1 cm

∴ 12.6 cm corrected critical height 11/28/49

11/28/49 (FC) Soup put into 15" reactor to just come to bottom - sight glass read 2.1 cm.

Summary:	HORIZONTAL AL TUBE	HORIZONTAL AL TUBE filled with Cd
Sight glass at critical:	14.35 cm	14.65 cm
Zero correction	- 2.1	- 2.1
Bottom -	- 0.4	- 0.4
Critical HT	12.25	12.55
- Vol	13.97	13.0
- MASS.	1.46 kg	1.80 kg 1.30 L ✓
	1.46 kg	1.55 kg
	1.46 kg	1.49 kg 1.50 kg ✓
	1/4 240	1/4 240



Exp. 325

11/28/49

12" A1 Reactor Untamped  $\frac{H}{X} = 244$

Source 10cm from bottom (18.3 on scale)

Trip Points

Inst.	TP	Starting scale
3	82 x 100	x 100
6	7 x 1000	x 25
4	—	x 10
5	—	x 1
7	4" from tube	—

Cronin  
Fox  
Henry  
Macklin  
Callihan  
S. Segal  
Creagan } Westinghouse  
visitors

Time	Sol'n Ht. Sight Glass Readings	0 #1	X #2	c/c <sub>1</sub>	c/c <sub>2</sub>	Dead Vol. taken from #8 earlier Going to 18cm on empty #8 #8 empty - fill to 11 from #7 repositioned counters
1:40	0	-	-			
1:43	5.5					
1:47	(11.0) 11.05	39.5	65.5			
		22.0	40.5			
		22.5	40.0			
1:58						go to 14 from #7
2:00	(14.1) 14.0	22.5	32.0	.96	1.25	
		24.0	32.0			
2:10						go to 18 from #7
2:10½	(16.3) 16.3	37.0	51.5	.60	.78	#7 empty
2:16						go to 18½ from #6
2:18	(18.6) 18.6	56.0	84	.40	.48	
2:23						go to 21 from #6
2:25	(21.1) 21.05	85.5	140	.26	.29	
2:31						go to 24½ from #3
2:34	(24.3) 24.3	168.5	322	.132	.125	
2:39½						go to 26.2 from #3
2:41	26.2	327	675	.068	.060	
2:48						go to 27.6 from #3
2:49	(27.8) 27.7					Subcritical
2:54						go to 28.0 from #3
2:55	(28.5) 28.1					Subcritical
2:57	(11)					add 3mm from #3
2:59	(28.4) 28.35					Critical with rod 2.8cm into soup

Conclude - crit at 28.3 (sight glass)

325 continued @ 326

To Drain to ~ 8 cm & add tampers water!  
 Go to 21.1 into #3 ✓ 3:07  
 Go to 16.3 into #6 ✓ 3:10  
 Go to 8.2 into #7 ✓ 3:15  
 Filling Tampers ~ 3:16 - 3:30

CRITICAL AT SIGHT GLASS = 28.3 cm.  
 Zero correction 0.2  
 Bottom correction 0.7  
 CRITICAL HT 29.2 cm  
 VOL 21.30 L ✓  
 MASS 2.23  
 2.44 kg.  
 H/x 240

Crossion out

Exp 326 12" Al Reactor Tamped H/x ~ 244

Source set at 6 cm (14.3 on scale)

Time	Sight Glass (cm)	rod in	rod out	#1	#2	co/c <sub>1</sub>	co/c <sub>2</sub>	Counters repositioned
3:44	(7.8)	7.8		22.0 21.5	20.0 20.5			Background
3:47	<del>##</del>							go to 11 out of #7
3:49	(11.1)	11.0		39.0	56.5	.56	.36	
3:55								go to 12.5 out of #7
3:56	(12.5)	12.5		71.5	128	.35	.16	
4:04								go to 13.5 " "
4:05	(13.5)	13.5		163	333 1/2	.124	.061	
4:12								go to 14.1 " "
4:14	(14.15)	14.1						Slightly Subcritical
4:19								go to 14.3 out of #7
4:20	(14.4)	14.3						10.4 rod scale Critical with 3.9 cm rod in Soap

Conclude critical at 14.2 cm (Sight Glass)

drain to 5.5 into #7 ✓ 4:39  
 dead volume into #8 ✓

#8 - DV + 9.80 cm = 9"  
 #7 19.5 cm

SUMMARY:  
 CRITICAL AT SIGHT GLASS = 14.2  
 Zero correction 0.25 L  
 Bottom correction 0.7  
 CRITICAL HEIGHT 15.1 cm  
 VOL. 11.01 L ✓  
 MASS 1.15  
 1.15 kg.  
 H/x 240

Zero point correction +0.2 cm with tampers empty  
 determined by comparison with 19" cylinder 11/29/49 (JF)

26  
11/29/99

Experiment # 327

Macklin  
Callahan  
Fox

9" Aluminum Reactor  $\frac{1}{X} = 244$   
Jamped

Trip Points: #3 - 82 on 100 scale; #6-7 on 1000 scale  
7 out scale: #3-100; #6-25; #5-2 #4-5

(Base of source) source: Re-zeroed at 6.8 on scale  
source set at: 16.8 on scale

Time:	H <sub>T</sub>				cp/c <sub>1</sub>	c <sub>0</sub> /c <sub>∞</sub>	
1:55	9.3	rod in					#4 empty
1:56							11 from #3
2:00	11.0		18.5 } 190	19.0 } 14.2			Blow back 86, Blkg.
			19.5 }	19.5 }			
2:11	14.9		25.5	28.5	.746	.50	
—	(20.1) 19.9		57.5	90.0	.33	.158	
2:30	22.0		112.5	199.0	.169	.1070	
2:35	23.4		345	663	.055	.021	stopped from #3
2:40	<del>24.0</del> 24.1		cut rod at 23 cm				Falling from #7
2:50	24.1		out rod at approx 28 cm				
	23.8		out rod out				

Conclusion: cut at  $24.0 \pm .1$  S.G  
corrected value for zero is 24.1

- #8 D.V. + 9.8 cm. = 9"
- #7 19.5 " " "
- #6 9 " " "
- #5 9 " " "
- #4 D.V. + 9.3
- #3 17.8 " "

zero correction: + 1.02 m. m.

(determined with tamper empty & top  
tamper out.)

Exp 327 (cont)

Summary:

CRITICAL AT SIGHT GLASS = 24.0 cm.

ZERO CORR. 0.1

BOTTOM CORR. 1.2

CRITICAL HEIGHT 25.3 cm

VOLUME 10.38 cc. ✓

~~MASS (10.38 x 1.12 x 0.993) = 1.1~~~~(10.38 x 0.993) = 1.00 g~~CRITICAL MASS.  $10.38 \times \frac{1.12}{1.00} \times 0.993 \times 93.3 = 1.04 \text{ g}$ 

H/x 240

1.04 g

28  
12/7/49

Exp 328

Macklin  
Fox  
Cromin

10" Al Reactor with 4 7/8" Al shells (empty) otherwise

completely tamped.

#X 237

Source at 16.8 on scale (10cm from bottom)

Instruments	starting	Trip
#3	X100	80 X100
#6	X25	6 X1000 (with BF <sub>3</sub> ion chamber)
#7	—	—
Process Monitor	—	—
#5	X1	—

Solution Inventory	B	C	D	E	F	G	H	J
10" cm	132	14.5	14.1	12.1	12.5	14.5	14.3	7.5

Since some water (from rinsing cyl) may be present - cyl J emptied into DV and drained back to avoid any spurious change in  $\frac{H}{X}$ .

Time	Sol'n Ht.	#1	#2	c/c	c/c	
2:25	7.4					cyl H
2:40		12.5	12.5			start G
	11.40	11.5	12.0			
2:52	19.8	32.5	45	.37	.267	stop rod #4
3:05	21.9	45.5	69	.264	.174	start F
3:15	25.0	95.5	158	.126	.076	
3:20	26.0	139	232.5	.086	.051	
3:30	27.0	244	418.5	.049	.029	
3:37	28.4	Critical with Rod 24cm out				
3:41	28.2	Critical Rod 28.5cm out				
3:44	27.95	Subcritical Rod out				

Critical at ~~27.8~~ 28.1 ± 0.1cm (Sight Glass Reading with rod out)  
Inventory Drain back - Same as above

SIGHT GLASS CRITICAL HT 28.1  
 .95  
 .60  
 Hc 29.6 cm  
 Vc 16,000 L ✓  
 Mc 1.57 ± .56 Kg.  
 H/X 240

Exp 329

12/8/49

10" A1 Reactor  $\frac{H}{X}$  n 239 6" Water Tamper. Top & Bottom Only!

Source at 10cm from bottom.

Instruments	Starting Scale	Trip Point
#3	100	84 X 100
#4	OUT	—
#5	1	—
#6	25	7 X 1000
#7	OUT	—
Process Monitor	(OK)	—

Time	Side HT.	#1	#2	c/c.	c/c.	Remarks
8:54	12.1	(50) 51	(42) 42	1.00	1.00	#8 MT at 7.4cm from #8/#7
		Waited for completion of Janitor Service				
9:30	20.0	81.	92.	.575	.457	#7 MT @ 22cm
9:47	26.0	134	159.5	.373	.264	MT #6 @ 33.8
9:57	34.5	227	312.	.220	.135	from #5.
10:12	42.0	525	820	.0950	.051	
10:14	CR In	~ 240	~ 300	~ .212	~ .14	Stopped # @ 43.4
10:14	47.4	Not Critical Est. crit 48.0				from #3
10:33	48.1	Not Critical New Est 48.8				
	48.6	" " 48.8				
	48.9	Super Critical (Vary slightly with rod out)				
At this point we drained back to 46.0 to see @ how high a power the counter would operate efficiently, in view of reflections, firing circuit, stop motor etc. The single result obtained is given below.						
10:57	46.0	1048	1175	.0477	.0358	
		↳ Extrapolate to 50.0		↳ Extrapolate to 55.6		

Conclusion: Critical @ 48.8 ± .1 cm on sight glass.

Bottom corr. .93  
 Fan corr. 1.07  
 —————  
 50.8 cm.  
 Hc corrected 50.1 cm.  
 Volume 25.4 L. ✓  
 Mc 2.65 kg X  
 H/X 240

30 12/8/49

Crosin  
Fox  
Morfell

#  
Exp 330

10" Aluminium Reactor - ~~2~~ Two empty  $\frac{7}{8}$ " shells (air) next to cylinder. Otherwise surrounded by water, in. Trip Tangs Trip Point, Instruments as in #329. Source @ 10cm from bottom.

Time	Hgt.	#1	#2	c/c <sub>o</sub>	g/c <sub>o</sub>	Remarks
12:48	12.0	9.0, 9.0	9.0, 9.0	1.0	1.0	#8 MT. from #7
1:03	18.0	18.0	20.5	.50	.44	
1:10	21.9	37.5	53.0	.24	.17	#7 MT
1:27	<del>22.7</del> 22.7	50.0	77.0	.18	.117	from #6
1:42	24.7	455	786.0	.0197	.0119	Est. Cr. @ 25.0
1:48	25.1					Prod @ 25 cm from bottom
1:51	24.9					Sub. Rod out

Conclusion critical @ 25.0 cm on scale.

Top corr. / 1.22"  
Bottom corr. / .93"  
27.15 cm.

Critical @ 25.0 cm on scale  
Top corr. .6  
Bottom Corr. .9  
Hc corr. 26.5 cm  
Volume 13.42L ✓  
Mc 1.40Kg  
M/x 240

12/8/49

Cronin  
Fox  
Hortiff

Exp #331

10" Aluminum Reactor. One empty 7/8" shell surrounding cylinders. Otherwise completely topped, including top tank. Trip Point, instrument as per #328. Source 10 cm from bottom.

Use background of Exp 330

Time	Hgt (12.0)	#1 (9.0)	#2 (9.0)	C/c. (1.0)	C/c. (1.0)	Remarks
2:07	17.3	15.5	17.5	.57	.515	From Exp 330 #8MT @ 7.2
2:16	20.0	33.5	48.0	.27	.187	Stopped #7
2:27	21.5	84.5	135.	.107	.067	From #3
2:33	22.6	Critical with rod @ 22				
2:37	22.4	Subcritical				

Conclusion @ 22.5 cm on scale

Solution Inventory same as Ex. 328

12/9/49 Filling of storage cyls M & N;

Cronin  
Fox

Filled reactor (10" al. to 24.5 cm) Emptying cyls. H & G - .4 cm out of F

cyl M: <sup>cm</sup> 26.5 at start	cyl N 14.2 at start
12.3 amt in cyl	12.3 amt in cyl
14.2 remaining	1.9 left

DV + 1.9 cm put back into H

Critical <del>22.5</del> on sight glass @	22.5
Zero Cor.	.6
Bottom Cor.	.9
<hr/>	<hr/>
24.65 cm	Corrected Hc 24.0 cm
	Vol 12.2 R. 12.16 ✓
	Mc. 1.27 kg X
	H/X 240



32  
11/12/49

in pit of  $\frac{4}{x} \cdot 239 = 33,777 \text{ cc} \equiv 66.75 \text{ cm in } 10'' \text{ cyl.}$   
 $\equiv 3.55 \text{ Kg X}$   
 $\equiv \text{~~3.80~~ Kg 4}$   
 in ea of 8 cyl = 8.34 cm  
 in set of 4 = 33.36 cm

to  $\frac{4}{x} \cdot 350$  total water required = 15.8 liters  
 for set of 4 = ~~1.94~~ liters  
 for 1 cyl = 1.94 liters

Distribution  
9-12-49

<del>17.6</del> <del>9.3</del> 8/3 into cyl #9	<del>19.1</del> <del>10.8</del> 8.3 into cyl #8	<del>19.1</del> <del>10.8</del> 8.3 into cyl #7	<del>21.4</del> <del>12.9</del> 8.5 into cyl #6
--	---	---	---

~~7.4~~

59.2 Reading	59.2	All cylinders, drawn in #9	
DI = 6.9	50.9	∴ 8.3 in #9	∴ drawn in #8
8) 66.75	42.6	∴ 8.3 " #8	" " #7
8.26	34.3	∴ 8.3 " #7	" " #6
	26.0	∴ 8.3 " #6	" " #5
	17.7	∴ 8.3 " #5	" " #4
	9.4	8.3 #4	
	1.1	8.3 #3	
	1.1 + DI	8.0 #2	

1.94 liters added to each sample for #2 which was 1.88 liters

9-13-49

Mixing

MT #2	} 17.8	1st Blowback (three right glass)			
MT #3		17.3	2nd	16.9	3rd
			16.6	Red and	16.55

Background counts

#1	#2	
48	34	} 40
52	37	
53	40	
49	41	

MT #4 28.7 (tamper chs.)

#1	#2	c/c <sub>1</sub>	c/c <sub>2</sub>
90	100	.53	.25

12/13/49

Exp 337

for 10" Al Cyl  $\frac{1}{4}$ " n  $35^{\circ}$  Untamped

Marklin  
Quoniam

Source 10cm from bottom

Instruments	start	trip
#3	x 100	78 x 100
#5	x 2	—
#6	x 50	6 x 1000
#7	—	8" from tube

G=50      G=40

Time	sol'n Ht	#1	#2	C <sub>1</sub>	C <sub>2</sub>	
1:35	28.7	90	100	.53	.28	.40
1:40	40.85	109	115	.459	.349	# 2, 3, 4, 5 MT
	46.5					from # 6
1:48	52.87	129	152	.39	.263	from # 7
2:05	58.7	142	180	.35	.22	from # 8
2:10	64.5	144	180	.35	.22	from # 9
2:20	50.1					into # 1
2:21	44.1					into # 2
2:23	38.1					into # 3
	32.0					into # 4
	26.0					into # 5
	40.82					from # 1
2:45	34.2					into # 9    6 cm total = 12 cm
	28.2					into # 8    6 cm total = 12 cm
2:47	22.2					into # 7
	16.2					into # 6
	12.2					into # 5

System <sup>apparently</sup> not critical untamped possibly critical at some large finite heights.

Solution showed no apparent inhomogeneity - using tamper as check on sol'n ht.

12/19/49

## Exp 333

40x

10" Al  $\frac{H}{x}$  m 350 completely tampedMachlin  
Gronim

Source at 10cm

Instrument	Start	Time
3	x 100	78 x 100
5	x 2	—
6	x 50	7 x 1000
7	—	8"

Time	Sol'n Ht.	#1	#2	c/c <sub>1</sub>	c/c <sub>2</sub>	
2:55	12.2	5, 5 } 5.0 5	4, 5 } 4.5 4.5			
3:25	16.0	7.0	7.5	.76	.60	from #2
3:30	18.3					#2 MT
3:38	22.0	21	31.5	.238	.143	from #3
3:50	24.0	88.0	146	.056	.03	from #4
3:55	24.8	Critical Rod at surface of sol'n				
3:58	24.6	Sub-Critical Rod out				

4:00

Critical at 24.7 cm  $\pm$  0.1cm sight glass reading only

## Solution Inventory

	#2	#3	#4	#5	#6	#7	#8	#9
cm in 10" cyl. =	24 + 6cm	12.3	12	10	12	12	12	12

H uncorrected 24.7

Zero correction + 0.6

Parallax Correction 0.9

26.2 cm.

Volume  $V_c$  13.3 R 13.27 ✓Mass ~~24.5 kg~~ 0.962 kg

H/x 352

Exp 338

12/14/49

10" AI  $\frac{H}{X}$  n 350 with 20  $\frac{1}{8}$ " layers of stainless steel also top lamp <sup>also top lamp</sup> surrounded by water

Machlin  
Callihan  
Crown

Source at 10 cm (=16.8 cm on scale).

Instruments	Start	Trip
3	x100	20 x100
5	x1	—
6	x25	7 x1000
7	—	4" from tube

Time	Sol'n Ht.	#1	#2	c/c <sub>1</sub>	c/c <sub>2</sub>	Notes
12:45	6.0 cm	4.25	5			} #2 MT front #3
1:00	12.0	4.25	5.5			
		4.5	5.0			
1:18	18.0	9.5	13.0	0.47	0.38	#3, MT, filling for #4.
25	21.1	16.0	24.0	0.28	0.21	
30	23.9	55.5	88.5	0.08	0.06	
37	25.2	CRIT. WITH 3cm C.R. in solution.				
40	25.0	Just CRITICAL.				
42	24.9	Sub critical.				

CRITICAL - SIGMA GLASS = 24 25.0 cm  
 Zen Corr. 0.40  
 Bottom Corr. 0.9  
 26.55 cm.  
 $V_c$  Volume 13.32 13.42 ✓  
 $M_c$  0.97 kg  
 $H/X$  352

Exp ~~337~~ 335

17/14/69  
RONIN  
MACCLIN  
CALLHAN.

10" AL. H/K = 350

Reflector: 6" Aero Top  
6" Aero Bottom  
2 1/2" S-seamless - sides. (No water inside).

Inserted safety rod to evaluate "back pond" count -

	H = 25.0	C <sub>0</sub>	C <sub>1</sub>	C <sub>2</sub>	C <sub>1</sub> / C <sub>2</sub>	C <sub>2</sub> / C <sub>0</sub>
1:55	H = 25.0	C <sub>0</sub> = 107	367	590	0.29	0.23
2:07	= 25.7	498	817	0.21	0.16	
:08	= 27.3					
:01	= 27.15					
:12	= 27.0					

Slightly super crit.  
" Sub critical

SIGHT GLASS AT CRITICAL = 27.1 cm.  
Drainback: Zen Bottom corr. 0.4  
cyl #2 #3 #4 Bottom corr. 0.9  
24+6w 12cm 12cm 28.4 cm

Machine  
Crown

Zero Determination	sight glass	Reactor
without water in tank but with 2 1/2" of stainless	- 0.4 cm	zero
with water in tank 6" deep plus steel	- 0.4 cm	zero
with water in tank 3ft deep plus steel	- 0.6 cm	zero.

CRIT. H<sub>T</sub> = 28.4 cm  
Vol = 14.4 L. 14.39 ✓  
M<sub>c</sub> 1.04 Kg  
H/K 352

12/15/49

Exp 336

CRONIX

10" Al  $\frac{H}{x}$  350

MACLEIN  
CALLINAN

Reflector: 2 1/2" stainless - sides, no top or bottom lamper.

Source at 16.8 on scale. (= 10 cm above reactor bottom).

Instruments	Start	Trip Points
# 3	x100	30 x 100
# 5	x1	—
# 6	x25	7 x 1000
# 7	—	4" from tube

Time	Sol'n Ht.	#1	#2	c/c <sub>1</sub>	c/c <sub>2</sub>	
12:00	12.2 cm	38 <del>37</del> 37	41 <del>42</del> 41			*2 empty at 6.0 cm; Filling <sup>for</sup> #3
		(37)	(41)			
12:15	17.9	61.0	71.5	0.61	0.57	*3 Empty; Filling for #4.
21	23.0	107.0	141	0.35	0.29	
27	27.0	185	296	0.19	0.14	
35	30.2	260	420	0.07	0.04	*4 MT; from #5
43	31.7	Sub critical.				
47	32.2	Super Crit. (Rod at 22.5 at ~ crit).				
48	32.0	" " ( " " 27. " " )				
49	31.85	" " ( " " 30 " " )				
50	31.75	Sub crit, rod out.				

SIGHT GLASS AT CRITICAL: 31.8 cm  
 Zero corrected 0.4  
 Bottom Correction 0.9  
 33.1 cm  
 Volume 16.88. ✓  
 1.22 kg  
 H/x 352

Exp 337

12/15/49  
MORFITT  
MACKLIN  
CRONIN  
CALLIHAN

10" Al  $\frac{H}{X}$  n 350

Reflector = 1/2" Stainless steel surrounded by water

Source at 16.8 on scale (10 cm from reactor bottom)

Instruments	Scaling	Trig
# 3	X100	80 X 100
# 5	X1	—
# 6	X100	7 X 1000
# 7 —	—	4" from tube

Back Background assumed to be 5 for both counts from Exp 333

Time	sol'n Ht.	#1	#2	g/c	c/c <sub>2</sub>
2:00	17.9 cm.	4.25	6.0		
		4.25 (10)	5.0	VOID	
		4.3	5.5		
2:05	25.1	26.0	45.5	.165	.121
	25.1	34.0	55	0.15	0.09
2:25	25.9	65	110	0.08	0.05
33	27.0	SUPER CRIT - ROD OUT			
34	26.7	SUPER CRIT - - -			

Filling from 4 } Source irregular placed

CRITICAL AT SIGHT GLASS = 26.9 cm -  
Zen correction 0.6  
Bottom correction .9

Volume. 28.4 cm.  
14.4 L. 14.39 ✓  
1.04 kg  
H/X 352

INVENTORY: 1 - Empty.  
at end of day 2 - DV + 6 cm in 10" reactor  
Mif 49 3 - 12 cm  
4 - 12 cm  
5 - 10 cm  
6 - 12 cm  
7 - 12 cm } See pg 34  
8 - 12 cm  
9 - 12 cm

12/12/49

Exp 338

10" Al - H/x = 350 -

Reflector - Sides - 1 1/2" Stainless  
Top & Bottom - 6" H2O.

MORFITT  
MACKLIN  
CRONIN  
CALLINAN.

Source - 16.8 cm n. scale = 10 cm above reflector bottom.

Back-ground assumed from Exp 336 C<sub>1</sub> = 37, C<sub>2</sub> = 41

	H	C <sub>1</sub>	C <sub>2</sub>	M <sub>1</sub> <sup>-1</sup>	M <sub>2</sub> <sup>-1</sup>
2:50 P	26.9	243	361	0.15	0.11
	28.0	326	500	0.11	0.08
3:05	29.5	538	853	0.07	0.05
15	31.8	Super cut (critical rod = 28.5)			
17	31.6	Sub cut Rod cut -			

Filling from 4.

Stop from 4, filling from 5

CRITICAL AT SIGHT GLASS = 31.7 cm -

Zen correction 0.4

Bottom correction 0.9

33.0 cm

Volume 16.7 d. ✓

121 kg.

H/x 352



40

17/15/49

Exp 339

MACKLIN  
MORFITT  
CRONIN  
CALLIHAN.

10" OD - H/K = 350

Reflector - 1 1/2" stainless on sides -

No water, top, bottom or sides -

Sample at 16.8 cm - (10 cm above reactor bottom).

Background - from #338  $C_1 = 37$ ;  $C_2 = 41$ .

	H	$C_1$	$C_2$	$M_1^?$	$M_2^?$
3:20 P	H = 31.6 cm	444	687	0.08	0.06
26	= 33.0	566	894	0.07	0.05
* 45	= 36.0	Apparently just critical.			
52	= 36.1	Slightly super crit.			

from #5

CRITICAL AT SIGHT GLASS = 36.0 cm.

Bottom corr. 0.9

Zero corr. 0.4

37.3 cm  
Volume 18.9 l ✓  
 $M_c$  1.37 kg x  
H/K 352

\* During this interval it was noted that level on #5 Reader chart showed slow decrease in level during 3:26 count and during the preceding interval when reactivity was astonishingly constant. This was first attributed to a leaky cylindrical valve allowing slow drain back - but could not be conclusively shown to be this - no other cause was apparent since during the period after insertion of control rods<sup>at 3:25</sup> the level was constant. #6 chart did not show the same action.

17/16/49

Spgr. 1.114 @ 20°C. 2 Samples were taken 9 AM.

Tag #  
830069  
830070

Sample #  
339A  
339B

INVENTORY -  
See pg #339

Verbal Report on 830069 0.069 g/g sol.

12/16/49

Exp 340

Callihan 10" Al H/X ~ 350 Reflector 3/4" stainless on sides  
 Cronin water on sides, top & bottom.  
 Martlett

14.8  
 Source @ ~~14.8~~ cm. 8 cm from bottom

Backgrounds for next sequence of exp

	No water	6" Water + Top Taper	Completely Tapered
#1 Counts	33.5, 33.5	36.5, 34.5 <del>33.8</del> , <del>34.9</del>	3.5, 4.0 (3.75)
#2 Counts	30.5, 33.0	31.0, 32.0	3.5, 4.0 (3.75)

Instrument	Starting Scale	Taps @
#3	100	8 x 1000
#4	NG	NG
#5	2	—
#6	25	8 x 1000
#7 (Plate M-1)	—	.6 m
#8 (Proc. Mem.)	— (2)	— (2)

Time	Height	#1 Counts	#2 Counts	1/M <sub>1</sub>	1/M <sub>2</sub>	Remarks
11:10	10.8	See above	Begin measurements	1.0	1.0	#2 M7 @ 5.7 from #3 & 4
11:48	18.7	7.0	9.5	.53	.40	#4 MTC @ 17.5
12:00	24.2	13.5	21.0, 23.0	.28	.18	from #6 stopped #6
12:10	27.0	27.5	49.5	.137	.076	Stopped #6
12:20	29.0	190.	351.	.031	.007	from #8
12:30	29.4 Rod	27.0 cm off bottom	Slightly super critical @ 29.4 cm			
12:32	29.1	Subcritical with rod out. Close to criticality have the above.				

Conclusion Critical @ 29.2 cm.  
 Zen Correction 0.6 cm  
 Bottom Correction 0.9  
 30.7 cm  
 Volume 15.6 L. ✓  
 1.13 Kg X  
 H/X 352

42 12/16/49

Exp 341

Callahan  
Crown  
Hans  
Moffitt

10" Al  $\frac{1}{2}$  - <sup>352</sup>329 Reflector  $\frac{3}{4}$ " stainless steel +

6" water Top + Bottom only."

Source + Treatment same as #340

See #340 for background readings Using 33.5 for both counts.

Time	Hgt	#1 Counter	#2 Counter	$\frac{1}{M_1}$	$\frac{1}{M_2}$	Remarks
1:38	29.4	150.0	204.5	.223	.164	From #6
1:43	32.1	196.0	288.0	.171	.116	*647 @ 32.5
1:52	37.1	406	665	.082	.050	From #9
2:07	39.3	738	1050	.045	.032	
	Rod is Temp up.	225	322	.15	.104	Stopped #9
2:30	41.3	Not Critical				From #7
	41.9	Not critical				
	42.3	Super critical with rod @ 39 cm from bottom				
	42.1	" " " " @ 45 " "				

Conclusion: Critical with sight glass @ 42.0 cm.  
 Zero corr. 0.4 cm  
 Bottom corr. 0.9  
 43.3 cm  
 Vol 21.9 L. ✓  
 1.59 kg  
 H/K 352

12/16/49

43

## Experiment 342

Callihan  
Crown  
Henry  
Mortfit

10" Al  $\frac{1}{2}$ " 359 Reflector  $\frac{3}{4}$ " stainless steel 8 mm wall.  
 Instruments & Scale same as #340  
 Background 33.5 cm for both counters.

Time	Hgt	#1 Counter	#2 Counter	$\frac{1}{M_1}$	$\frac{1}{M_2}$	Remarks
2:58	42.1	436	713.5	.077	.047	from #7
3:08	45.15	901	875.	.037	.038	
3:15	Rod in	300 282	NG	.111	Rd vert. 1.9 cm.	
3:25	46.9	Not critical				
3:27	48.1*	Critical with rod @ 37 cm.				
3:29	47.9*	" " " " 40 cm				
3:30	47.7*	" " " " 42				
3:31	47.5*					
3:32	47.4					
3:33	47.3					

Critical @ 47.35 cm  
 Zero corr. 0.4  
 Bottom corr 0.9  
 Corrected Ht. 48.65 cm  
 Vol 24.62 ✓  
 mass 1.7829  
 $\frac{1}{M}$  352

\* Reading taken with rod at hgt shown.

44  
 Edwin  
 Callahan  
 Flora (Hartford)  
 Fox  
 Henry  
 Morrell

1/19/49

Exp 343

10" Aluminum Reactor. Reflector  $\frac{1}{2}$ " stainless steel +  
 Water side Top & Bottom.

Inst. Trip #s  
 3 84 x 100  
 5 7 x 1000  
 6 3" from source  
 7

Background for next experiment. Source @ 6.8 cm.

Inventory  
 2 = DV + 6 cm  
 3 = 12  
 4 = 12  
 5 = 10  
 6 = 12  
 7 = 12  
 9 = 12  
 7 = 10

	#1	#2	Source @
Fully tamped + S.S.	3 3/4, 3 3/4	4, 4 1/4	10 cm from bottom
Top & Bottom tamped + S.S.	39.5, 38	34, 35	10 cm from bottom
S.S. Reflector only	dry 39	wy 34.5	10 cm from bottom

Time	Hgt	#1	#2	1/4"	1/8"	Remarks
10:15	11.9	37.5	4.0	1.0	1.0	#2 at 5.5
10:40						from #3 MT 17.3
70%	19.9	7.5	11.5	.46	.35	from #4
10:50	23.4	11.5	19.5	.33	.205	
11:00	28.0	38.0 36.5 34.5	67.0	.102	.06	stopped #4
11:17	29.0	86	15%	.04	.026	from #5
11:28	30.0		critical			Rod at 50 cm from bottom
11:35	29.8		critical			Rod out tamped down.
11:40	29.6		Sub-critical			

Critical at 29.8 sight glass

corn bottom .90  
 zero .6

0.1.3 cm.  
 $V_c$  15.9 L ✓  
 $M_c$  1.15 kg  
 $H/K$  352

7123

Callahan  
Moffitt  
Top  
from  
Ocean

Ex. 344

10" A1 1/2" stainless steel 6" water Top and Bottom

Source at 10 cm from bottom

Inst. same as Ex. 343 #1 #2  
background = 39 34.5

Time	Ht.	#1	#2	1/n <sub>1</sub>	1/n <sub>2</sub>	Remarks.
12:05	29.8 cm	138	170	.283	.204	from #5
12:10	33.9	178	240	.219	.144	stopped at #5 - start #6.
12:25	40.0	290	443	0.13	0.08	Stop for #6
:35	45.0	542	880	$\frac{0.07}{0.05}$	0.04	Stop for #6, start for #7
:45	50.0	Solo critical -				
:50	51.0	Seyar cut (cut rod at 50 cm).				
:53	50.6 -	Sub cut.				

CRITICAL - SIGHT GLASS = 50.8 cm -

Photo counter 0.9

Zero - 0.4

CRITICAL HEIGHT 52.1 cm

Critical Vol. 26.42 l ✓

M<sub>c</sub> 1.91

H/X 352

46  
17/19/49

Exp 34J

Henry  
Morfitt  
Flora  
Joy  
Calkin

10" Al Receiver - 1176 ~ 350 - 1/2" 1/2" Standard  
Steel Reflector - as with.

Temp pts etc same as + 343

Background: #1 39  
#2 34.5

	H = 78.2 cm -	C <sub>v</sub>	C <sub>v</sub>	#1 M <sup>7</sup>	#2	
3:15 P		102	126			
		<u>101</u>	<u>127</u>	0.38	0.27	Filling #5-
1:25	= 38.3.	186	207	0.21	0.13	#5 MT; Filling #6.
20	= 45.9	321	309	0.12	0.07	
	= 50.0					#6 MT; Filling #7-
	= 55.4					
50	= 56.3					
55	= 57.2					
	57.6					

Sub critical -

almost critical -

Super crit. rod out. (crit. rod at 54 cm from bottom).

CRITICAL - SIGHT GLASS = 57.4 cm.

Bottom Connector = 0.9

Zero Correction = 0.4

58.7 cm.

Vol. 29.7 d. ✓

M<sub>c</sub> 2.15

H/x 352

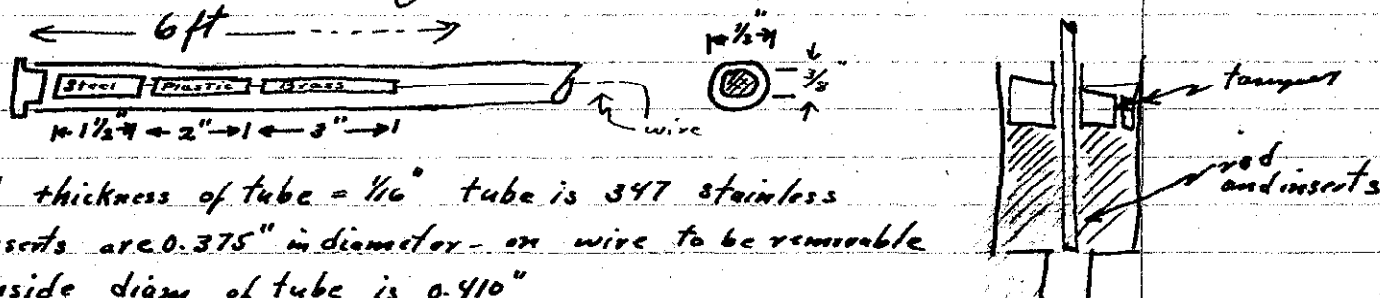
- INVENTORY - 1-MT  
2 - DV + bin in 10' cap.  
3 11.9  
4 12  
5 12  
6 12 cm  
7 12 cm  
8 12 cm  
9 12 cm

Cronin 12/21/49  
 Flora  
 Fox  
 Merrill

Experiment 346

10" Al Reactor  $H/K \approx 350$  Completely Tamped Special Fitting

Purpose: To evaluate magnitude of perturbation introduced into proposed Hartford Reactor by recirculant source guide tube.



wall thickness of tube =  $1/16$ " tube is 347 stainless  
 inserts are 0.375" in diameter - on wire to be removable  
 inside diam of tube is 0.410"  
 plug at end is silver soldered in.

Tube held up by Safety Rod Magnet (replacing Cd rod) zero of rod = 18.5 cm scale  
 Part A Rod tube completely out. usual fully tamped as Ex 333

Time	Solv Ht.	#1	#2	$1/M_1$	$1/M_2$	Remarks
1:42	9.9	40	40	1.0	1.0	#2 HT @ 5.9 cm
1:57	20.0	13.0	18.0	.308	.22	#3 HT @ 17.4 cm
2:10	23.1	37.0	61.0	.108	.066	from #4
	24.7	Critical Rod at 20 cm				
	24.6	" " " 23 cm				H sight glass 24.4
	24.5	" " " 25.5				Zero corr. 40.6
	24.3	Sub-Critical Rod out				Bottom Cor. 0.9
						Hc 25.9 cm
						Vc 13.1 L
						Mc .93 L

Critical at 24.4 cm on sight glass

Part B

with special tube and Insert in Reactor. (bottom of tube at bottom of reactor)

2:40	24.3+	59.5	105	.067	.038	Tube plus insert
2:50	24.3	71	124	.056	.032	tube in - insert out
3:10	25.05	Critical Rod at 27 cm				
3:05	24.9	Sub Critical Rod out				
		Critical at 25.0 $\pm$ 0.1 cm on sight glass				
3:15	24.9	Sub-Critical				INSERT Back in tube
	25.05	Critical Rod at 25				
		Critical at 25.0 $\pm$ 0.1 cm on sight glass				

Drainback same as Ex. 345

Hc sight glass	25.0
Zero corr	4.6
Bottom corr.	0.9
Hc	26.5 cm
Vc	13.42 + 13.42
Mc	0.97
H/K	352



48  
Crown  
Flora  
Fox  
Mortitt  
12/23/49

Experiment #347

H/X 350

10" Aluminium Reactor - 4 7/8" shells of  $UO_2(NO_3)_2$

as side reflector. No top or bottom reflector.

Source 10 cm from bottom 16.8 on scale.

Instruments	Set at	trip at
#3	10	78 x 100
#4	NG	—
#5	#1	—
#6	#25	.7 x 1000
#7	—	6" @ 7

Background

Time	Soln Ht.	#1	#2	$1/M_1$	$1/M_2$	Remarks	
9:49	12.2	26.25, 26.25	27.0	27.5	1.0	1.0	from #2 MTS.8
9:57	18.1	47	49.5	.55	.55	#3 MT	
10:05	23.0	81.5	100	.32	.275	from #4	
10:22	26.0	137	184	.19	.147	stopped #4	
10:32	28.0	230	332	.113	.081	from #5	
10:45	30.0	843	1061	.03	.025		
10:58	31.0	Critical at 25 cm Rod from reactor bottom					
	30.8	Slightly super critical					
	30.7	slightly sub-critical					

System Critical at 30.75 cm on sight glass.

Zero Corr. 0.4

Bottom Corr. 0.9

$H_c = 32.05$  cm

$V_c = 16.2$  L ✓

$M_c = 1.17$  KgX

H/X 352

12/23/49

Exp. 348

Crown  
Flora  
Fox  
Henry  
Mortill

10" Al Reactor

2 shells of  $UO_2(NO_3)_2$ 

as side reflector no top or bottom reflector

Source 10 cm from bottom 16.8 on scale

Trip pts. same as #347

Background = same as exp. #347

Time	Solu. Ht.	#1	#2	$M_1$	$M_2$	Remarks
1:25	17.6	64.5 <del>32</del> 64.5	61.61	<del>0.403</del> .403	<del>0.44</del> .44	#4 empty @ 26.5
1:40	27.8	188	246	<del>0.139</del> .139	.109	
1:50	31.1	357	509	.073	.053	
	31.1	Rod in 241	306	.108	.088	
2:02	32.1	618	912	.042	.030	
2:13	34.0	Subcritical w/ rod out.				
2:17	34.5	"	"	"	"	(slightly)
2:20	34.95	Critical w/ rod at 30 cm.				
2:22	34.6	Subcritical w/ rod out				
2:23	34.75	"	"	"	"	

System critical at 34.95 cm. on sightglass.

Sight Glass 34.85

Zero Correction 0.4

Rod in Cor. 0.9

$$H_c = 36.15 \text{ cm}$$

$$V_c = 18.3 \text{ dl. } \checkmark$$

$$M_c = 1.33 \text{ kg X}$$

$$H/X = 352$$

50 12/18/49

H/k  $\infty$   
350#  
Exp 349Crown  
Fox  
Mortill10" Aluminum Reactor 1 shell of  $UO_2(NO_3)_2$   
as side reflector. No top or bottom reflector. conc.  
Source 13 cm from bottom 19.8 cm scale.

Instrument	Original Setting	Trips @
3	20	80 x 100
4	NG	—
5	1	—
6	50	.8 x 1000
7	—	.6 1

Time	Soln. Hgt.	#1	#2	$1/M_1$	$1/M_2$	Remarks.
11:48	15.2	50	41.5	1.0	1.0	#2 MT @ 6.5
11:57	25.1	117	124	.43	.33	#3 MT @ 20.
12:03	30.1	178	203	.28	.205	#4 MT @ 29
12:14	37.9	390	536	.128	.08	from #5
12:20	42.9	1004, 1024	857, 854			#5 MT @ 40.7
Rod in	42.9 +	408	448			
12:25	46.4					Critical with rod @ 37.0
12:30	<del>46.0</del> 46.0					Critical with rod @ 40.
12:31	45.8 <del>46.8</del>					Just Critical Rod out
12:32	45.65					Subcritical.

Conclusion. Critical @ 45.8 cm on sight glass  
 Zero Corr. 0.4  
 Bottom corr. 0.9  
 Drainage as above 47.1 cm

$$H_c = 47.1 \text{ cm.}$$

$$V_c = 23.9 \quad \checkmark$$

$$M_c = 1.73 \text{ kg X}$$

$$H/k = 352$$

M. S. Gordon  
for  
Cromin

Exp #350

~~11/1/51~~10" Aluminum Reactor 1 shell of  $UO_2$  ( $Al_2O_3$ ) as side reflectorThe concentration is approximately  $1/2$  that of the previous experiment. No top or bottom reflector.

Source at 10 cm from bottom

Instruments	starting	Trips
3	x 20	80 x 100
4	NG	—
5	x 1	—
6	x 25	5.5 x 1000
7	—	4" from tube ( $1/2$ mg source)

Time	Sol'n	# 1	# 2	$\frac{1}{M_1}$	$\frac{1}{M_2}$	
9:00	12040	39.5 41.0 39.5	39.5 33.0 35.5			#2 MT at 6 cm
9:15	18.0	66.5	58	.60	.58	#3 MT at 17 cm
9:30	28.5	151.0	169	.26	.20	#4 M at 29.1
9:38	34.0	253	318	.16	.11	from #5
9:55	40.0	691	992	.058	.034	"
10:00	40.00	334	431	.12	.079	Control Rod in
10:12	43.7	Critical	Rod at 34 cm			from #6
10:13	43.5	Critical	Rod at 39			
10:14	43.3	Sub critical				

Critical at 43.4 cm  $\pm$  0.1 cm on sight glass

Drain back into cylinder as taken out.

Sight glass 43.4 cm

Zero Corr. 0.4

Bottom Corr. 0.9

 $H_c = 44.7$  cm $V_c = 22.4$  ✓ $M_c = 1.64$  $H/\lambda = 352$

52

McLendon  
Corwin  
Fox

Expt 351

 $H/X \approx 350$ 

10" AL Reactor

2-1" shell of  $UO_2(NO_3)_2$ 

@ ~ 12% conc.

no other reflectors

Source at 10cm

Starting scales #6-25; #5-1; #3-20

Time

Time	Ht	$C_1$	$C_2$	$1/C_1$	$1/C_2$	#2 Empty at 6.6m
<del>1:25</del>	12.2	32.0 } 31.5 31.0 }	38.0 } 38.5 39.0 }			
1:35	17.6	59.0	69.5	.53	.55	3 Empty at 17.0
1:40	23.0	107.0	134.5	.295	.285	
1:48	26.9	192.5	239	.22	.16	
1:55	"	182.0	242	.173	.16	
2:00	31.0	424	592	.074	.065	
	" rod in	271	358	<del>.108</del> .108	.114	
2:13	34.5	cut. rod at 33				
	34.3	sub. cut with rod out				

Conclusion: cut at  $34.4 \pm .05$ Drumstick ~~is~~ as filled

Sight Glass	34.4 cm
Zero Correction	0.4
Bottom Corrected	0.9
$H_c$	35.7 cm
$V_c$	18.1 l ✓
$M_c$	1.31 Kg X
$H/X$	352

Fox  
McLendon  
Crosier

Exp. 352

10" Al Reactor with 4 shells of  $UO_2(NO_3)_2$  @ 12% conc

no other reflector

Starting conditions same as Ex 351

Time	Ht	#1	#2	$\frac{1}{M_1}$	$\frac{1}{M_2}$	
3:05	10.9	25.0	23.0			
<del>3:10</del>	<del>18.2</del>	26.0	23.5			
3:20	18.2	46	41.5	.55	.50	#3 MT at 17.0
3:27	24.0	89	74	.28	.25	
3:30	26.0	125	144	<del>.20</del>	.19	Stopped #4
3:40	29.1	295	376	.20	.062	From #6
3:45	31.5	Critical Rod at 25 cm		.086		" " "
3:46	31.3	" " " 29 "				into #6
3:47	31.1	Sub Critical Rod out				

Critical at 31.2 ± 0.1 cm (sight glass reading)

Drain back same as taken out.

Sight Glass	31.2 cm
Zero Correction	0.4
Bottom Corr.	0.9
$H_c$	32.5 cm
$V_c$	14.5 L ✓
$M_c$	1.20 kg ✓
H/X	352

12/30/49

Expt 353  $H/X \approx 359$

10" AL Reactor

1 shell of H<sub>2</sub>O temper

Fox

No top or bottom reflector.

Henry  
Crown  
Mortiff

Imp points: PM - 5" ; #3 - 85 ; #6 - 6 on LN  
(16.8 on scale)

Source at 10 cm. Starting scales - most sensitive

Time.

Time	HV	C <sub>1</sub>	C <sub>2</sub>	C <sub>10</sub> /C <sub>1</sub>	C <sub>20</sub> /C <sub>2</sub>	Remarks
12:46 PM	12.2 cm	49.5 } 49.5 49.5	36.5 } 36.5 36.5			#2 empty at 6.0 #3 " at 16.9
12:56 PM	17.9 "	81.0	63.0	.61	.58	
1:02 "	23.9 "	131.0	117.0	.38	.31	
1:10 "	27.9	177.0	173.0	.28	.21	#4 " at 29.3
1:17	36.0	436.0	489.0	.11	.075	#5 stopped at 38.
1:35	40.0	1019.	1035	.049	.035	
1:40	40.0 (Rod in)	433.0	479.0	.11	.076	
1:53	42.5	super critical; critical withdrawal at 38.0				
	43.1	"	"	"	"	35.0 at 38.0
	42.8	"	"	"	"	38.0
	42.5	sub-critical				

Conclusion: Critical at 42.6 cm ± 0.1 mm

Drain: Into #5 D 38.0  
" #5 " 29.3  
" #4 " 17.5

Sight Glass 42.6 cm.  
Zero Corr. 0.4  
Bottom Corr. 0.9  
H<sub>c</sub> 43.9 cm  
V<sub>c</sub> 22.2 L ✓  
M<sub>c</sub> 1.61 kg  
H/X 352

$$\frac{H}{X} \approx 350$$

12/30/49

Exp. 354

Henry  
Modified  
Crosbie

10" Al Reactor 2 shells of H<sub>2</sub>O no other tamper top or bottom  
Starting conditions same as Exp. 353

Time	Ht.	1	2	$c_{10}/c_1$	$c_{20}/c_2$	Remarks	
2:20	11.8	37.5 } 37.5 } 37.5	32.5 } 33.0 } 32.5			#2 M.T. #3 M.T. @ 13.5	
2:36	20.1	95.0	81.0	.395	.40		
2:47	25.0	167	161	.22	.20		
2:56	30.0	396	432	.095	.075	#4 M.T. @ 29.4	
3:05	32.4	990	1093	.038	.030		
3:06	34.2	Critical Rod at 28cm					
3:15	34.0	Critical with rod out.					
3:16	33.95	Subcritical with rod out					

Conclusion: Critical @ 34.0 cm ± 0.05 in quartz glass.

- Zero Corr. 0.4
- Bottom Corr. 0.9
- Hc 35.3 cm
- Vc 17.9 f ✓
- Mc 1.30 Kg
- H/X 352



Henry  
Mofitt  
Crosier

12/30/49

Exp. ~~358~~ 355

10" Al Reactor 4 shell of water no other temper  
Starting conditions same as Ex. 353

Time	Ht	#1	#2	$\frac{1}{m_1}$	$\frac{1}{m_2}$	
3:30	13.1	31 } 30 29 }	27 } 26.5 26 }			
3:40	25.0	138	131	.222	.20	413 107 317.0
3:45	28.1	281	289	.107	.092	stopped #4
3:50	31.0	Sub critical Rod out.				
4:00	31.7	Critical Rod 29.5 cm				
	31.6	Critical Rod at 31 cm				
	<del>31.3</del>	Critical Rod at 32				
	31.1	Sub critical Rod out				

Critical at 31.2 ± 0.1 cm on sight glass.

Drainback -

#5 #4 #3 #2  
12cm 11cm 12cm

Sight Glass 31.2 cm.  
Zero corr. 0.4  
Bottom corr. 0.9  
Hc 32.5 cm  
Vc 16.5 Z ✓  
Mc 1.20 kg  
HX 352

1/4/50

W. Landon  
Moffitt  
Gross

Exp 356

15" Al Reactor H/X = 359 completely water topped

Source at 5 cm (11.8 on scale)

Instruments	Trip	Start
3	80 x 100	x 10
5	—	x 2
6	5.6 x 1000	x 25
7	4" -	4" from tube

Inventory	#2	#3	#4	#5	#6	#7	#8	#9
	21.3	5.3	4.9	5.3	5.3	5.3	5.3	5.3

Time	Ht	#1	#2	$\frac{1}{M_1}$	$\frac{1}{M_2}$	
10:30	6.0	4.0 any	3.5 any	1.0	1.0	#2 MT @ 3.3
10:50	10.0	6.5	7.5	.61	.46	#3 MT @ 7.5
11:00	12.5	12.5	17.0	.32	.21	#4 MT @ 12.6
11:09	14.3	3.5	77.0	.092	.075	from #5
11:20	15.0	Supercritical with Temp 5 mm.				
11:22	14.9	" " " 3 mm.				
11:24	14.8	Subcritical				

Critical @ 14.85 ± .05 cm. on sight glass  
 Zero corr. - .8  
 Bottom corr.

Sight Glass Ht.	14.85	14.85
zero	+ .8	- .8
Bottom	- .9	+ .4
	<hr/>	<hr/>
	14.35	14.45
Hc	14.85	
Vc	17.0	14.57 ✓
		Mc 1.20
		H/X 352

58  
1/4/50

Exp 357

Crossin  
McLendon  
Hortill

15" Aluminum Reactor H/X = 359 No reflector  
Source @ 14.8 8 cm from bottom.

Instruments & Inventory as per 356

Time	Hgt.	#1 as 120 10.0, 10.5	#2 25, 26	$1/4_1$ 1.0	$1/4_2$ 1.0	Remarks	
12:10	10.1					243 M.T. 4 M.T. @ 12.8	
12:17	19.2	(10.0)	(25.3)			SMT @ 19.2	
12:20	19.2	50.5	109	.208	.234		
Lunch							
1:20	21.1	86.5	184	.13	.14	From #6	
Red in		70	158	.165	.162		
1:31	23.0	171	445	.061	.057	Stopped #6	
1:37	23.9	334	943	.030	.027		
		180	500				
1:42	25.0	Rod @ 16.0					
1:44	24.9	" @ 17.5					
	24.8	" @ 19.0					
1:46	24.65	Critical with rod out.					

Conclusion: Critical @ 24.65 on sight glass.

Solution zero measured on drain back

Solu zero @ 10 cm on page. Temperature empty.

Boiling correction 2mm.

∴ Solu zero @ 0.8 cm. Temp tank full.

sight gl. ht.	24.65
zero	-1.00
bottom	+1.4
Hc	<u>24.05</u>
Vc	27.4 ✓
Mc	1.99 Kg
H/X	352 ✓

1/4/50

Crosini  
McDonald  
Merfield

Exp 358

9" Aluminum Reactor H/X = 359 Complete Taper  
Source @ 17.5 10 cm from bottom. Trip Points as per 356

Inventory	#1	#3	#4	#5	#6	#7	#8	#9
	20.74	14.5	13.5	14.5	14.5	14.5	14.5	14.5
Time	Hgt.	#1	#2	#3	#4	#5	#6	REMARKS
3:20	22.7 (temp at 7.1)	10	3.5, 4					#2 MT at 7.4
3:40	21.6	18	9.5		.55	.4		#3 MT at 18.5
3:46	26.7	31	16.5		.32	.23		#4
3:52	33.0	227	13.6		.094	.028		#4 MT
4:04	34.3	Critical Rod at 29 cm						#5
4:06	34.1	Critical Rod at 31.						into #5
4:10	33.9	Critical Rod at 46						into #5
4:12	33.7	Sub Critical Rod out						into #5

Critical at 33.8 ± 0.1 cm

Drain back as taken out.

Sight Glass reads + 0.2 cm.  
at zero with empty taper tank

sight glass Ht 33.8  
zero 0  
Bottom 1.2  
Hc 35.0  
Vc 14.30 ✓  
Mc 1.04 Kg  
#/X 352 ✓

60 1/6/50

Exp # 359

Crown  
McHardow  
Morfitt

12" Aluminum Cylinder Tamped H/x = 359

Source @ 15.5 cm from bottom.

Instrument	Trip	Start
3	80X100	X10
4	NG	—
5	—	X2
6	6X1000	X25
7	.73	—

Inventory

#2

DV + 4.2

#3	#4	#5	#6	#7	#8	#9
8.2	7.5	8.2	8.2	8.2	8.2	8.2

Time

10:37

Hght. 10.0

#1 5.0, 4.5  
#2 4.5, 4.0  
1/M 1.0  
1/2 1.0

Remarks 2MT, #3 MT @ 10.0

10:55

15.0

(4.75) 14.0  
(4.25) 18.5  
.34 .235

from #4

11:03

16.6

36.5 50.0  
.13 .085

stopped #4 Est Cr: 17.5

11:13

17.9

Critical with rod @ 12.0

11:17

17.7

Super Critical, rod @ 15.0

11:20

17.5

" " " 21.5

11:24

17.45

Subcritical with rod out

Conclusion Critical @ 17.50 cm on sight glass  
zero cor.  
Bottom

$$H_c = \frac{1.25 + .6}{19.35}$$

$$V_c = 14.12 \checkmark$$

$$M_c = 1.02$$

$$H/x = 352$$

1/5/50

Crown  
McLendon  
Mortier

Exp. # 360

61

H/K 359

12" Aluminum Cylinder Untamped  
Source & Instruments as per #359

Time	Soln.	C <sub>1</sub>	C <sub>2</sub>	1/M <sub>1</sub>	1/M <sub>2</sub>	
11:30	17.8	45.5	59	1.0	1.0	Nominal BG
11:34	20.0	60	78	.75	.75	from #5
11:42	25.0	105	162	.43	.365	MT'd #4
11:50	28.6	176	294.5	.26	.20	emptied #5
12:00	32.0	378	696	.12	.085	
	Rod in	220	370	.21	.16	
	35.0	Subcritical				
	35.4	Super critical rod				
	35.2	Critical with rod out.				
	35.1 +	Subcritical				

Conclusion: Critical @ 35.2

#1	#2	#3	#4	#5	#6	#7	#8	#9
MT	DV	8.0 cm	8.0 cm	8.0 cm	8.0 cm	8.5 cm	8.0 cm	7.8 cm

Boyc correction 3mm.

right glass Ht 35.2  
 zero cm. ~~1.25~~  
 Bottom 11 .0  


---

 Hc 37.05  
 36.8  
 Vc 27.0 ✓  
 26.8 ✓  
 Mc 194 Kg  
 H/K 352

Wgt. of  $\text{Bi}_2\text{O}_3 \cdot \text{CO}_2$  in shells

Shell	Tare	Gross	Net
18A	19.0	<del>68.0</del> 68.0	<del>49.0</del>
18B	19.0	<del>68.5</del> 68.5	<del>49.5</del> 49.5

No shell

Cross Section area  $\text{cm}^2$ 

10A + 10B

197  $\text{cm}^2$ 

12A + 12B

233

14A + 14B

268.5

16A + 16B

302

18A + 18B

817. ~~817~~

} See p 97 Book 28.

"OD" 22  $\frac{1}{8}$ " "ID" 18  $\frac{3}{4}$ " Thickness 3  $\frac{7}{8}$ "  
 Actual Measurements. Not from print.  
 Corrected for wall thickness.

1/6/50

Crosby  
McLendon  
Morfitt

Exp #361

12" Aluminium Reactor surrounded by 3-7/8" Bi<sub>2</sub>O<sub>3</sub>CO<sub>2</sub> dry  
one 1 7/8" shell. H/X 359.

Source @ 16.5 cm 9 cm from bottom.  
Instruments as per #359

Time	Solu.	C <sub>1</sub>	C <sub>2</sub>	1/M <sub>1</sub>	1/M <sub>2</sub>	Remarks
3:25	11.0	26.23 (25)	38.5, 48. (39)	1.0	1.0	16 MT
3:30	17.1	42.0	72	.60	.54	
3:42	23.1	106.	215	.236	.18	from #7 7MT
3:48	25.5	166	330	.15	.12	#8 MT @ 28.3
3:54	29.05	413	824	.06	.05	
	31.5	Sub. Est. crit		31.8		
	32.0	Super critical Rod @ 30.				
	31.8	Subcritical				

Conclusion: Critical at 31.9 cm.

Decided to eliminate experiment of 2 shells of Bi<sub>2</sub>O<sub>3</sub>CO<sub>2</sub>  
because only 3.3 cm difference in gap between this  
exp + exp #359.

Inventory See #360

st. glass Ht	31.9
zero	1.25
Bottom	.6
Hc	<del>33.75</del>
Vc	33.5
Mc	24.4 g
H/X	1.77 kg
	352



64  
1/6/50

Exp #362

Crown  
Richardson  
Mortiff

12" Aluminium Reactor Surrounded by one - 7/8" shell of  
Bi<sub>2</sub>O<sub>3</sub>-CO<sub>2</sub> (data p 97 boxes) H/X = 359

Source @ 16.5 cm 9.0 cm from bottom.

Instrument	Temp	Start.
3	82X100	X10
4	NG	—
5	—	X2
6	5.4X1000	X25
7	.7	—

Time	Solu Hgt.	#1	#2	$\frac{0}{1M}$	$\frac{x}{1M}$	Remarks
9 <sup>49</sup>	11.1	24 ✓	33.0 ✓	1.0	1.0	#2, 3 MT.
9 <sup>47</sup>	18.0	52	47.0	.46	.70	#4 MT @ 16.5
9 <sup>52</sup>	23.1	84	105	.29	.31	#5 MT @ 26.0
9 <sup>57</sup>	27.1	138	204	.17	.16	from #6
10 <sup>02</sup>	31.0	318	554	.076	.0595	
	Rod in	190	299	.13	.11	
New add'n	Rod in	280	410	.086	.087	
10 <sup>14</sup>	32.6	776	963	.031	.024	Stopped #6
	34.7	Crit Rod @ 22.0 cm.				from #7
10 <sup>22</sup>	34.3	" " @ 25.0				
10 <sup>30</sup>	33.9	" " @ 29.0				
	33.7	Subcritical Rod Out.				

Conclusion: Critical at 33.8 cm

Inventory. See Exp 360

st. glass	33.8
zero.	1.0
Bottom	.6
Hc	35.4
Vc	25.8 g
Mc	1.87 Kg
H/X	352 ✓

1/6/50  
 McJendon  
 Morfitt  
 Callihan  
 Cronin

Exp. 363 H/x = 359

12" Al Reactor with one 78" shell of water  
 no other reflectors  
 Source at 16.5 cm (9.0 cm from bottom)

Instrument same as Exp. ~~362~~ 362

Time	So'l'n Ht.	#1	#2	Y/m <sub>1</sub>	Y/m <sub>2</sub>	
2:25	11.3	31	39	1.0	1.0	#2, 3, MT
		31	39			
2:32	17.9	64	64	.485	.60	#4 MT of 18.
2:37	22.1	125	155	.25	.25	
2:45	24.0	201	200	.154	.195	
2:55	<del>25.5</del>	203	289	.153	.135	
2:58	25.5	378	601	.082	.065	
2:59	Rod in	220	300	.14	.130	
3:06	26.15	620	1003	.05	.039	Start #6
	Rod in	300	430	.103	.099	
	27.1	Rod at 25.5				
	26.9	Subcritical Rod out				

Critical at 27.0 ± 0.1 cm

27.0  
 zero 1.0  
 Bottom .6  


---

 Hc 28.6  
 Vc 20.9 ✓  
 Mc 1.52  
 H/x 352

66 1/9/50

#  
Exp. 364

Crown  
Flaccin  
Mortitt  
Henry

12" Aluminum Reactor surrounded by 2 7/8" shells  
of water as side tempers. No other reflectors H/X = 359

Inst Number	Start @	Trips at
3	x10	84x100
4	NG	NG
5	x2	—
6	<del>x25</del> out	out.
7	—	3 1/2" average ~ .7 average.

Source @ 15.5 cm 8 cm from bottom.

Time	H <sub>eff.</sub>	#1	#2	1/M <sub>1</sub>	1/M <sub>2</sub>	Remarks
10:50	11.2	28.0 ✓	29.0 ✓	1.0	1.0	#24 #3 MT
11:05	18.7	78.0	84.0	.36	.34	From #4
11:12	22.0	185.0	246.0	.15	.12	#4 MT at 17.8
11:16	23.0 With Rod	192.0	250.0			Use #5
11:18	23.0 No Rod	302.0	426.0	.09	.068	
11:24	24.1	1045	856	.03	.03	
11:28	25.1	Rod at 13.0, # 12.1 cm of rod - <del>sub</del> critical				
11:30	24.9	Critical with rod at 14.0 (10.9 cm. of rod)				
11:32	24.7	" " " " 16.0 (8.7 " " " )				
11:33	24.5	" " " " 21.0 (3.5 " " " )				
11:35	24.35	subcritical				

Conclusion: Critical at 24.4

zero c.	1.0
Bottom =	.6
Hc	26.0
Vc	19.0 ✓
Mc	1.38
H/X	352

1/9/50

Exp. 365

Cronin  
Macklin  
Morfitt  
Henry

12" Al. Reactor surrounded by 3 -  $\frac{7}{8}$ " shells + 1 -  $\frac{1}{4}$ " shell  
of water. Other conditions same as # 364  
 $H/X \approx 359$

Time	HV.	#1	#2	$C_{10}/C_1$	$C_{20}/C_2$	Remarks
11:52	10.8	16.0 } 16.0	15.0 } 15.0	1.0	1.0	
		16.0 }	15.0 }			
11:57	17.5	35.0	33.0	.46	.46	
12:03	22.1	147.0	189.0	.11	.08	
		With rod 95.0		.17		
12:12	23.3	Subcritical				
12:13	23.2	Subcritical				

Conclusion: Critical at 23.25

Drain back (see Exp. 360)

Sight glass Ha	23.25
zero	1.0
Bottom	.6
<hr/>	
Hc	24.85
Vc	18.1 ✓
Mc	1.31
H/X	352

1/9/50

Exp. # 366

No star reflector

Crosby  
Moffitt  
Machlin  
Henry

12" Al. Reactor. 1- $\frac{3}{8}$ " shell filled with  $\text{Bi}_2\text{O}_3\text{CO}_3$  slurry\*  
Other factors same as #364  
 $H/k \approx 359$   
(0.8 gm/cm<sup>3</sup>)

Time	Wt.	#1	#2	C <sub>10</sub> /C <sub>1</sub>	C <sub>10</sub> /C <sub>2</sub>	Remarks.	
1:33	10.0	30.0	37.0	1.0	1.0		
		30.0	36.0			#4 MT at 18.0	
1:37	18.5	76.0	77.0	.39	.48	From #5	
1:44	23.0	161.0	208.0	.17	.18		
1:48	25.0	290.0	452.0	.10	.08		
	" Roddn.	195.0	275.0	.15	.13		
1:53	26.5	917.	971.	.03	.04		
	" Roddn.	340	500	.09	.08		
2:02	27.5	critical with rod at 18.0 (9.5 cm. of rod)					
	27.3	" " " " 20.0 (7.3 " " " )					
	27.1	" " " " out					
	27.0	subcritical					

Conclusion: Critical at 27.1  
zero 1.0  
Bottom .6

$$H_c = 28.7$$

$$V_c = 20.9 \quad \checkmark$$

$$M_c = 1.52$$

$$H/k = 352$$

\* See p 70

1/9/50

EXP # 367

Crown 12" Al reactor 3-7/8" shells Bi<sub>2</sub>O<sub>3</sub> Co<sub>2</sub> slurry \*  
 Macklin + 1 1 3/4" shell with Bi<sub>2</sub>O<sub>3</sub> Co<sub>2</sub> slurry. No other reflectors.  
 Herford Source & instruments for #367 Total Bi thickness - 3 1/2"  
 H/x = 359

Time	Sh. Hgt.	#1	#2	C/C <sub>1</sub>	C/C <sub>2</sub>	Remarks
4:56	10.6	18.0	17.0	1.0	1.0	#2, 3, 4 MT.
5:04	17.8	42.0	40	.43	.43	4 MT. @ 18.0
5:10	22.0	197	239 <del>197</del>	.09	.071	
5:14	23.4	Critical with rod @ 15.0				
5:16	23.2	" " " " 20.0				
5:20	23.0	Slightly subcritical with rod out.				

Conclusion: Critical @ 23.1 cm. on slightly glass  
 zero 1.0  
 Bottom .6

Hc 24.7  
 Vc 18.0 ZV  
 Mc 1.31 Kg X  
 H/x 352

Drawback for #360

\* See p 70

70  
11/10/50

Bi- Slurry Data.

Used in experiments 366, 367, 368.

Shell #	Tare lbs	Gross lbs	Net lbs	Area cm <sup>2</sup>	Depth Slurry cm	Volume cc	P <sub>slurry</sub> g/cc slurry	P <sub>Bi</sub> g/slurry	P <sub>H<sub>2</sub>O</sub> g/cc
12A	11.0	45.5	34.5	116	70.2	8140	1.92	.879	.847
12B	11.0	47.0	36.0	116	76.4	8860	1.84	.843	.811
14A	12.5	49.5	37.0	134	68.0	9110	1.84	.843	.811
14B	12.5	52.0	39.5	134	73.1	9800	<del>2.03</del> 1.83	.838	.807
16A	14.0	55.0	41.0	151	65.0	9810	1.90	.870	.838
16B	14.0	57.0	43.0	151	67.7	10220	1.91	.875	.842
18A	19.0	134.5	115.5	408	72.0	29400	1.78	.815	.785
18B	19.0	152.	133.0	408	82.4	33600	1.80	.824	.794
							Ave. 1.85	.848	.817
							Deviation ± 3.8%		

Slurry was made up on wgt basis:

$$\begin{array}{r}
 19.0 \text{ lbs Bi}_2\text{O}_3\text{CO}_3 \\
 + 15.0 \text{ lbs H}_2\text{O} \\
 \hline
 34.0 \text{ lbs}
 \end{array}$$

$$\begin{array}{l}
 \text{Wgt \% Bi}_2\text{O}_3\text{CO}_3 \quad \frac{19}{34} = 55.9 \% \\
 \text{Wgt \% Bi} \quad .820 \times 55.9 = 45.8 \% \\
 \text{Wgt \% H}_2\text{O} \quad \frac{15}{34} = 44.1 \%
 \end{array}
 \left. \begin{array}{l} \\ \\ \end{array} \right\} \text{These data used to obtain last two columns}$$

$$\begin{array}{l}
 \text{Ave. g slurry/cc} \quad 1.85 \\
 \text{Ave. g Bi}_2\text{O}_3\text{CO}_3\text{/cc} \quad 1.034 \\
 \text{Ave. g Bi/cc} \quad 0.848 \\
 \text{Ave. g H}_2\text{O/cc} \quad 0.817
 \end{array}$$

11/1/50

Exp #368

Crossin  
McKendrew  
Mortitt

17" Al reactor 3-7/8" shells + 1-1 1/4" shell, all filled with  $\text{Bi}_2\text{O}_3\text{CO}_2$  slurry. See p 70 for concentration. No other reflector. Source @ ~~16.5 cm~~ 16.5 cm 9 cm from bottom.

$H/x \approx \frac{500}{493}$

Instrument	Start @	Trip @
3	X10	79X100
4	NG	NG
5	X2	—
6	X25	6X1000
7	—	0.72 @ 4"

Time	Hgt.	#1	#2	$C_{10} / C_{50cm}$	$C_{10} / C_2$	Remarks
9:30		Began filling to cover source. Took <del>some</del> from each cyl on way up: A ~ 5 cm B ~ 5 cm C ~ 2 cm D ~ 2 cm E ~ 2 cm F ~ 2 cm.				
9:47	12.3	13.0, 14.0, 14.0	16.0, 14.5	1.0	1.0	Entered on above
10:18	18.5	23.5	23.0	.60	.70	2 cm ea from G, H, J
10:27	24.5	55.	74.5	.255	.225	2 cm ea from J, H, G
10:34	26.5	100	157	.14	.106	from F
10:44	28.0	307	521	.046	.037	from E
10:50	29.0	Critical with rod @ 20.0				
	28.8	" " " "				
	28.6	Slightly super with rod out.				
10:52	28.5	Subcritical.				

Drainback as above.

Conclusion Critical at 28.55 on sight glass.

$$\begin{array}{r} \text{Zero c.} \quad 1.0 \\ \text{Bottom c.} \quad .6 \\ \hline \text{Hc} \quad 36.15 \end{array}$$

$$V_c \quad 22.0 \text{ g.} \quad \checkmark$$

$$M_c \quad 1.17 \text{ kg}$$

$$H/x \quad 493$$



72  
1/11/50

Exp #369

Crown  
McLendon  
Mortitt

12" Al reactor Untemped  $H/X = 500$   
Source @ 17.5 10 cm from bottom.  
Instruments Same as 368.

Time	Solv Hgt.	#1	#2	$c/c_0$	$X/c_0$	Remarks
12:50	10.0	14.5	39.5'			
		14.5'	39.0			
12:53	13.5	16.0 (16.5)	(26.0), 26.0			#1 - MT
1:00	18.1	27.0	39.0	.61	.67	#2 - MT @ 17.5
1:07	22.0	35.5	56.5	.47	.46	#3 - MT @ 24.0
1:14	28.0	52.0	103.	.32	.25	#4 - MT @ 30.2
1:21	35.0	89.5	213.	.18	.12	#5 - MT @ 38.0
1:32	40.6	162.	439	.102	.06	
1:44	46.0	567	855	.03	.03	#6 - MT @ 46.5
1:53	48.7	Super - Rod @ 38.0				
	48.5	" - Rod @ 40.0				
	48.3	Critical - " @ 42.0				
	48.05	Slightly super - Rod out				
	47.85	Sub-critical - " "				

Conclusion: Critical at 47.95 on sight glass

Draw back - 8 - 12' cms into #6, #5, #4, #3  
4.5 - " " " #2

sight glass ht. 47.95'  
zero c. 1.00  
Bottom c. 0.6  
Hc 49.55'  
Vc. 36.1 L ✓  
Mc 1.91 Kg  
H/X 493

1/11/50

Exp. #370

Crown  
McLendon  
Masfitt

12" Aluminum Reactor 1- 3/8" shell of water.  
H/X = 500

Time	Solv - off	#1	#2	%c.o.	%c.o.	Remarks
22.7	12.0	18, 18	37, 37	<del>37.5</del>	4	#1 MT
23 1/2	20.0	37.5	59.5	.48	.63	#2 MT at 15.5
2:45	23.9	59	109	.30	.34	from #9
3:00	26.9	87	176	.21	.21	9 MT at 26.0
3:03	30.0	158	369	.11	.10	from #8
3:12	32.15	363	922	.05	.04	from #7
3:17	34.0	Rod at 30 cm critical				
3:19	33.75	Rod at 32 cm critical				
3:21	33.55	Sub Critical				

Critical at 33.65 ± 0.1 cm on sight glass.

Drainback:

#8 } as taken out #9  
#7 }

33.65 -  
1.0  
6

Hc 35.25

Vc 25.7 L ✓

Mc 1.36 Kg X  
H/X 493

11/50

#

371

Exp ~~371~~  $\frac{H}{X} \approx 500$

Crown  
McLellan  
Morfit

12" Al Reactor fully water tamped

Source at 10 cm  
Instrument as 4367-

Inventory:

	#9	#8	#7	#6	#5	#4	#3	#2	#1
cm in 12"	8.0	4.9	4.8	8	8	8	8	6	M.T.

Time	Solv H <sub>2</sub> O	#1	#2	C <sub>1</sub> /C <sub>0</sub>	C <sub>2</sub> /C <sub>0</sub>	Remarks
3:47	11.7	2.5 ✓	4.5 ✓	1.0	10.5	#1 MT from #2
3:52	16.6	5.0	10.5	.50	.43	#2 MT @ 17.5
4:00	19.05	18.0	22	.25	.225	from #3
4:07	21.0	19.0	45	.13	.10	
4:15	22.1	45	112	.056	.04	
4:22	23.1	Critical with rod @ 20.0		20.0		Temp 1 mm high
4:25	22.9	" " " "		30.0		Temp on
4:29	22.75	Subcritical				

Conclusion: Critical @ 22.80 ± 0.05 cm on sgt glass.

$$\begin{array}{r}
 22.80 \\
 1.25 \\
 \hline
 24.05 \\
 \hline
 H_c \\
 \\
 V_c \quad 18.0 \text{ Z.V.} \\
 M_c \quad 0.95 \text{ kg} \\
 H/K \quad 493
 \end{array}$$

1/11/50

Exp # 372

Crown  
McKandow  
Morfield

12" Al Reactor. Surrounded by 3-7/8" shell + 1-1/4" shell. Water filled. No other reflector. H/X ~ 500  
Source & Instruments as per #367  
For Inventory See #371. Use Background of ~~15.0~~ 30.0

Time	Soln. Hgt.	#1	#2	C/c. <sub>10</sub>	C/B. <sub>10</sub>	Remarks
4 <sup>32</sup>	23.0	29.5	49.0	.085	.072	25.5 from #3 M7e
4 <sup>40</sup>	24.0	33.0	58.0	.076	.078	from #4.
4 <sup>52</sup>	27.0	99.0	206	.15	.145	
5 <sup>00</sup>	28.0	417	913	.048	.033	
5 <sup>04</sup>	28.6	Super critical				
5 <sup>03</sup>	28.5	Super critical				
5 <sup>04</sup>	28.3	Subcritical				

Conclusion: Critical with slight glow @ 28.4 cm.

Inventory

	#9	#8	#7	#6	#5	#4	#3	#2	#1
cm w 12"	9.0	9.0	9.0	9.0	9.0	8.5	8.5	8.5	DV+3
								9.0	

$$\begin{array}{r}
 28.4 \\
 1.0 \\
 \hline
 30.0
 \end{array}$$

Vc 21.92 ✓  
Mc 1.16 kg  
H/X 493

Boing correction 0.25 cm.

1/12/50

EXPERIMENT # 373

H/X ~ 500

12" Al Reactor surrounded by 3 - 7/8" shells + 1 - 1 3/4" shell filled with UO<sub>2</sub>(NO<sub>3</sub>)<sub>2</sub> @ 12% conc.

CRONIN  
MORETT  
McLENDON

Source: Scale - 17.5 cm. Source Ht. = 10.0 cm.

Instruments:	Initial Scale	Trip Pts.
3	100	79 x 100
4	5	-
5	25 x 2	-
6	25	5.9 x 1000
7	-	.72 @ 4"

TIME	Ht.	#1	#2	M <sup>-1</sup>	M <sup>-2</sup>	REMARKS
1:05	12.9	8.0, 8.5	17.0, 15.5	1.0	1.0	#1 MT @ 30
1:13	20.0	8.25	16.25	-	-	#2 MT @ 14.0
		18.	32.	.44	.50	
1:21	25.0	43.5	106	.184	.151	#3 MT @ 22.0
1:27	26.9	100	263	.081	.061	Stopped #4
1:34	28.5	Super critical (Rod @ 21 cm)				
1:35	28.3	" " (Rod @ 28 cm)				
1:37	28.1	Subcritical				

Conclusion: Critical with sight glass @ 28.2 cm  
1.0  
.6

Drawback on per # 372.

Ht 29.8  
Vc 21.7 L  
Mc 1.15 Kg  
H/X 493

Lab. Colorimetric Analysis on this material 0.0534 g/g sample. Corresponding to H/X = 477

4/12/50

EXPERIMENT #374

H/x = 477

CRONIN  
MORFIT  
MCLONDON

12" AL. REACTOR - 1 -  $\frac{7}{8}$ " shell of  $UO_2(NO_3)_2$

Source: 10 cm. from bottom.

Instruments: Same as #373.

TIME	Ht.	#1	#2	$M^{-1}$	$M^{-2}$	REMARKS
2:41 pm	13.0	(16.5)	(32.0)			#1 & #2 MT
		16.5	31.5			
2:48	22.3	41.0	82.0	.40	.39	#3 - MT @ 22.3
2:53	28.0	86.5	220	.145	.191	
3:00	31.2	193	513	.086	.056	#4 MT @ 30.3
3:20	32.9	SUB CRITICAL				
3:26	33.5	"	"			
3:28	34.1	CRITICAL - Rod @ 25.5				
3:30	33.9	"	"	@ 28.5		
	33.65	Slightly Super Critical				
	33.55	SUB-Critical				

Conclusion: Critical at sight glass = 33.6 cm.

Drainback as per #372.

Sight Glass reads -1 cm when level is zero in 12" cyl.

$$\begin{array}{r}
 33.4 \\
 1.0 \\
 .6 \\
 \hline
 H_c \quad 35.2
 \end{array}$$

Vc 25.7 L ✓  
 Mc +36 kg  
 H/x 493

1/13/50

Exp. #375

H/X 2477

Crown  
McKendow  
Mortitt  
Henry.

10" Aluminium Cylinder Surrounded on sides by 2 1/2" stainless steel reflector. Water outside stainless on sides, also top & bottom. 30 - 35 cm.

Source Scale: - 17.5 Source Hgt: - 10.0 cm.

Time	Soln Hgt.	Starting Scale			Trip Scale		Remarks
		#1	#2	M <sub>1</sub> '	M <sub>2</sub> '		
12:53 pm	12.3	2.0	2.0			#1 MT @ 2.8 cm.	
		(2.0)	2.5				
1:10	11.7	Readjustment of Ht due to blow back of sight glass.					
1:19	20.9	3.75	5.5	.53	.41	#2 MT @ 17.5	
1:27	26.0	4.75	9.25	.42	.24		
1:37	30.1	7.5	15.0	.27	.15	#3 MT @ 30.8	
1:45	36.1	30.0	78.0	.067	.029		
1:51	38.1	Super Critical - Rod @ 32.0 cm					
1:54	37.8	Critical - Rod @ 37.0 cm.					
1:58	37.5	Critical - Rod out!					
	37.4	Sub-Critical					

Conclusion: Critical @ sight glass = 37.50 cm. -

.5  
 .9  


---

 H<sub>c</sub> 38.9 cm.  
 V<sub>c</sub> 19.7 g ✓  
 M<sub>c</sub> 1.04 kg  
 H/X 493

With water in tank, sight glass reads minus 0.5 cm. @ zero soln level.

SOLID INVENTORY:

CYL'S - #1 #2 #3 #4 #5 #6 #7 #8 #9  
 DI. + 2 13.0 12.0 12.0 13.0 13.0 13.0 13.0 13.0 - cms in 12" cyl.

1/13/50

EXPERIMENT # 376

CRONIN 10" Al. - Surrounded by 2 1/2" stainless reflector only.  
 McLENDON (No H<sub>2</sub>O present)  
 MORETT  
 HENRY

Source: Scale 17.5 - 10.0 cm from bottom.

Instruments as per # 375 -

TIME	HT.	#1	#2	M <sub>1</sub>	M <sub>2</sub>	REMARKS
		18.0	37.0			
2:07	37.6	86.0	264.	.21	.14	
2:11	40.7	116.0	356.	.155	.104	#4 NT @ 43.0
2:23	45.0	482.	828	.037	.045	
2:27		104		.17		Rod in!
2:30	46.8	CRITICAL - Rod @ 42.0 cm.				
	46.6	" " " 45.0 "				
2:32	46.4	" - Rod out!				
	46.2	SUB-CRITICAL				

Conclusion: Critical @ sight glass = 46.4 cm.

Drain back:  $\frac{1}{2}$  INVENTORY

#1	#2	#3	#4	#5	#6	#7	#8	#9
DV+40	13.0	13.0	13.0	13.0	13.0	13.0	13.0	13.0

46.4

zero

Bottom

---

Hc 47.6

Vc 24.1 X ✓

Mc 1.28 Kg

H/X 493

BONE CORRECTION - 0.2 cm.



1/15/50

## EXPERIMENT #377

 $H_x = 477$ 10" AL. - FULLY H<sub>2</sub>O TAMPED

SOURCE : SCALE 17.5 - 10.0 cm from bottom.

INSTRUMENTS : AS PER #375.

TIME	HT.	#1	#2	$M_1^{-1}$	$M_2^{-1}$	REMARKS	
		1.5	2.75				
3:10 pm	11.6	(1.5)	(3.0)			#2 MT 17.0	
3:20	24.9	5.0	11.0	.30	.27	#3 MT 30.0	
3:28	30.1	8.5	25.5	.177	.117		
3:42	34.0	31.5	90.	.048	.033		
3:47	36.3	CRITICAL - Rod @ 30.0					
3:50	36.1	" " @ 34.0					
3:52	35.9	" " @ 40.0					
3:53	35.7	Slightly Super - Rod out!					
3:55	35.6	SOB - CRITICAL -					

CONCLUSION: CRITICAL @ SIGHT GLASS = 35.65 cm.

DRAINBACK AS PER #376

sight glass	35.65
zero cm.	.5
Bottom cor.	.9
$H_c$	<hr/> 37.05

$V_c$	18.8 L
$M_c$	1.00 Kg
$H/x$	493

1/16/50

Exp. 378

$\frac{H}{X} = \frac{493}{977}$

Manfitt  
Machlin  
Crown

15" Al Fully H<sub>2</sub>O tamped

Source: 5cm from bottom 12.5cm on scale  
 Instruments: Trip Start  
 3 82x100 x100  
 4 — x10  
 5 — x1  
 6 5.8x1000 x25  
 7 3" from tube —

Inventory: DV 1 2 3 4 5 6 7 8 9  
 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8 in 15" cyl.  
 Dry B.G. (12.5) 13.0 (35) 35.5  
 Est. Cr. l ≈ 16 cm.

Time	Sol'n Ht.	#1	#2	M <sub>1</sub> <sup>-1</sup>	M <sub>2</sub> <sup>-1</sup>	Remarks
12:50	6.1	2.25 (2.0)	3.0 4.0 (3.5)	1.0	1.0	#1 MT @ DV.
12:40	12.0	4.75	7.75	.42	.45	#2 MT @ 7.7 from #3
1:00	14.0	7.0	13.5	.29	.26	#3 MT at 13.4
1:10	16.0	18	30	.11	.097	from #4
1:20	17.35	156	36	.013	.0097	from #5
1:25	Rod in tamped	19	41	.11	.097	
1:30	17.80	Critical Rod at 10cm				
1:35	17.60	Critical Rod at 12cm				

Critical ~~rod~~ at 17.5 cm ± 0.1 cm  
 zero cor .0  
 Bottom .4  
 H<sub>c</sub> 17.9  
 V<sub>c</sub> 20.4 Z ✓  
 M<sub>c</sub> 1.08  
 H/X 493

82  
1/16/50

Ex 379

Monitt  
Madelin  
Crosin  
Henry.

15" Al Reactor unstamped  $H/K = 477$   
Instruments + source same as Ex. 378

background = 12.5 35

Time	Sol or HT	#1	#2	$1/M_1$	$1/M_2$	
1:40	17.9	32.0	43.5	.39	.81	
		32.0	42.5			
1:54	23.9	68.0	127.5	.184	.275	#4 MT at 21.2
2:00	25.0	87.1	185	.144	.189	#5 MT at 25.0
2:14	26.95					#6 #7
		194	4955	.064	.07	
	Body Rod in	80	160	.157	.22	
	(Rod	120	255	.104	.137	
2:30	28.15	Sub Critical Rod out				
2:35	28.70	Critical Rod at 19				
2:37	28.55	Critical Rod at 21				
	28.40	Critical Rod at 23				
	28.30	Critical Rod at 28				

Critical at  $28.2 \pm 0.1$  cm by sight glass.

zero cor. - .3  
Bottom + .4  
Hc 28.30

$V_c$  32.3 I ✓  
 $M_c$  1.71 kg  
 $H/K$  493 ✓

4/18/50  
Crown  
McLendon  
Morford

Exp # 380

15" AI Reactor Untamped  $H/X \approx 720$

Source @ 20.5 cm 13 cm from bottom.  
Bak (Conservative Estimate Criticality) 41. cm.

Instruments	Start @	Trip @
3	x100	84 x 100
4	x10	—
5	x2	—
6	x25	5.4 x 1000
7	—	—

Time	Solu' Hgt.	#1	#2	$\frac{1}{M}$	$\frac{1}{M}$	Remarks	
9:26	4.6	—	—	—	—	9 MT	
9:38	11.5	14.0, 14.5, <u>14.9</u>	29.0, 31.0, <u>29.5</u>	1.0	1.0	2 cm from #1, 2, 3 4, 5	
9:52	20.5	23, 24	26.5, 26.5	.60	—	2 cm from #6, 7	
10:03	28.5	43	74	.33	.40	2 cm from #1, 2, 3, 4	
10:15	36.55	90	214	.155	.138	2 cm from #5, 6, 7, 8	
10:23	40.0	148	378	.095	.074	#2 MT from #2	
10:28	44.1	—	—	—	—	#2 MT <del>#3 MT</del>	
10:36	45.05	Super rod @ 30					
10:38	44.70	Super rod @ 40					
10:40	44.5	Critical					
10:41	44.45	Subcritical					

Conclusion: Critical @ 44.5 cm on sight glass.

$$H_c = \frac{-0.3}{+0.4} = 44.4 \text{ cm}$$

$$V_c = 50.8 \text{ L } \checkmark$$

$$M_c = 1.79 \text{ Kg}$$

$$H/X = 733$$

1/17/50

## Dilution

from Pent III Mass required for 15" untamped cylinder  
 at  $\frac{1}{4}$  u 800 is from 1.8 to 2 Kg. For 12" untamped nothing  
 definite.

To insure maximum probability of 12" being critical  
 2.4 Kg of X were left in pit storage cylinder. Water added.  
 (2.4 liters per cyl to give  $\frac{1}{4}$  u 721 assuming previous  $\frac{1}{4}$  u 60477)  
 This gives maximum volume in pit about 62 liters.

Colorimetric analysis from lab sampled E 380 = 0.0355 gm u/gm  
 This is equivalent to  $\frac{1}{4}$  u = 741.5

1/18/60

Exp #381

Crown

15" Reactor Tamped  $H/X \approx 720$

McLendon  
Morfitt

Instruments same as #380  
Source @ 175cm 10 cm from bottom  
Critical Est. - 29 cm

Time	Solow Hgt.	#1	#2	$1/M_1$	$1/M_2$	Remarks
11:29	12.2	2.0	4.0 35	1.0	1.0	#6 MT
11:43	20.05	5.5	13.0	.364	.298	#7 MT #8 MT
11:52	23.0	10.0	27.5	.20	.14	# 5 MT
12:08	25.65	47.	136	.042	.028	from #3
12:08	26.6	Critical est @ 22.				
12:10	26.4	" " " 25				
12:14	26.2	Subcritical				

Conclusion Critical @ 26.3 cm.

Zero cor.	0
Bottom	.14
$H_c$	26.7
$V_c$	30.4 $\checkmark$
$M_c$	1.07 kg
$H/X$	<del>493</del> 733

Inv.	1	2	3	4	5	6	7	8	9
	6	6	6	6	6	6	6	6	6

Boing Correction 3mm.

(6)

Bottom correction: Sight Glass reads +3 mm when solution at zero. This value was recalled a week after experiment. Value was checked by comparison with 15" cyl. <sup>measurement.</sup> which ~~was~~ gave some answer. ~~Check~~  
~~Checked under cylinder to see result.~~

4/19/50

Exp #382

Crowd  
McLendon  
Marlitt

12" Al Reactor Tamped  $\mu/k \approx 720$   
Source @ 22.5 15 cm from bottom.

Instruments	Starting scale	Trip @
3	X100	82 X100
4	X10	—
5	X2	—
6	X25	5.1 X1000
7	—	—

Inventories: 9.5 cm of height per cylinder

Time	Solv Hgt	#1	#2	$\frac{1}{M}$	$\frac{1}{M_0}$	Remarks
9:02	16.9	9.0 10.0	36.0 36.0	1.0	1.0	#1 #2 MT } BG for last.
9:31		2.0 } 1.5 } 1.75	3.0 3.0			B.G for tamped. #3 MT @ 22.2
9:40	30.9	6.0	17.0	.292	.177	#4 " @ 31.5
9:52	33.0	7.5	24.0	.433	.125	
10:06	37.2	15.0	49.0	.117	.061	#5 off @ 40.1
10:15	41.7	SUB-CRITICAL		ROD OUT!		
	42.8	SUPER-		ROD @ 38.0		
10:22	42.6	CRITICAL /		" @ 40.0		
	42.3	SLIGHTLY SUPER.		ROD OUT!		
10:27	42.1	CRITICAL		ROD out		
10:30	42.0	SUB-CRITICAL		-		

CONCLUSION:

CRITICAL @ 42.1 on SIGHT GLASS.	42.1 cm
Ferr Correction	0.5
Bottom Correction	0.6
$H_c$	43.2 cm
$V_c$	31.5 L.
$M_c$	1.11 kg

Borg Correction 32cm.

1/19/50

87

Exp. # 383

CROWIN 12" AL REACTOR - UNTAMPERED  $H/X \sim 720$ MORFITT  
MCLENDON

SOURCE @ 225 15 cm from bottom.

INSTRUMENTS: AS PER # 382

TIME	SOLN HT	#1	#2	$\frac{\circ}{m_1}$	$\frac{x}{m_2}$	REMARKS
		9.5	36.0			B.G.
10:45 am	42.3	41.5	137.	.274	.265	#5 MT
		<del>38.5</del>	<del>7#</del>			
11:00	50.2	49.5	156	.192	.231	#6 MT @ 52.7
11:10	60.0	50.0	139	.190	.259	#7 MT @

Conclusion: System extrapolates to 0. —



2/7/50

Exp 384

Cronin

12" Reactor Untamped H/x = 80 High N. Rate

Fox

Moffitt

Macklin

Source @ 8 cm from bottom. Zero @ 11 cm

Instrument	Stats @	Traps @
3	X10	85X100
4	X100	—
5	X2	—
6	X25	6X1000

Time	Ht.	I	II	%	%	
		12.0 (12.7)	24.0 (25.9)	1.0	1.0	
12:30	9.1			Ave of 6 5-minute counts		3 MT.
12:50	15.0	28.5	49.5	.445	.485	#1 about MT.
1:03	19.5	48	89	.27	.285	from #3 & #7
1:14	25.1	94	182	.135	.140	from #7 & #9
1:35	29.2	176	351	.072	.072	#1 MT #5 MT
1:40	31.85	328	656	.039	.039	#7 MT. 9 MT

Out of Solution.

Extrapolated Critical Height = between 34.2-34.6 sight glass ht.  
(Reasonably good extrapolation possible.)

Sight Glass 34.4 T  
Lens Cor. 0.2  
Bottom Cor. 0.6

H<sub>c</sub> 35.2 cm TV<sub>c</sub> 25.67 L T 25.7M<sub>c</sub> 6.06 kg T

H/x = 88.0

2/7/50

Exp 385

Crown  
Fox  
Maecilia  
Mortit

12" Reactor Tamped  $H/x \approx 80$  High Nitrate  
Source @ 15.0 cm 4 cm from bottom.

Instrument Same as #384

Time	H <sub>g</sub>	#1	#2	V <sub>c</sub>	M <sub>c</sub>	
2 <sup>40</sup>	6.1	4.5	3.0	1.0	1.0	H 1 M.T.
3 <sup>05</sup>		4.5	4.0			
3 <sup>26</sup>	10.0	7.5	6.5	.60	.54	from #3
3 <sup>30</sup>	14.0	22.5	3.1	.20	.135	#3 M.T. @ 10.5
3 <sup>32</sup>	15.5	Critical with Taper on Rod @ 10 cm.				from #5
3 <sup>35</sup>	15.3	"	"	"	"	Rod @ 15 cm.
3 <sup>35</sup>	15.1	"	"	"	"	Rod Out.

Critical at 15.2 ± 0.1 cm.

When sight glass reads minus 2 mm solution is at zero in 12" cyl.  
No water in taper tank.

Sight Glass	15.2 cm	
Zero Corr.	0.5	
Bottom Corr.	0.6	
H <sub>c</sub>	16.3 cm	
V <sub>c</sub>	1.89 l	11.9
M <sub>c</sub>	2.81	

$H/x = 88.0$

7/8/50

Cornin  
Fog  
Merfitt

Experiment # 386

10" Al Reactor Completely Tamped Heglin No. 14/x-280  
Source @ 17cw 6cw from bottom

Instruments	Strs @	Frips @
3	X 10	95 X 100
4	X 100	—
5	X 2	—
6	X 2.5	5.6 X 1000
7	—	2"

Background for Untamped Case if needed #1 19, 19 #2 17, 16  
Background for Tamped Case #1 4.050 #2 3.031

Time	Solv Hgt.	#1	#2	C/c	Q/c	Remarks
10:37	8.8	4.5 av	3.0	1.0	1.0	From #1 & #5
10:45	14.2	6.5	7.0	.69	.43	#1 MT
10:51	18.0	15.0	17.0	.30	.176	#5 MT
11:02	20.0	52.0	71	.087	.042	from #9
11:08	21.2	Critical Temp down Rod @ 12.0 cm				from #7
11:10	20.8	" " " Rod @ 24.0 cm				
11:12	20.6	Sub <del>critical</del> Critical Rod out.				

Conclusion: Critical @ 20.7 cm slight glass.

Zero Corr = +.5 cm

21.2

Bong Corr +.25

21.45

3" section = +.90

Corrected Hc = 22.35 22.4

Vc = 11.32 11.3

Mc = 2.68 2.67 ✓

H/x = 88.0

2/8/50

Experiment #387

Conrad  
Fox  
Mearns

10" Aluminum Reactor Untamped. High  $M_0$   
Source & Instruments as per 387 386.  
Background taken as off #386

H/x = 80

Time	Solu Hgt.	#1	#2	% <sub>1</sub>	% <sub>2</sub>	Remarks	
11:18	20.85	33	36	.575	.465		
11:32	30.0	40	47	.475	.350	#5M@25	
11:39	37.6	47	64	.405	.260	#7	
11:45	46.2	45.9	55	.345	.220		
		Out of Solu.					

Conclusion: Critical above 80 cm if at all.

Sight Glass > 80 cm  
 $H_c$  > 81 cm  
 $V_c$  > 41  
 $M_c$  > 9.68

$H/x = 88.0$

Boing correction .25 cm

ZERO Correction on 10" cyl = at zero in cyl sight glass reads minus 0.5 cm (-.5 cm)

92 <sup>2</sup>/<sub>8/50</sub>

Exp #388

Crown

9" Al Reactor Temp. High NO<sub>3</sub> H/x ≈ 80

Fox

Source & Instruments for #386

Moritt

R. Robt (HP observation)

Time	H <sub>0</sub>	#1	#2	c/c	c/c	Remarks
3 <sup>10</sup>	12.3	3.0, 3.5 <u>3.25</u>	3.0, 2.50 <u>2.75</u>	1.0	1.0	#9 MT @ 17
3 <sup>32</sup>	20.2	7	8	.465	.345	#7 MT @ 19.0
3 <sup>40</sup>	24.3	19.5	24.5	.167	.112	
3 <sup>50</sup>	25.5	40.5	59.5	.08	.046	From #5
4 <sup>00</sup>	26.7	Critical Temp Down Red @ 25.0				
4 <sup>05</sup>	26.5	Subcritical				

Conclusion Critical @ 26.6 cm on sight glass.

Bottom 1.15

Zen Cor. 0.0

H<sub>c</sub> 27.7 cm

V<sub>c</sub> 11.34 L 11.4

M<sub>c</sub> 2.68 Kg 2.69

H/x = 88.0

	1	3	5	7	9
cm in 9"	12	12	12	12	7 + DV
cm in 15"	4.3	4.3	4.3	4.3	2.5

Sight Glass Reads 0 at zero level in reactor for water enclosed system

=x

2/9/50

Exp #389 A

Crown 15" Al Reactor Completely Tamped High No<sub>2</sub> 11/10/50.  
 Fox Source @ 13cm on scale 2cm from bottom. Cd Bladed  
 Merfeld  
 Robin (obs) Temper.

Instrument	Start	Trip
3	x10	96 x 100
4	x100	—
5	x1	—
6	x25	5.4 x 1000
7	—	2"

Time	Hght	#1	#2	1/4 <sub>1</sub>	1/4 <sub>2</sub>	Remarks	
1:49	4.1	3.75, 4.25 (4.0)	2.0, 2.0 (2.0)	1.0	1.0	#9 MT, from #5	
1:59	7.0	5.0	3.5	.80	.57	#8 MT, from #5	
2:09	9.1	8.0	6.0	.50	.33	5MT	
2:20	10.5	12.0	11.5	.33	.175		
2:29	11.5	25.0	26.0	.16	.078	from #3	
2:40	12.0	68.0	68.0	.059	.030		
2:45	12.4	Subcritical					
2:48	12.5	Critical Rod @ 13 cm.					

#389 B

Top Temper up. Using Previous log.

2:52	12.5	11.0	10.0	.365	.20	from #3	
2:54	13.2	15.0	13.0	.27	.155		
3:05	14.2	26.0	26.0	.155	.078		
3:12	14.9	59.0	66.0	.068	.030		
3:18	16.3	Subcritical					
3:22	15.5	Critical Rod @ 17 cm.					

389A  
 Jiggle Calcs 12.45 cm  
 Bottom Corr. +0.4  
 Zero Corr. -0.2  
 H<sub>c</sub> 12.7 cm  
 V<sub>c</sub> 14.47 1.45  
 M<sub>c</sub> 3.42 ✓

#389 B  
 15.4 cm  
 +0.4  
 -0.2  
 15.6 cm  
 17.78 17.8  
 4.19 4.20 ✓

#/x = 88.0

94 2/9/50

Exp #390

Crowd  
Fox  
Mafett  
& Rohr  
(HP lab.)

15" Al Reactor Untamped H. Nos H/x  $\approx 80$   
 16 cm on scale 10 cm from bottom.  
 Source @ 10 cm set on scale.  
 Instruments on par #389-A

Time	Solen High	#1	#2	$\frac{x}{1m}$	$\frac{\odot}{1m}$	Remarks
3:37	15.7	30, 36 (34)	32 (32)	1.0	1.0	#3, 5, 7, 9 MT
3:44	17.0	42	44	.81	.73	from #1
3:48	18.0	52	57	.65	.56	
3:53	19.1	68	79	.50	.405	
3:59	19.9	82	99	.415	.325	
4:02	20.8	120	148	.285	.215	

Inch of Solen.

Extrapolation #1 Counter 22.7  
 " #2 Counter 22.6

Conclusion Critical @  $22.6 \pm 3mm$   
 Bag correction 0.2 cm

Sight Glass Records + 4 mm solen, cylinder @ 70 +  
 top of stand empty

Sight glass 22.6<sup>†</sup>  
 Zero corr. -0.4  
 Bottom corr. +0.4  
 Hc 22.6<sup>†</sup> cm  
 Vc = \* 25.8<sup>†</sup> L  
 Mc 6.09<sup>†</sup> Kg X

H/x = 88.0

† Extrapolated

Tube Date 8-1-

Volume occupied by closed end Aluminium Tubes. (106 tubes)

$$\text{O.D.} = 1'' = 2.54 \text{ cm}$$

Tube height as 1 cm then volume of 106 Tubes per cm of height

$$(0.7854)(2.54)^2(1) \times 106 = 5.066 \times 106 = 537.0 \text{ cc/cm}$$

Volume inside closed Tubes per cm length.

$$\text{I.D.} = 15/16'' = 2.38 \text{ cm}$$

Tube height as 1 cm, the volume of 106 tubes per cm of height

$$(0.7854)(2.38)^2(1) \times 106 = 4.45 \times 106 = 471.7 \text{ cc/cm}$$

Volume displaced by open end tubes per cm. length.

$$537.0 - 471.7 = 65.3 \text{ cc/cm per 106 tubes}$$

or 0.616 cc/cm per tube.

$$\begin{array}{r} 1140 \\ 65 \\ \hline 1075 \end{array}$$

Volume displaced by roots per cm height

$$(0.7854)(0.375)^2(1)(6.45) = .712 \times 3 = 2.14 \text{ cc/cm per 3 roots}$$

$$\begin{array}{r} 65.3 \\ \hline 67.4 \end{array}$$

Total area of void  
using open tubes



Volume Bottom Plate =

$$V_A - [V_B + V_C + V_D + V_E] = 1765 - [702] = 1063 \text{ cm}^3$$

$V_A \equiv$  Volume Solid Plate

$$V_A = \frac{\pi D^2 H}{4} = 0.7854 \times (14.8125)^2 \times 0.625 \times 16.39 = 1765 \text{ cm}^3$$

$V_B =$  Volume center Hole

$$V_B = 0.7854 \times (1.5625)^2 \times 0.625 \times 16.39 = 19.6$$

$V_C =$  Volume 108  $1\frac{3}{8}$ " holes

$$V_C = 0.7854 \times (1.125)^2 \times .375 \times 16.39 \times 108 = 6.11 \times 108 = 659.9$$

$V_D =$  Volume 108  $\frac{1}{4}$ " holes

$$V_D = 0.7854 \times (.25)^2 \times (.25) \times 16.39 \times 108 = .196 \times 108 = 21.1$$

$V_E =$  Volume 6  $5/16$ " holes

$$V_E = 0.7854 \times (.3125)^2 \times (.25) \times 16.39 \times 6 = .314 \times 6 = 1.8$$

Volume of Leveling Screws 3.6 cc.

$$\text{Volume Plate + Screws } \frac{1067 \text{ cm}^3}{1.140} = 936 \text{ cm lit.}$$

2/14/50

Exp. #39

Crowd  
Fox  
Hortliff  
Krauss  
Rohr.

15" Al Reactor Tamped. Containing tube bundle  
<sup>open-encl</sup>  
106 tubes spaced on per period # LDP-D 814, 15, 16.  
Purpose of experiment: to evaluate effect of void produced by  
aluminum before running B: - ~~core~~ - core experiment.  
No tube in normal position of source, safety rod or control rod.  
H<sub>2</sub>O<sub>3</sub> H/X ≈ 80

Time	Solu Hgt.	#1	#2	1/4"	1/2"	Remarks
2:57	9.2	5.0, 4.5	4.5 ✓	1.0	1.0	#2 7 H.T.
3:04	14.0	7.5	7.5	.60	.60	#5 H.T @ 13.0
3:12	16.0	15.5	18.0	.29	.25	
3:20	16.8	24.5	26	.185	.175	
3:24	17.3	45.0	47.5	.100	.095	Stop #3
3:31	17.6	68.0	73.5	.067	.061	From #1
3:40	17.9	162	113	.027	.025	
3:42	18.2	Critical Rod @ 9cm.				
3:45	18.1	" " @ 15cm				
3:47	18.0	Subcritical				

5.06 area  
1.06 factor  
30.36  
5.06  
5.36 cm<sup>2</sup>  
2.2  
53.8  
for closed  
tube  
1190 cm<sup>2</sup>  
53.8  
602 cm<sup>2</sup>  
net  
area

Conclusion Critical @ 18.05" <sup>on</sup> sight glass

Inside Cross-sectional area of one tube	4.45 cm <sup>2</sup>	} def. .61 x 106 ----- 64.66	1190 cm <sup>2</sup> 53.8 ----- 602 cm <sup>2</sup> net area
outside " " " " " "	5.06 cm <sup>2</sup>		
15" area =	1140 cm <sup>2</sup>	cont height =	18.05"
Void area =	67	zero corr =	.20
net area =	1073	Bot. " =	+ .40
		Bot. Plate =	-.95

see attached sheet

H<sub>c</sub> = 17.3  
V<sub>c</sub> = 18.56  
MC = 4.39 ✓

H/X = 88.0

Instrument	3	4	5	6	7
Start @	100	20	X2	25	—
Trip @	85 X 100	—	—	5.5 X 1000	5.5

96  
2/15/50

Exp 392

M/4

Crown  
Fox  
Krenai  
M. S. P. H.  
Robt.

15" Aluminum Reactor Tamped. Contains tube bundle  
~~at 100~~ All tubes closed at lower end. Spaced as per drawing  
 LDP- D. 814, 5, 6.  
 Purpose of experiment To determine effect on homogeneity  
 spaced voids thru the 15" cylinder, for comparison with  
 water in Bi metal in same space.

Instrument	Std @	Trips @
3	95 x 100	95 x 100
4	10	—
5	1	—
6	25	6 x 1000
7	—	2" (88)

Source set @ 16.5 cm      0 at 9.5 cm.

Time	Solu	#1	#2	1/N <sub>1</sub>	1/N <sub>2</sub>	Remarks
3:13	9.3	4.5, 5.0, 4.5 (4.75)	3.5, 4.0 (3.75)	1.0	1.0	#9 AT from 27 #1 AT @ 13.2
3:30	16.0	5.0	3.0	.95	—	#5 AT @ 20
3:35	19.9	6.0, 5.0	3.5, 4.0	—	—	
3:44	23.6	5.0	4.5	.90	.83	
3:50	27.4	6.5	5.0	.73	.75	#3 AT @ 30.5
4:00	35.5	8.0	7.5	.59	.50	
4:05	38.8	10.0	9.0	.475	.42	

Out of solution. Straight line extrapolation = 55

Conclusion: Critical only above 45 cm if at all.  
 (But Estimate of criticality 54 cm)

Inventory:	#1	#3	#5	#7	#9
cm in "shallow" cyl.	9.0 cm	9.0 cm	9.0	11.0	1.0 cm + DV

Crit height > 55  
 H<sub>c</sub> > 54  
 V<sub>c</sub> > 32.4  
 M<sub>c</sub> > 7.69, 7.70 ✓

H/x = 88.0

2/16/50

393

NH <sup>7/2</sup>

97

Ex ~~393~~

Callahan  
Mafitt  
Kraese  
Fox  
Rohv  
Gronin

### 15" Al Reactor Tamped

contains 100 Al tubes closed at lower ends and filled with 250 cc of water approx 60 cm ht. Spaced as per drawing LDP-D 814-15-16

Instruments	Stand	Trips
3	x100	96 x100
4	x10	—
5	x1	—
6	x25	5.5 x1000
7	—	3 inches

Source zero at 9.5 cm on scale set at 16.5 cm on scale.  
#1 counter moved to ~~22"~~ from tamper tank to front of shield (in line with source)

Time	Set V	#1	#2	1/M	1/M <sup>2</sup>	Remarks
10:15	10.1	7.5 } 7.75 8.0 }	4.0 } 5 6.0 }			
10:30	<del>15.0</del> 15.0	14.5	9.0	.53	.55	#7 m Tab 11.5 cm Stopped #5 at 15.6
10:40	17.1	37.5	29.0	.205	.172	
10:45	17.8	<del>37.5</del> 37.5	57.	.105	.087	
11:00	18.3	333	23,300	.023	.018	#3
	(Control Rod at 18.5)	259	216.0	.03	.023	
	(Control Rod in)	97	74.5	.08	.067	
11:15	18.5					

Critical at 18.4 cm ± 0.1 cm

zero on	-12	
bottom "	+4	
plate	-95	
Hc	17.65	17.65
Vc	10.62	10.62
Mc	2.54	1.99

H/x = 88.0  
~ 115

? (Solid UNH on fid cylinder walls?)

~~Ex 394~~

~~Inventory in 15" Al cyl (with 100 tubes)~~  
~~#1      #3      #5      #7      #9~~  
~~9.0cm    9.0cm    9.0~~

2/17/50

Experiment #39<sup>4</sup>

Crown  
Fox  
McAfee

15" Al Reactor Water Reflected Side only + 106 tubes  
no rock LDR-D-814.5.6 filled to depth of 27 cm with metal  
Resonance

Instruments	Start @	Trips @
3	X100	95
4	X10	—
5	X1	—
6	X25	5.5 X 1000
7	—	88

Source sub @ 13 cm. (Zero at 6 cm on seal)

Time	Subst. Hgt	#1	#2	1/M	1/M <sub>2</sub>	Remarks
9:25	10.5	14.5, 150 <u>14.5</u>	4.0, 3.5 <u>3.75</u>			#9 & #7 MT @ 11.0
9:35	17.2	21.5	5.0	.673	.75	5 MT @ 28.4
9:42	24.3	30.5	8.5	.475	.442	
10:00	28.0	38.0	11.5	.382	.326	
10:07	30.1	<del>41.5</del> 44.5	14.0	.335	.268	

Tubes covered at this point  
Experiment Stopped.

Conclusion: Critical @ >40 cm.  
(Best estimate of criticality: 44 cm.)

Inventory: 15" cm. "half size" tubes

#	1	3	5	7	9
cm	9.0	9.0	9.0	9.0	2.0 cm + D.V.

H<sub>c</sub> ~ 44  
~~H<sub>v</sub>~~ ~ 26.4 ft  
 M<sub>c</sub> ~ ~~4.97~~  
 4.95

$\frac{1}{x} = 7.48$

$\frac{1}{x} = 88.0 ?$  (solid UNH on pit of wall)  
 = ~~130.3~~ 115

Pit fitted with all cylinders & leak tested

2-21-50

Dilution

orders #1 2 3 4 5 6 7 8 9  
 J A C E F G H D B

Aimed at  $H/x = 240$

removed contents of cyl #9 ( $H/x$  <sup>DFC</sup> 76  $\approx 4.7$  l.) in cyl M  
 now stored in pit.

Redistributed 4.6 cm (15" reaction tubes in pit)  
 (calc 2.77 liters) in 8 each of #1 thru #7  
 [all samples in pit gave SG reading 32.8]

Residue (DV + 0.2 cm (0.6 SG - 0.4 gas cov))  
 had 5.34 l water added, pit & mixed. This  
 mixture was drained jointly into SG9.

Quit for day at this point. Plan to add

4.11 liters water to each of #1 thru 7 and  
 mix in pit cylinder tomorrow.

Plan  
 JWM

2-22-50

J Fox recalculated  $H/x$  getting 88 rather than the  
 76 previously found by DFC.  $\therefore$  halted dilution

2-23-50

JWM & RKM also recalculated  $H/x$  also & got 88.0 after a  
 few false starts. Formula appended.

for solutions containing only  $H_2O$ ,  $HNO_3$ ,  $UO_2(NO_3)_2$

let  $A = \frac{gm U}{gm soln}$   $B = \frac{moles N}{moles U}$   $C = \frac{gm H_2O}{gm U}$

$$H/x = \frac{H_1 + H_2}{x} = \frac{2(moles H_2O) + 1(moles HNO_3)}{C(moles U)}$$

molecular wd of U taken as 235

H	"	"	1
N	"	"	14
O	"	"	16
U	"	"	235

$$\frac{moles HNO_3}{moles U} = B - 2$$

$$\frac{moles H_2O}{moles U} = n$$

where  $n$  can be found simply by solving

$$\frac{gm soln}{gm U} = \frac{1}{A} = \frac{391 + 63(B-2) + 18n}{235} \quad \text{whence } n = \frac{235 - 63(B-2) \times 391}{18}$$

$$\text{and } H/X = \frac{\frac{235}{9A} - \frac{63}{9}(B-2) - \frac{391}{9} + (B-2)}{C}$$

round about check  
correction for  
H<sub>2</sub>O HNO<sub>3</sub>

or

$$H/X = \frac{1}{C} \left[ \frac{26.11}{A} - 6B - 31.44 \right]$$

for H<sub>2</sub>O  
HNO<sub>3</sub>  
UO<sub>2</sub>(NO<sub>3</sub>)<sub>2</sub> only

C = assay ( $\frac{\text{gm X}}{\text{gm U}}$ )

A = concentration ( $\frac{\text{gm U}}{\text{gm solution}}$ )

B = N<sub>2</sub> ratio ( $\frac{\text{mole N}}{\text{mole U}}$ )

Values used here C = .933 A = .1680 (from weighted average of analyses)

B = 6.98 (not final value) (note final experimental analyses tho.)

$$H/X = \frac{1}{.933} \left[ \frac{26.11}{.1680} - 6(6.98) - 31.44 \right] = \frac{1}{.933} [155.42 - 41.88 - 31.44] = \frac{82.10}{.933} = 88.0$$

dilution formula as always

cc of water to add per cc of old solution is

$$\left( \text{new } H/X - \text{old } H/X \right) \left( \frac{9}{235} \right) (\text{old density}) (\text{old concentration in gm/gm soln})$$

holds for any solution when only water is to be added to raise the H/X value.

→ Note: In order to reduce confusion resulting from "scrap-paper" calculations made in the past let us agree that:

1. The H/X corresponding to a given laboratory analysis will be calculated from formulas at top of this page.  
(or formula on next pg if phosphorus present)
2. The calculation will be made by calculating machine if the result entered in this book (or subsequent books) at the place in the book where dilution or receipt of solution was made.
3. Dilutions will likewise be recorded; sufficient space in book will be left (after dilution data are recorded) to record laboratory analysis, requisition number, & H/X.



4. H/x's for dilution may be made at any time.  
The official H/x will be calculated from a sample especially submitted for that purpose.
5. The official H/x calculated as above will be recorded along with the official H<sub>c</sub>, V<sub>c</sub> & M<sub>c</sub> at bottom of each data sheet

JMM 2/23/50.

Further dilution calculations:

To go to 240 H/x from 88

$$(240-88) \left( \frac{9}{235} \right) (1.505) (1.568) = 1.373 \frac{\text{cc water to add}}{\text{cc present solution}}$$

now Cyls #1-6 contain 4.6 cm at 0.604 g/cm or 2.77 liters each  
#7 is 1 liter less because of bottom plate or 1.77 and 3.6 liters (DV+2mm) mixed with 5.34 liters of water is in 8 & 9.

∴ Total solution of H/x = 88 was 23.0 liters to which (23.0)(1.373) = 31.58 l of water should be added. As 5.34 liters are in 8 & 9 already 26.24 liters should go into 1-7. Cylinders 1-6 require  $\frac{26.24}{6.64} = 3.95$  liters H<sub>2</sub>O each

$$\text{and \#7 } (3.95) \left( \frac{1.77}{2.77} \right) = 2.53 \text{ liters H}_2\text{O}$$

An H/x computation formula for  $\text{UO}_2(\text{NO}_3)_2 + \text{HNO}_3 + \text{H}_3\text{PO}_4 + \text{H}_2\text{O}$  has been derived:

let A = gms U / gms solution

B = moles N / moles U

C = gms X / gms U

D = moles P / moles U

molecular weights used

U 235

O 16

N 14

P 31

H 1

$$\text{H/x} = \frac{1}{1.0718} \left[ \frac{26.11}{A} - 6B - 7.89D - 31.44 \right]$$

Phosphate  
Nitrate  
Water  
Uranyl nitrate

This can be readily derived as before  
let m = moles H / moles U whence H/x = m/c

Considering the acids as anhydrides take

	MW	moles	weight
$\frac{1}{2}(P_2O_5)$	71	D	71D
$\frac{1}{2}(N_2O_5)$	54	B-2	54(B-2)
$VO_2(NO_2)_2$	391	1	391
$\frac{1}{2}(H_2O)$	9	m	9m

$$\begin{array}{r} 62 \\ 80 \\ \hline 142 \\ 71 \\ \hline \end{array}$$

-  $HNO_3$   
 $H_2O + N_2O_5$   
 $2 H_3PO_4$   
 $3 H_2O + P_2O_5$

$$\frac{\text{grams solution}}{1 \text{ mole } U} = \frac{235}{A} = 71D + 54(B-2) + 391 + 9m - 31.444$$

$$\text{whence } H/x = m/c = \frac{1}{c} \left[ \frac{235}{9A} - \left(\frac{71}{9}\right)D - \left(\frac{54}{9}\right)B + \left(\frac{54}{9}\right)(2) - \frac{391}{9} \right]$$

$$1.0718 \left[ \right]$$

New Dilution ~ H/X ~ 240

2/24/50

Experiment #395

105  
H/V ~ 200  
H<sub>2</sub>N<sub>2</sub>

Mosfitt  
Fox  
Mocklin  
Henry

15" Al Reactor Water Reflector sides only + 106 Tubes  
w/ source LDP-D-814, 5.6 filled to depth 27cm with Bismuth metal.

Source Zero at +1.5 cm.  
Source Set. @ 11.5 10 cm from bottom

Starting Inventory:

Cyl. #	1	2	3	4	5	6	7	8	9
cm in tube filled 15" reactor	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	6.0

Instrument	Start	Trip
3	x 10	98 x 100
4	x 20	—
5	x 5	—
6	x 25	5.8 x 1000
7	—	2" from source.

Time	Sol. H <sub>2</sub>	#1	#2	1/M <sub>1</sub>	1/M <sub>2</sub>	Remarks
1:00	12.6	9.5 } 9.0 } 9.0 }	4.5 } 5.5 } 5.0 }	1.00	1.00	
1:15	19.8	11.0	6.5	.84	.77	fill from #1
1:20	26.2	15.0	8.0	.61	.62	
1:25	30.0	18.5	12.0	.50	.42	fill from #2 at 29.2
1:30						Max. wt. of Bi. at 30.0
1:30	38.0	28.0	22.0	.33	.23	

Drawback: #1 10.5 cm in 15 cm with tubes (204 cm)

- 2
- 3
- 4
- 5
- 6
- 7
- 8
- 9

H<sub>c</sub> ~ 45

V<sub>c</sub> ~ 27.0

M<sub>c</sub> ~ 2.76

2.75 ✓

H<sub>1/2</sub> = 230

DV + 4.0 cm

Conclusion Critical above 40 cm.  
But extends criticality 45 cm

2/22/50

H/12240  
H.N.B.

Experiment # 396

Fox  
Macalini  
Moffat

15" Aluminum Reactor Water Reflector Sides only  
+ 106 open-end tubes in rack LDP 2814, 25, 6.

Source zone 1.5 cm Set @ 12 on scale.

Instrument	Start	Trip
3	x 20	92 x 100
4	x 50	—
5	x 2	—
6	x 25	5.8 x 1000
7	—	1 1/2" = .8

Time	Solu Hgt.	#1	#2	1/M <sub>1</sub>	1/M <sub>2</sub>	#9 MT @ 2.5
9:35	13.1	7.0, 6.0	6.5, 7.0	1.0	1.0	#8 MT @ 8.3
9:45	16.7	24	25.5	.27	.265	#7 MT @ 14
9:48	17.5	51.5	61.0	.126	.106	#6 MT @ 17
Red in		36.	40	.18	.17	from #1

rod worth 3-4 mm Expected critical 18.0

10:04	18.1	leaked base into #1 cylinder checked none OK				
10:14	17.95	133	164	.049	.041	
	18.35					

Conclusion: Critical on sight glass @ 18.15

zero cor.	- .20
Bot "	+ .40
Plate	- .95
Hc	17.90
Vc	18.47.7
Mc	1.90 ✓
H/x	= .290

1/2/50

### Exp # 397

H/X = 230  
H, N<sub>2</sub>

Fox  
Henry  
Moeckli  
Kestel  
Rohr

15" Aluminum Reactor. Water Reflector Sides only.  
+ 106 closed end tubes in 106 LDP-D 814, 5, 6.  
Source 220 @ 1.5    St @ 17 cm.

Sources & Instruments same as #396

Time	Tube Height	#1	#2	X 1/4"	⊙ 1/4"	Range
1:26	17.8	11.0	6.0	1.0	1.0	9 MT @ 40
1:31	25.6	14.0	6.5	.79	.82	8 MT @ 140
1:40	32.0	18.0	9.0	.61	.67	7 MT 21.0
1:48	39.9	23.0	14.0	.48	.43	6 MT 29.0
2:00	50.1	32.5	22.0	.34	.27	1 MT 39.9
		33.0	22.0	—	—	2 MT 18.0
2:18	59.8	48.5	36.0	.23	.17	3 MT 59.6
2:40	69.5	47.0	61.5	.14	.09	4 MT

Critical @ > 80 cm if at all.

Best estimate of criticality 85 cm.

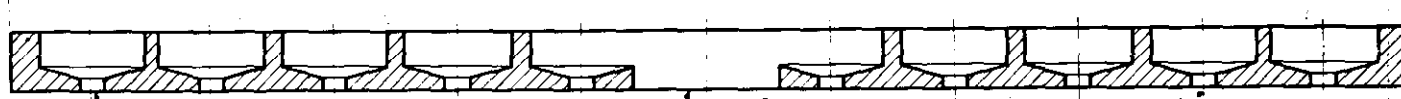
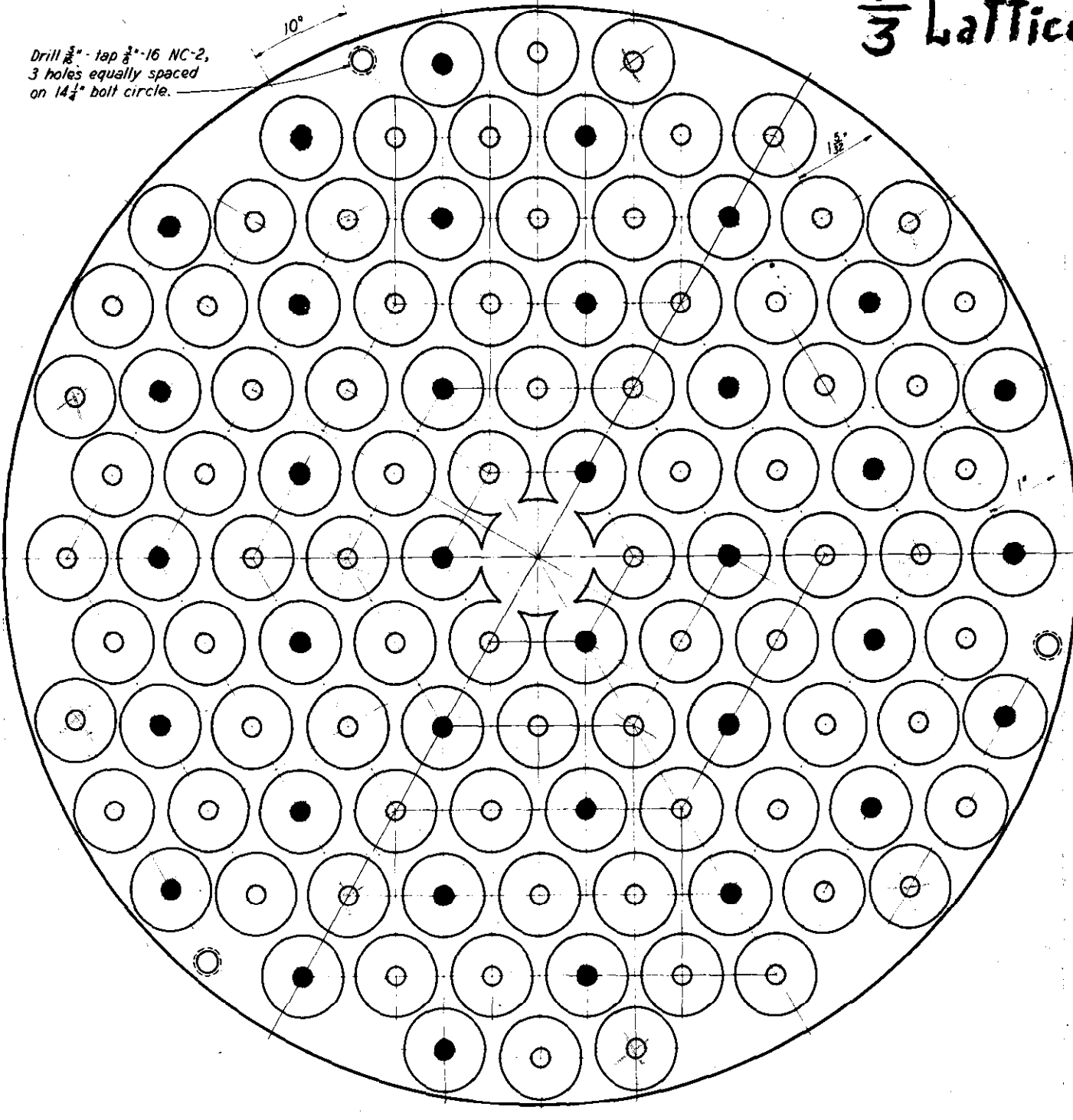
Inventory	1	2	3	4	5	6	7	8	9
cm in 15" 106 vial	9.5	10.0	10.0	10.0	10.5				

H<sub>c</sub> ~ 85  
V<sub>c</sub> ~ 51.2  
M<sub>c</sub> ~ 5.2 ✓

$$H/X = 230$$

# $\frac{1}{3}$ Lattice

Drill  $\frac{1}{8}$ " - tap  $\frac{3}{8}$ " - 16 NC-2,  
3 holes equally spaced  
on  $14\frac{1}{8}$ " bolt circle.



Drill  $\frac{1}{8}$ " thru - counter drill  
 $1\frac{1}{8}$ " x  $\frac{1}{8}$ " deep - 106 holes  
on same center pattern  
as Guide Plate.

Drill  $1\frac{3}{8}$ " thru center

$1\frac{5}{8}$ "  
 $2\frac{3}{8}$ "  
 $3\frac{1}{8}$ "  
 $5\frac{1}{8}$ "  
 $6\frac{3}{8}$ "

Material:  
 $\frac{3}{8}$ " 3S Aluminum plate.

## CM TUBE RACK - BOTTOM PLATE -

Allen *QUM*  
LDP-D-816  
2-2-50

7/28/50

Exp. #398

109  
H/X 240  
H. No 3

Fox  
Macelin  
Murphy  
Rohr.

15" Al Reactor Tamped Solid only, Containing 36 voids  
as per print p 108. H/X = 240  
Source @ 11.5 cm.

Instrument	Start @	Trip @
3	X 10	92 x 100
4	X 20	—
5	X 2	—
6	X 25	5.8 x 1000
7	—	— 2" (By pass)

Time	Ht.	#1 (11.25)	#2 (9.25)	X 1/4	⊙ 1/4	Remarks
9:22	12.5	11.0, 11.5	7.5, 7.0	1.0	1.0	#9, 8 HT.
9:36	17.25	17.5	11.5	.64	.63	#7 @ 15 cm.
9:41	22.5	193	137	.058	.053	
	Blade in	92.5	—	.121	—	Slipped from #6
9:55	23.2	Critical with rod @ at 20.				
	<del>23.1</del>	Critical " " @ 30				
9:59	23.0	Subcritical with rod out.				

Conclusion: critical @ 23.05 cm. on sight glass.

$$36 \times 5.06 = 182$$

$$+ rods \quad \underline{\quad 2 \quad}$$

$$\underline{\quad 184 \quad}$$

$$1190$$

$$\underline{184}$$

$$956 \text{ cm}^2$$

zero cor.	- .20
flat cor.	+ .40
plate	<u>- .95</u>
Hc	22.30
Vc	21.3 ✓
Mc	2.17 ✓

$$H_c / X = 230$$



7/2/50

Experiment #399

H/4  
~240  
H. No

Fof  
Macklin  
Mafed  
Rohr

15" Al Reactor Temped. ~~Top~~ Side only +36 tubes  
filled with 250 cc. tubes spaced on per #108.  
Source @ .6m from bottom. Instruments same as exp #398.

Time	Soln Hgt	#1	#2	1/4"	1/8"	Remarks	
11:10	7.8	8.5 ✓	4.5 ✓	1.0	1.0	#9 & #10	
11:20	12.0	13.0	7.0	.65	.65		
11:33	16.0	31.5	20.5	.27	.22		
	Rod in	29	—	.29	—		
11:37	17.1	56	37	.15	.121		
11:47	18.0	204	147	.042	.030		
	Rod in	120	—	.071	—	0.2 min.	
	18.3+	Silent with rod out.					
11:50	18.5-	Rod @ 20 cm.					

Conclusion:

Critical with slight glow @ 18.40 cm.  
Total cor.

$$\begin{aligned}
 H_c &= 17.65 \\
 V_c &= 16.87 \times 1.1 \\
 M_c &= 1.72 \text{ kg} \checkmark
 \end{aligned}$$

$$H/x = 230$$

2/28/50

Experiment #400 -  $H/K \approx 240$  H<sub>2</sub>O

Maceoin  
Fox  
Moffatt  
Robin

15" AI Reactor Tamped Sides only + 106 tubes  
filled with 250 cc H<sub>2</sub>O. See layout on p 108  
Source set 8cm on scale

Time	Solu Hgt.	#1	#2	$\frac{1}{H_1}$	$\frac{1}{H_2}$	Remarks
2:44 - 2:55	10.2	7.5 (29)	3.0	1.0	1.0	A9 HD. 47
3:00	17.0	15 (19)	7.0	.50	.43	H7 HT @ 14
3:06	19.5	22.5 (16)	11.0	.33	.27	Tube #6
3:18	22.0	47.5 (28)	27.0	.158	.111	5 stopped
3:27	23.8	188 (57)	125.0	.040	.024	
	Rod in	95	—	.079	—	
3:38	24.4	Critical Rod @ 20.0				
3:42	24.3	Subcritical with rod out.				
3:44		237 (27)				

Conclusion: Critical with sight glass @ 24.35  
 Total Correction  $\frac{-1.75}{23.40}$   
 $H_c = 23.40$   
 $V_c = 19.2 \text{ #6}$   
 $M_c = 1.45$   
 $\frac{H_c}{K} = 230$

112 3/2/53  
Fox

Exp # 401  $\text{H}_2\text{NO}_2$   $H/X \approx 240$

Marlatt  
Robson

15" Al Reactor Water Tamped sides only + 36 tubes  
filled with Bi spacers as per page 108  
Source @ 10 cm scale 8 1/2 cm from bottom.

Instrument	Set @	Frip @	
3	x10	78x100	#9 MT @ 48
4	x10	—	
5	x1	—	
6	x25	6x1000	
7	—	0.76	

Time	Solu Hgt.	#1	#2	$\frac{1}{M}$	$\frac{1}{M}$	Remarks
9:52	10.4 10.6	10.0 9.15 ✓	4.0 3.0 (3.5)	1.0	1.0	#9 MT @ 48
10:25	15.2	15.0	7.0	.63	.50	#7 MT 9.0
10:42	15.4, 15.6, 15.8 on 6/ow back	36.0	17.0	.265	.205	#7 MT
10:50	20.0	100.5	53.0	.095	.066	
	<del>20.8</del>	60	—	.16		
11:10	21.0	Subcritical for with rod out.				
		Critical. 17 cm up from bottom				

Conclusion out at 20.95

Total correction - .75

$$H_c = 20.20$$

$$V_c = 19.34 \checkmark$$

$$M_c = 1.96 \checkmark$$

$$H/X = 230$$

3/2/50  
Fox  
Moulin  
Mortill  
Rohrer  
Rohrer

Experiment #402A

H<sub>2</sub>NO<sub>3</sub>  
H/X = 240

15" Al Reactor <sup>Completely</sup> Water Tamped H<sub>2</sub>NO<sub>3</sub> H/X = 240

last runs as per #401

Source 6 cm from bottom.

Time	Solu Hgt	#1	#2	1/4"	1/8"	Remarks
1:54	8.0	6.5, 7.0	3.5, 3.5	1.0	1.0	9AT @ 1.8
2:02	11.1	20.5	8.0	.34	.44	8AT @ 7.0
2:12	12.0	38.5	17.0	.175	.205	7AT @ 12.0
2:20	12.6	81.5	42.5	.084	.082	6 reading
2:27	13.2	35				Red in Taper up
	13.0	Critical	Taper down			Red @ 10 cm
	12.9	Critical	" "			Red out
		Sub "	" "			" "

402B  
Top Taper raised to 63 cm.

2:48	12.9	13.5	10.0	.50	.305
2:55	14.0	25.0	15.0	.27	.23

Comparing results here with that of exp 389A4B gave rise to possibility of height of water in taper tube affecting critical height of system with top tapered up. Accordingly raised source to 12.9, added water to fill taper tube &

3:04	14.0	23.5	12.0	.27	.23
3:07	15.0	67.0	37.0	.10	.095
3:10	Red in	40		.17	
3:12	15.5	Critical	with red out.		
3:13	15.4	Subcritical			

402-A  
out. Ht. 13.0  
correction + .2

402-B  
crit Ht 15.5  
cor. +.2  
Hc = 15.7  
Vc = 17.90 ✓  
Mc = 1.82 ✓

Repeat of Darcy correction { 2.5 mm.  
2.0 mm

Hc = 13.2 ✓  
Vc = 15.0 ✓  
Mc = 1.53 ✓

114 3/2/50

H/X = 240  
H: NO<sub>2</sub>

Fox  
Macklin  
Mortitt  
Rohr  
Rohrer

Experiment # 403

15° Reactor Untarped.

Sources & instruments as per # 401  
Benz. 17.0, 9.0

Time	Solu H <sub>2</sub> O	#1	#2	X 1/4	⊙ 1/4	Remarks
3:15	15.7	51	28	.333	.32	
3:22	17.9	86.5	56	.195	.16	#6 H <sub>2</sub> O @ 18.7
3:30	20.0	149.0	112	.115	.08	from #5
	22.0	527.5	442	.022	.020	
3:42	Rod in		315	.055		
3:47	22.65	Substantial Rod out,				
3:48	22.8	Graded Rod @ 15 cm. (close to critical than above)				

Conclusion: Critical with sight glass @ 22.7 cm.  
Total correction .0

$$H_c = 22.7 \text{ m}$$

$$V_c = 25.8 \text{ L}$$

$$M_c = 26.3 \text{ kg}$$

$$H/X = 230$$

3/3/50

115  
H.H. ~ 2460  
H. 103

# Experiment #404

For 12" Reactor Tamped.

Machin  
Merrill  
Rohrer

Source set at 6 cm from bottom -

Instrument	Set	Temp @
3		87 X 100
4		_____
5	X1	_____
6	X25	6 X 1000
7		"
Beyond Tamped	#1	2.0, 2.0
"	#2	17.0, 17.5

Time	Set Ht.	#1	#2	1/4"	1/8"
10:40	8.0	5.25	2.0	1.0	1.0
11:08	12.5	10.5	5.5	.50	.36
11:15	14.5	30.0	18.0	.175	.111
11:24	15.0	51.0	29.0	.103	.069
11:32	15.8	Subcritical rod @ 12 cm Taper down.			
11:35	15.65	" " " 20 cm Taper down.			
	15.50	Barely subcritical.			

9 MT, 7 MT  
@ 9.5 cm h

Stopped 6  
from 3

Conclusion Critical @ 15.5 cm on Sight Below

geo. cor. +.7  
 Bot. cor. +.6  
 $H_c = 16.8$   
 $V_c = 12.2^{1.3} \text{ m}^3$   
 $M_c = 1.25 \text{ kg V}$   
 $\#/2 = 2.30$

Exp # 405

Fuf  
Maxlin  
Murtin  
Robber

12" Reactor Untamped

Source + Instrument Same as #404

Time	Beagm. Hgt.	#1	#2	X	⊙	
1:04	15.4	37.38	24.5	.58	.70	#6 M7 @ 20.0
1:12	20.2	67.5	51.5	.30	.33	
1:19	22.9	91.5	77.0	.24	.22	from #5
1:40	27.4	183.5	163.0	.12	.104	#5 M7 @ 20.0
1:48	29.8	389.5	371.0	.056	.045	
	Red in "	230.0	—	.074	—	
1:53	31.2	Too high to count.				
2:01	31.95	Critical Rod @ 26 cm.				
2:04	31.70	Subcritical Rod out. (Barely)				

Conclusion Critical at 31.75 cm on signal glasses.

	1	2	3	4	5	6	7	8	9
cm in 12" of	~9	~9	~9	~9	~9.2	9.1	9.2	8.0	DV + 2.0
~730 cm <sup>2</sup> liters	6.55	6.55	6.55	6.55	6.70	6.63	6.70	5.82	4.96

{Soup at zero - tamper water drained}  
SG reading = 0.5 cm.

right plane. 31.75  
zero cor +.5  
Det. " +.4

$H_c = 32.25$

$V_c = \frac{24.0}{23.9} \text{ tel.}$

$M_c = 2.44 \text{ kg. } \checkmark$

$H/x = 230$

3/6/50

Exp # 406

117  
H/H ~ 240  
Hi NO3

Henry  
Hickman  
Kert. H  
Rohr  
Rohrer

10" Reactor Temped

Source @ 8 in from bottom. Zirc @ 1.5

Instruments	Start	Trip
3	X10	90 X100
4	X10	—
5	X1	—
6	<del>—</del> out	—
7	—	1 1/2" .72

Time	Sub	Untemped	Temped	21.0 ✓	16.0, 15.5 X	2.0, 1.0 1.0 ⊙	
<del>10:40</del> 10:40	7.5	4.0 ✓	1.0 ✓	1.0	1.0	1.0	#947
10:50	14.1	6.0	2.5	.67	.40		at 15.5
11:02	16.9	8.5	5.0	.47	.20		from #7
11:14	19.8	27.5	17.5	.163	.057		from #6 for 16.3
11:25	20.8	71.5	47.5	.085	.052	.021	Est. crit 21.5
11:32	21.5	Critical Temp down Rod @ 17cm.					
	21.3	" " " " " " " "					
11:39	21.1	Subcritical " " " " " " " "					

Conclusion: Critical @ 21.2 on sight glass.

Zero +.5  
Bolter +.9

Hc = 22.4  
Vc = 11.45 l  
Mc = title kg.  
1.17



704

Exp # 407

Henry  
Maxwell  
McFell  
Rohr  
Robner.

10" Reactor Untamped.

Source, instruments & background same as #406.

X O

Time	Solu Hgt.	#1	#2	1/4	1/2	Remarks
	<del>9.5</del>	<del>43.5</del>	<del>25.0</del>			
	9.5	21.0	15.8	1.0	1.0	
1:25	19.8	43.5	25.0	.48	.62	#6MT @ 29.5
1:34	25.1	56.	37.5	.375	.42	
	30.5	70.5	49.	.30	.32	#5MT @ 43.
2:20	44.8	106.0	86.0	.198	.184	
2:30	54.9	135.0	113.0	.156	.140	#4MT @ 52.
2:44	71.9	178	168.	.118	.094	#3MT @ 63

Maximum advisable height in cylinder

Best Estimate of criticality 105-115 cm by extrapolation  
 Probably safe  $H_c > 165$ ,  $V_c > 53$   $M_c > 5.4$   
 with Solution at reactor zero - Taper drained  
 Sighted glass read = 0.3 cm.

Dilution calculation - targeted #/X = 350

Phoned analysis: Sample 830128 is 0.08851 gm<sup>0</sup>/gm solid

See formula  
Pg 101

$$\therefore \text{present } \#/X \text{ is } \frac{1}{.933} \left[ \frac{26.11}{0.08851} - 6(6.98) - 31.44 \right] = \frac{1}{.933} [294.99 - 41.88 - 31.44]$$

↑  
modified values

$$= \frac{221.67}{.933} = \boxed{237.6}$$

Water to add is

$$(350 - 237.6) \left( \frac{9}{235} \right) (1.230) \left[ (0.08851)(0.933) \right]$$

$$= \frac{(112.4)(9)(1.230)(.08258)}{235} = \frac{(1011.6)(0.1016)}{235} = \frac{102.8}{235}$$

$$= \boxed{0.437} \frac{\text{cc water to add}}{\text{cc present solution}}$$

max needed = 37 l. for 12" untamped + 4V or 6 cyls active impit  
 of present soup  $\frac{37}{1.437} = 25.75$  l. is needed for dilution  
 or 4.29 l. in each of 6 cyls + add 1.875 l. water. (check)

3/7/50

Dilution continued

4.29 l per cyl is  $\frac{4790}{506.6} = 8.95$  & record 0.05 cc

9<sup>45</sup>

#2 completely filled #7 full from yesterday #1 & 9 RT

#2 & #7 removed

310 on to 4E

150

Drew 8.5 cm into #1

add H<sub>2</sub>O

" 8.5 cm into #3

after emptying

1.875 L

206

" 8.5 cm into #9

1.875 L

" 8.5 cm into #4

" "

1.880 L

" 8.5 cm into #5

" "

1.875 L

" 8.5 cm into #6

1.875 L

#1 & #3 need further mixing. i.e. some of #1 water went in #3  
∴ pool #1 & #3 & mix these two together in reactor before adding others.

dilution completed in #s 1, 3, 4, 5, 6, 9  
[after A, C, E, F, G, B] others M, H, J, D, Q  
empty #2  
to ship

3/9/50

Inventory & H/x sample troubles Cyl M resampled 3/8 gave colorimetric analysis 0.141 checking the 0.1339 taken on solution before putting it into M. This was from #9 & ∴ expected to be typical of pit & official for H/x. Recalculations of volumes I'd made it apparent that the pit soup volume was if anything smaller than the original Y-12 shipment volume ∴ H/x = 88.0 computed (p.101) therefore is declared official for expt. 384 - 392. (393 & 394 for 2 quats)

Tentative explanation is pptn of UNH on walls of cyl 9 before samples 830126 & 830127 were taken & solution transferred to cyl M.

Cyl. P in no. 2 position, position 7 & 8 empty

3/9/50

Exp 408  
~~Exp 408~~

$H/X \approx 350$

J.W. Morfitt  
J. Fox  
R. Macklin  
C. Schuske

10" reactor ~~emptied~~ untamped  
Run primarily for mixing purposes.

Injunct

Instrument no. 6 at 6 x 1000  
" 3 at 90 x 100  
Photo mult. at 7" approx

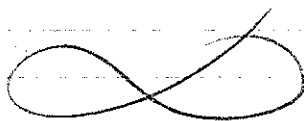
preliminary mixing - no side tamping, top lamps at 70 cm.

Time	Sol. Ht.	#1	#2	$1/M_1$	$1/M_2$	Remarks
1:00	18.3	41.0	20.0	1	1	#1 & #3 empty
1:05						feeding from #4
1:55						working on leak
2:20						leak fixed
2:24	30.5	96.0	39.5	.427	.507	+ mixing contained
2:33	42.3	81.0	56	.479	.351	#4 empty
2:40	54.8	97.	69	.424	.290	
2:50	66.9	106	74	.387	.270	air in line (in 3 min)

Drain back

1	3	4	5	6	7	
4.4 + D.V.	12.5	12.5	12.5	12.5	12.2	Err in 10" reactor

Conclusion: infinitely safe (multiplication probably less than 5 at  $H=0$ )



3/10/50

Experiment # 409

Fol.  
Macklin  
Morfitt  
Henry

10° Reactor Tamped  $\frac{H}{X} \approx 350$   $\frac{H}{X} \approx 7$

Strip Points: #3 91 x 100 Source: 10cm. from bottom  
 #6 5.8 x 1000  
 PM .74 at 1.5 in.

Time	Sol. Ht.	M <sub>1</sub>	M <sub>2</sub>	$\frac{M_1}{M_{10}}$	$\frac{M_2}{M_{20}}$		
10:50	13.8	4.5 } 4.5 4.5 }	1.5 } 1.5 1.5 }			#1 MT at 4.0 #9 MT at 16.0 Fill from #3	
11:10	18.2	7.0	2.5	.64	.60		
12:10	24.0	20.0	12.0	.22	.12		
12:20	25.5	43.5	26.0	.103	.058		
		Rod in 15.0		.30			
12:30	27.05	Critical with rod at 22.0 (3.5 in soap + 15.0 in tamped)					
	26.85	Critical (slightly spaw)					
	26.55	Subcritical					

Conclusion: Critical at 26.75 cm.

1 3 4 5 6 9  
 12.0 12.5 12.5 12.5 12.5 4.8 + D.V.

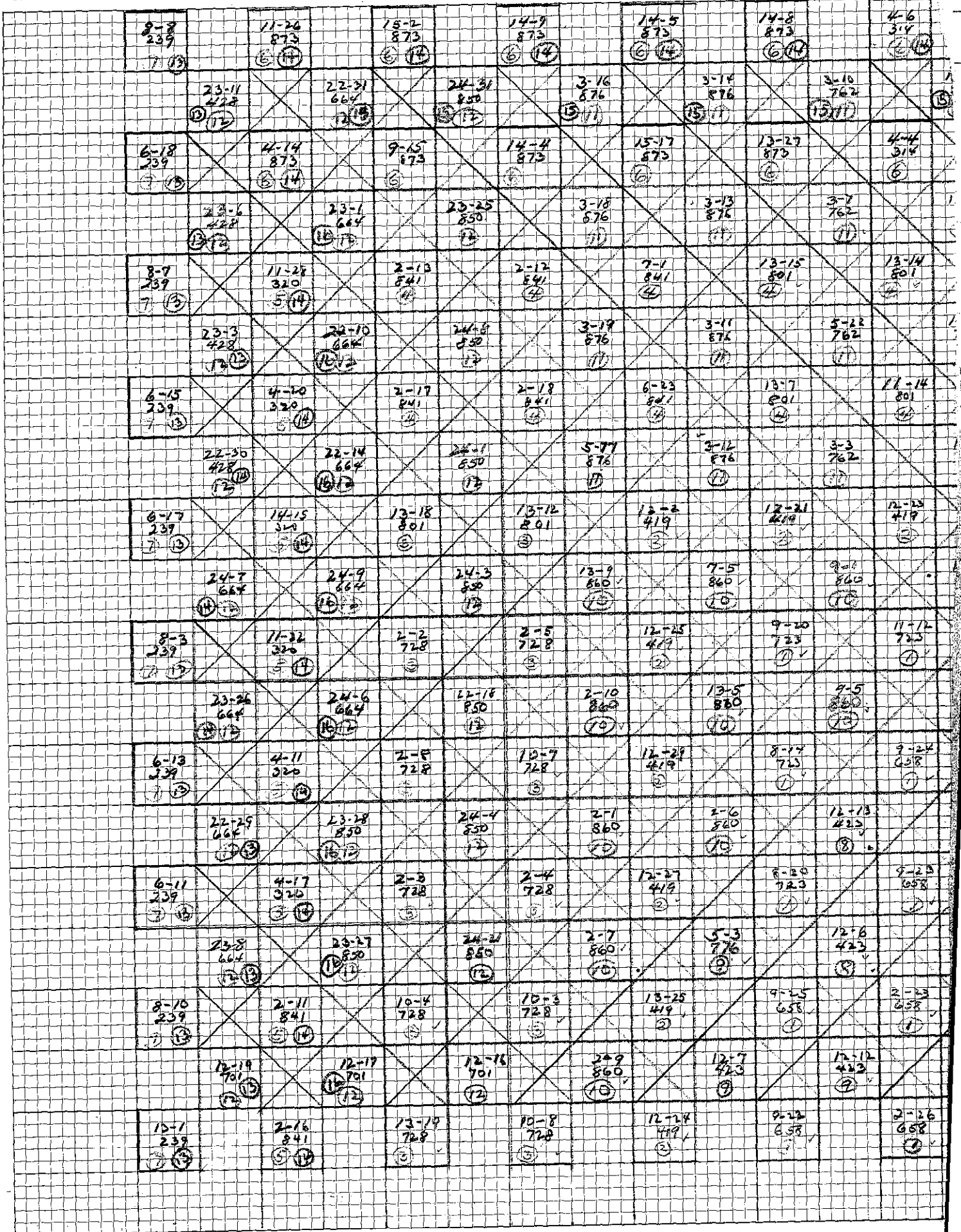
st. Hl. 26.75  
 Total cor. 1.90  
 $H_c = 28.65$   
 $V_c = 14.23$   
 $M_c = 1.05$

Top

EUGENE DIETZEN CO.  
MADE IN U. S. A.

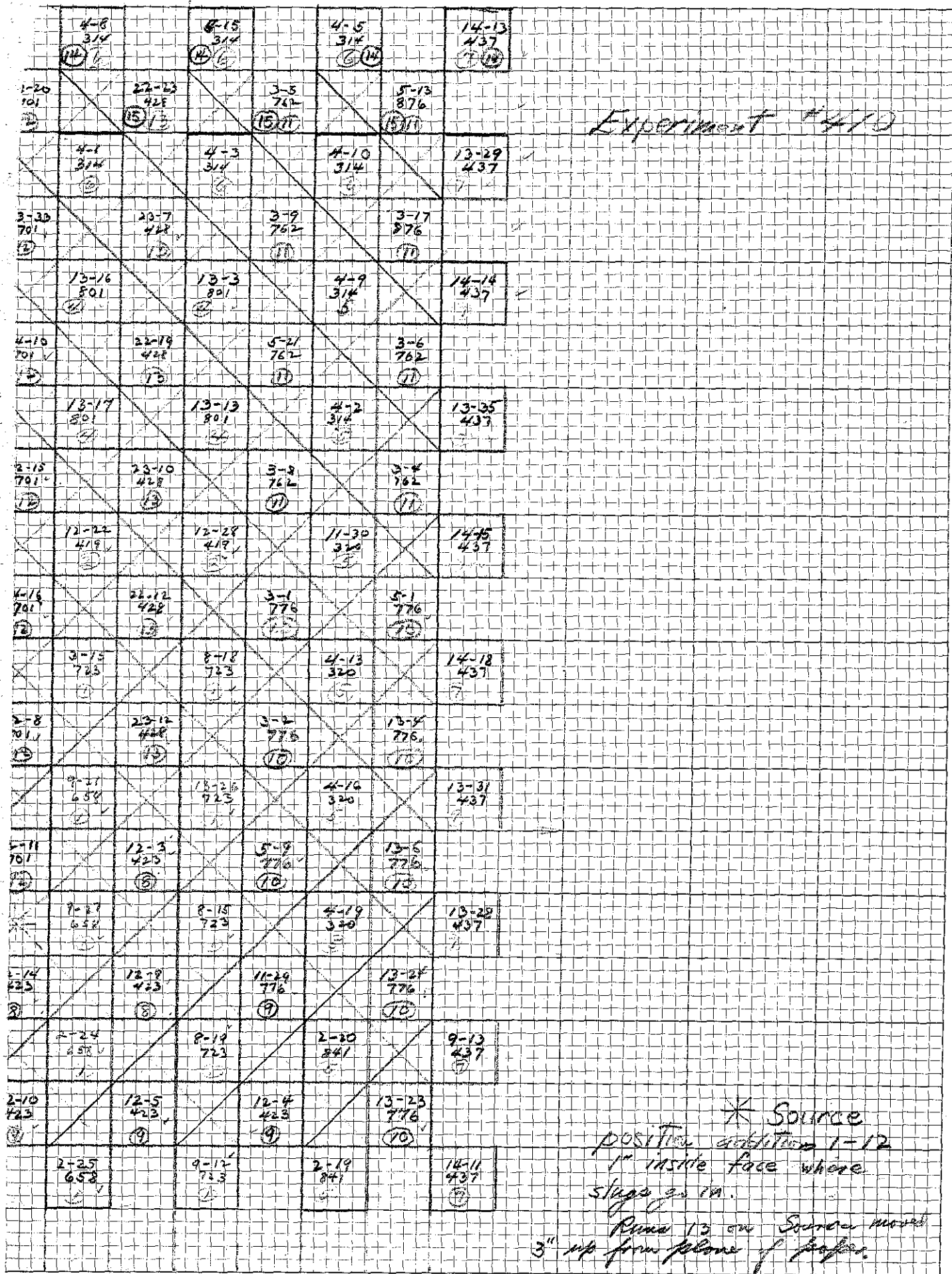
NO. 340DR-10 DIETZEN GRAPH PAPER  
10 X 10 PER INCH

*Remains*



Bottom

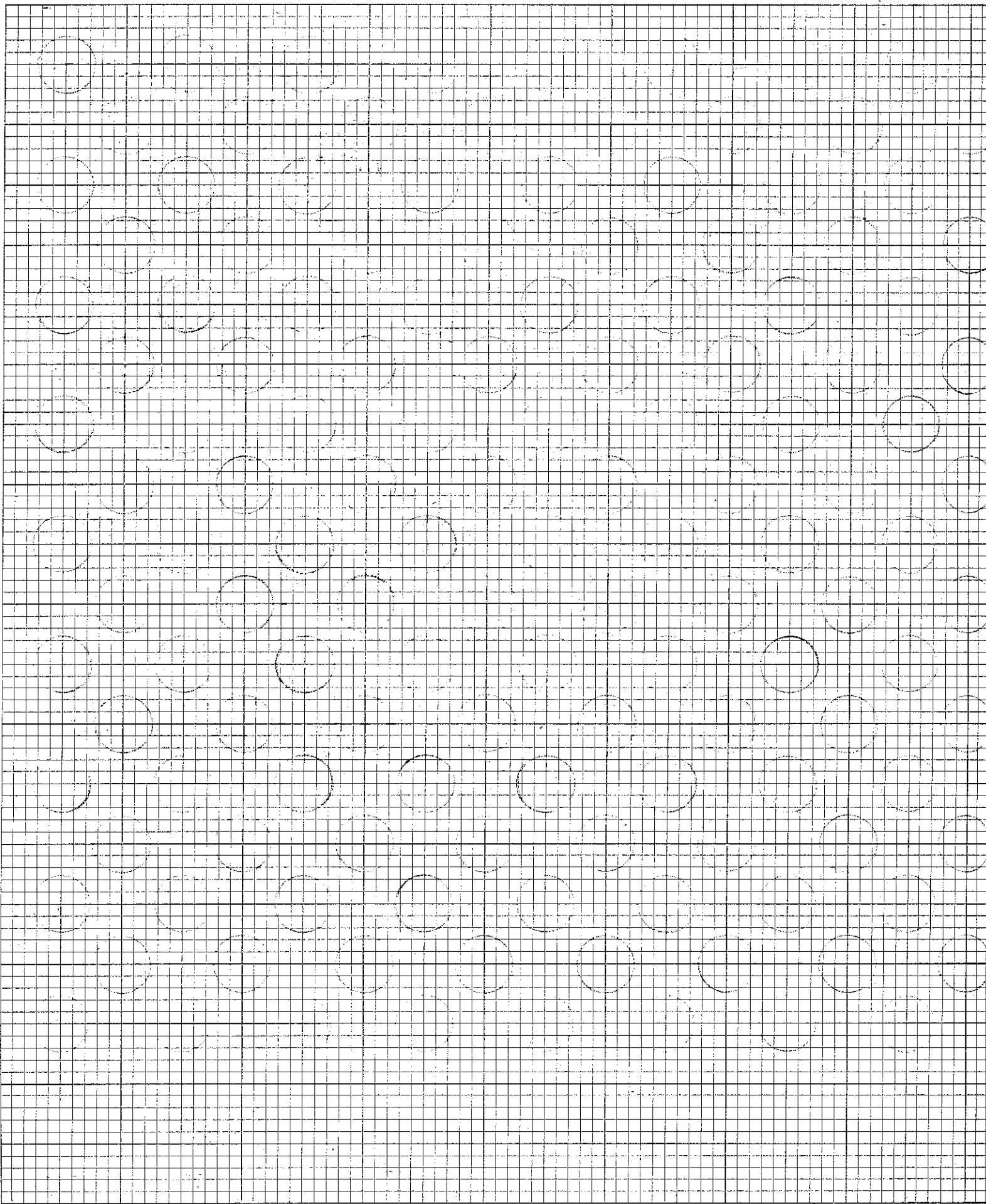
*Cont.*



Experiment #410

Closed End

\* Source position addition 1-12 1" inside face where slugs go in.  
 Run 13 on Source moved 3" up from plane of paper.



11  
11

MADE IN U.S.A.  
EUGENE DIEZGEN CO.

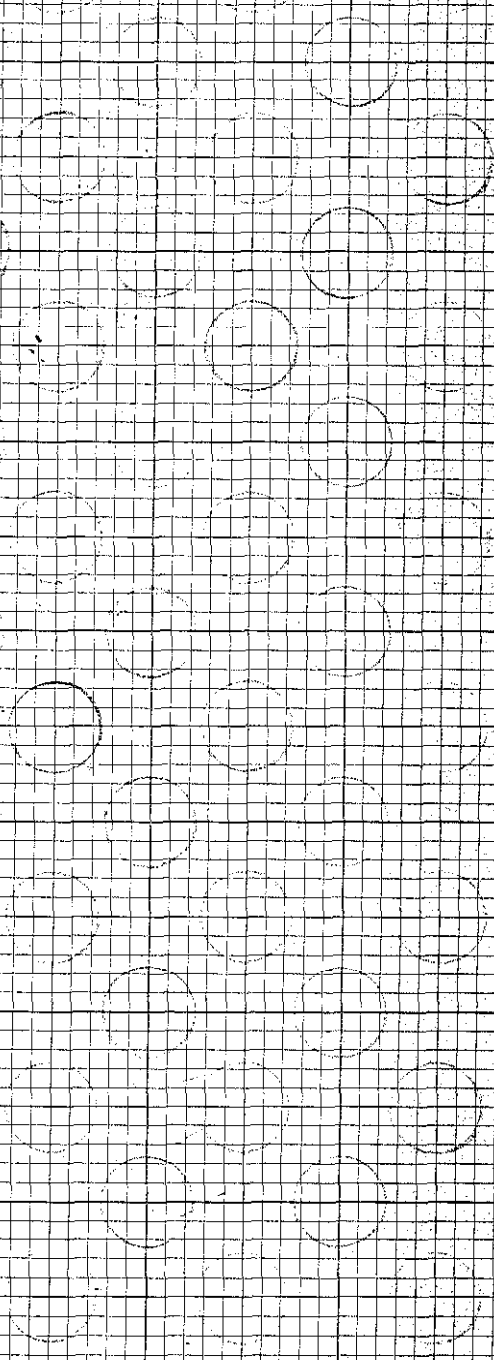
EUGENE DIEZGEN CO.  
MADE IN U.S.A.

NO. 340DR-10 DIEZGEN GRAPH PAPER  
10 X 10 PER INCH

NO. 340DR-10 DIEZGEN GRAPH PAPER  
10 X 10 PER INCH

Cont.

Expt #410  
Critical Array 145 Slugs  
Scale  $\frac{1}{3/8}$



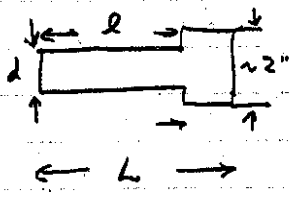


EXPERIMENT # 410

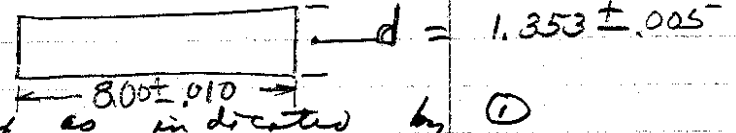
3/12/50.

MACLEIM  
McLENDIN  
MURPHY  
CALLINAN

To test criticality, if any, of array of U-235 slugs  
Slugs are ~~1.36"~~  $1.41 \pm 0.05"$  diameter =  $d$ ;  $l = 8.0 \pm 0.5"$   
 $L = 9.375 \pm 0.125"$

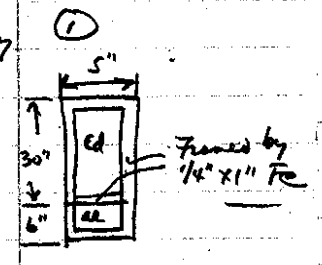


FINISHED SLUG



20 slug mounted in Lucite matrix as indicated by  
on attached plot -

- Cd safety sheet - 5" x 30" cad<sup>cd</sup> suspended by magnet
- 2 Cd control sheets - 2 12" x 30" (same as safety except 12" wide).



TRIP PTS	TRIP	SCALE
#3	92 x 100	x 10
#7	OK. (1.5")	-
#6	5.7 x 1000	25
#4	-	$\frac{100}{50}$
#5	-	2

Source - 7 cur on pebble - see chart for position in lattice.  
Control Rods zero = #1 = 0  
#2 = 3.5 cur (compensator at 88 cur).

Cont -

\* 410 (Cont)

Time	Conditions	Water	C <sub>1</sub>	C <sub>2</sub>	Applied	1/μ <sub>1</sub>	1/μ <sub>2</sub>
12:01 P.	20 Slugs No water		33.0	20.0			
12:28 P.	20 Slugs Source Covered	Water Gauge 38.6 cm	35.0	20.0	①		
12:38 P.	20 Slugs Covered	Water Gauge 75.5 cm	10.5	57.5	①		
			2.25	8.75			
			3.25	8.00	①	1.0	1.0
1:19 P.	30 Slugs No water		31.0	18.5	① + ②		
	Source Covered	WG 38.6 cm	9.0	8.5			
	30 Slugs covered	WG 83.5	2.5	1.00		~1.0	~1.0
						#1 34.0	#2 20.0
						#1 10.5	#2 7.0
						1.75	1.25
Time	Condition	Water	C <sub>1</sub>	C <sub>2</sub>	Applied	1/μ <sub>1</sub>	1/μ <sub>2</sub>
1:48	42	0	35.00	18.5			
1:52	42	38.5	10.5	9.5			
1:58	42	83.5	2.5	1.05			
2:08	56	100.	2.25	1.00			
2:18	72	100	2.25	1.00			
2:28	90	Full!	2.5	1.50			
3:00	110	0	38.5	21.5			
3:17	110	Full!	1.75	1.25			
3:20	115	38.0	16.25	12.5	Σ <sup>8</sup>	.65	.56
			3.25, 2.50	1.75, 2.00		.54	.62
			← counter occasionally counts 64. Most of time 40				
4:20	122	0	35.5	21.5	Σ <sup>9</sup>		
4:35	122	Full!	2.5	3.6			
4:40	122	"	3.6*	2.5	Σ <sup>9</sup>	.485	.500
4:55	140	0	22.0*	21.5	Σ <sup>10</sup>		
5:20	140	Full!	5.3*	4.0	Σ <sup>10</sup>	.333	.310
5:25	<del>140</del> 160	Full!	6.5*	4.75	Σ <sup>10</sup>	.269	.263
5:55	194	0	20.0*	23.	Σ <sup>11</sup>		
7:15	194	Full!	-	180	Σ <sup>12</sup>		
7:25	184	with one blade in & one blade @ ~20 cm					
		At this point the slugs were rearranged.					
		Now in lattice:					
		All positions filled EXCEPT three marked with green ⑬! This gives total of 184 slugs.					
		Safety Red was removed & source placed in some position as to height & lengthwise along lattice but moved about 3" towards face of lattice where slugs are inserted.					
		* by actual count of interpolation around instrument faulty.					

Time	Number Slugs	Wats Gage	Control Rod 1	CR #2	
7:37	184	80	48	0	Critical
<del>7:40</del>	<del>162</del>				Source Out.
7:40	162				All positions except GREEN (13) & (14)
8:00	162	85			Subcritical Rods & Source Out.
8:14	153				All position with GREEN (13) (14) (15) Removed.
8:16	153	82.5			Subcritical
8:17	153	86.1			Critical @ 45.5 Rod #1 Method in.
8:22	145	Water <sup>98</sup>			Critical Rods at source out Appears to be critical or slightly supercritical

See sketch of loading positions & loading schedule on following pages.

Conclusion:

145 slugs in 9x9 square lattice  
+ 8x8 lattice four centered with  
neighb to above is critical slow  
completely water topped.

3/14/50

Experiment #411

Crosby  
Fof  
Macklin  
Mortill  
Robb

12" Reactor Untamped  $H/X \approx 350$   $M/U \approx 7$

	Start @	Trip @
#3	X100	85 X 100
#4	NG	—
#5	X1	—
#6	X25	6 cm $\times$ 8 cm sensitive
#7	—	1 1/2"

Background for <u>Tamped</u>		
	5.5, 5.0	#1
	2.5, 3.5	#2
Background for <u>Untamped</u>		
	28.5, 26.5	#1
	21.0, 19.0	#2

Time	Solen Key	#1	#2	X	⊙	Remarks
10:37	10.1	27.5	20.0	1.0	1.0	9MT @ 2.5
10:45	19.9	39.5	26.0	.70	.77	6MT @ 11.0
11:00	32.2	327.0 323.0	218.0 215	.084	.092	5MT @ 19.9
11:24	Rod in.	244	145	.125	.138	4MT @ 28.5
		Rod write 5 mm				Stopped #3 from #1
11:28	33.5	404	277	.068 -.066	.072	
11:37	35.7	670 400	466 290	.041	.043	Rod write 1.9 cm.
11:50	38.7	Sub-critical Rod out.				
	39.3	Critical with CR at 31 cm from bottom				
	39.1	" " CR at 35 cm				
	38.8	Sub-critical				

Critical at  $38.9 \pm 1$  mm on sight glass.

+ .7  
+ .6

$H_c = 40.2$

$V_c = 29.3 \text{ L}$  ✓

$M_c = 2.14 \text{ kg}$  ✓

$H/X = 327$

128 <sup>3</sup>/<sub>14/50</sub>

Experiment 412

12" Reactor Tamped  $\frac{1}{4}$ " to 350  $\frac{1}{4}$ " to 7

Crowd  
Pot  
Machin  
Muffin  
Rohr

Instrument & Sources as in 411.  
14.85 cm before long. 14.6 after long.

Time	Soln Hgt.	#1	#2 <sub>25</sub>	$\frac{1}{M_1}$	$\frac{1}{M_2}$	Remarks
—	10.6	3.25	<del>3.0</del>	1.0	1.0	#4 & 6 M.T.
<u>1<sup>15</sup></u>	14.6	8.0	<del>3.0</del>	.65	.83	from #5
<u>1<sup>24</sup></u>	18.0	46.	21.0	.114	.119	
	Rod in	17.0		.31		stopped #5 from #3
<u>1<sup>32</sup></u>	19.2	Supercritical		Rod @ 10		
<u>1<sup>34</sup></u>	19.0	"		Rod @ 13		
<u>1<sup>36</sup></u>	18.8	"		Rod @ 18		
	18.6	"		Rod @ 20		
	18.4	Sub-critical				
	Critical at 18.5 ± 0.1 cm on sight glass.					

Sight Glass reads 0.7 cm below 0 cm scale when soln level is reactor at zero & no water in tower tank.

$$\begin{aligned}
 \text{st. ht.} &= 18.58 \\
 \text{zero} &= .19 \\
 \text{Bot.} &= .6 \\
 \hline
 H_c &= 20.0 \\
 V_c &= 19.59.6 \checkmark \\
 M_c &= 1.07 \checkmark
 \end{aligned}$$

$$H_c = 327$$

3/15/50

Experiment HB

Fox  
Richardson  
Morrill  
Borkus

15" Reactor Tamped  $\mu/x = 350$   $\mu/u = 7$

Background for Tamped	#1	#2
" " Untamped	8.0	2.0
Source @ 5 cm from bottom	7.0	2.0
	#1	#2
	25	9.5
	25	9.5

Solution Inventory

#1	#3	#4	#5	#6	#9
5	5	5	4.5	5	DV + 1 cm

Instrument	Start @	Traps @
3	x10	85x100
4	N6	—
5	x2	—
6	x25	6.1 x 1000
7	—	1 1/2"

Time	Solu Hgt.	#1	#2	$\mu/x$	$\mu/u$	Remarks
9 <sup>30</sup>	7.5	7.5	2.0	1.0	1.0	#9 MT #6 MT
* 11 <sup>07</sup>	12.1	20.5	5.5	.37	.45	from #5 MT @ 120
11 <sup>24</sup>	13.4	32	10.0	.235	.20	from #4
11 <sup>22</sup>	14.5	92.5	32.5	.081	.0615	
	Rod in	38	11.5	.188	.174	
11 <sup>35</sup>	15.1					Critical Temp Down Rod @ 15 cm
11 <sup>37</sup>	14.9					" " " " " 20 cm
11 <sup>39</sup>	14.7					Subcritical

Conclusion: Critical @ 14.8 on sight glass.

Zero cor. - .1  
But " + .4

Hc 15.1  
Vc 17.2 ft ✓  
Mc 1.26 kg ✓

$\mu/x = 327$

\* Instrument Trouble

3/15/50

## EXPERIMENT # 414

15" AL. REACTOR - UNTAMPED

 $k_x \sim 350$  $k_0 \sim 7.0$ 

INSTRUMENTS &amp; SOURCE AS in #413. —

TIME	Soln Ht	#1	#2	X 1/M <sub>1</sub>	⊙ 1/M <sub>2</sub>	REMARKS -
	7.5	25.0	9.5	—	—	BACK GROUND —
2:00 pm.	14.9	44, 45	19, 19.5	.56	.489	
2:21	18.0	63	30	.397	.317	Ht Ht @ 18 cm
2:30	22.0	134	73	.182	.130	from #3 stopped @ 23.5
2:42	24.0	377	227	.066	.042	from #1
	Rod in.	220	110	.113	.085	Rod worth 9 mm.
3:25	25.0	Critical Rod @ 23 cm.				
3:30	24.95	Subcritical Rod out.				

Conclusion: Critical @ 24.95 cm in sight glass.

Solution level zero's at sight glass = +0.3 cm.  
Tampex tank empty.

st. gl. ht	24.95
zero	-.30
Bot	+ .4

$$H_c = 25.05 \text{ l}$$

$$V_c = 28.5 \text{ gal } \checkmark$$

$$M_c = 2.09 \text{ kg. } \checkmark$$

$$\frac{H}{x} = 327$$

3/24/50

Exp. 415

Fox  
Morfitt  
Cesium

Phosphate - Uranium nitrate sol'n P/X = 50 N/X = 2.8 H/X = 350  
15" stainless steel Reactor Untamped

Source at 10cm from bottom

Trip Point

#3 80 x 100  
4 —  
5 —  
6 - 6.2 x 1000  
7 - Trip

Starting scales.

#3 x 100  
#4 x 5  
5 x 1  
6 x 25  
7 —

Time  
2:00  
3:05  
3:20  
3:40  
3:58

Soln Hgt.  
12.6  
20.2  
25.3  
33.5  
40.6  
Rod in  
44.5  
44.80  
43.85

#1	#2	H/M	H/c
24.5 25.5, 26.0, 24	9.0, 1.0, 9.5	1.0	1.0
55.5	19.0	.45	.50
80	32.0	.31	.295
154	74.0	.163	.128
478	267	.053	.036
274	140	.091	.068

Critical Rod @ 30.0  
Critical Rod @ 39.0

⊗  
Remarks:  
1.5 cm from  
each  
#1 MT @ 15cm  
1 cm from #2 & #3  
#5, #7, #8  
#4 MT #9 MT  
#8 MT #78 MT  
#6 MT

1/10 cm as #2

Conclusion: Critical 43.90 cm. on sight glass.

Invariant on 15" cylinder.

#1 2 3 4 5 6 7 8 9  
6.4 6.4 6.3 6.3 6.4 6.4 6.4 8.53 DU + 1cm

Right Glass out Ht. 43.90  
Zero. H/c cor -1.10  
+ .40

Hc 43.20  
Vc 99.2  
Mc 2.72

H/X = 316.0  
P/K = 49.56  
N/K = 2.72  
sp. gr. 1.645  
g/m/cc = .0336 x 1.665  
= .05927



132

3/27/50

Ex 416

Rohr  
Fox  
Cromin

15" Stainless Steel Reaction Water tamped  
P/X n 50 M/X n 2.8 H/X n 300

Source at 10 cm ~~at~~ from bottom

Solution Inventory =	1	2	3	4	5	6	7	8	9
in 15" cyl	6.4	6.4	6.3	6.3	6.4	6.4	6.4	5.3	DU + 1cm

Time	Instruments	Stand	Trip	Co/c <sub>1</sub>	Co/c <sub>2</sub>	Notes
	#3	X 10	75 x 100			
	#4		—			
	#5	X 1	—			
	#6	X 25	6 x 1000			
	#7	—	Trip	⊙	⊕	
	<del>#1</del>	#1				
10:25	1cm					#9 MT
10:29	6cm.					#8 MT
10:45	11.6	8.02 7.75	12.1			
		7.55	15			
10:55	12.0					#3 MT
11:00	16.5	10.5	3.0	.748	.33	
11:10	<del>19.3</del>	14	3.25	.553	.31	#2 MT @ 18
11:32		32	10	.242	.10	
11:44	26.5	134	52	.0192	.058	#4 MT @ 24.5
11:50	Rod in	39	11.5	.198	.087	
12:04	27.45		Super			Rod at 20
12:16	27.1		Sub			Stopped

Conclusion crit at 27.25 ± .1 cm

Total cor.

- .50

Hc

26.758

Vc

30.49

Mc

~~1.81~~ Kg.  
1.69 ✓

H/X = 3160

P/u = 49.56

EX. 417

Crown 15" SS REACTOR TOP TAMPERS UP (@ 75cm.)  
 Flux  
 Rods

SAME INSTRUMENTS as 416

$P/k \approx 50$      $H/k \approx 300$   
 $H/k = 316$

TIME	H <sub>z</sub>	#1	#2	c/c <sub>1</sub>	c/c <sub>2</sub>
1220	27.1	41	19	.189	.0526
1227	28.5	82	38	.094	.0266
1240	30.2	Super	Rod at 23		
	30.0	Super	Rod out		
	29.9	Sub			

Feeding from #6

conclusion critical at  $29.95 \pm 0.05$  cm.

cor.  $\frac{-0.5}{29.45}$

$V_c = 33.57$

Mk  $\frac{1.99}{1.86} \text{ kg.}$

$H/k = 316$

$P/k = 99.50$

134 7/28/50

Rehearsal  
for  
Madeline  
Morfit's  
Cabin

Ex 418

1140  
954  
186

P.U. = 49.52 N:da 2.8 H/A = 316.0  
= 300

with 10<sup>6</sup> tubes filled with 5% HNO<sub>3</sub> in water by volume

15" stainless steel Reactor water tamped  
no top tamper

Inventory

	MT	MT	MT	MT	✓	MT	MT
#1	2	3	4	5	6	7	8 9
	6.4	6.4					
	12.05	12.05	12.05	12.05	12	12.05	12 10 DU+2

Drainback

Source at 20 cm  
using outside control rod

Instruments	Stentisy	Trip Pts
#3	X100	84 X100
#4	X5	—
#5	X1	—
#6	X25	6 X1000
#7	—	trips

Time	Sol. Ht	#1	#2	c/c <sub>1</sub>	c/c <sub>2</sub>
3 <sup>00</sup> PM	23.2	7.0	1.5		
		7.0	2.0		
3 <sup>15</sup> PM	30.2	9.0	2.5	.78	.80
3 <sup>30</sup> PM	45.5	13.5	4.5	.54	.45
3 <sup>45</sup> PM	60.3	16.5	8.5	.425	.235
4 <sup>15</sup> PM	67.3	14.5	8.0	.48	.25 (tubes floating previously)
4 <sup>30</sup> PM - Morfit's Cabin	59.5	14.0	7.5	.50	.27
4 <sup>45</sup> PM	45.3	11.5	4.5	.61	.45
4 <sup>00</sup> PM	29.7	8.5	3.0	.82	.67
5 <sup>00</sup> PM	23.1	7.0	2.0	1.0	1.0
		6.5	3.5		

Conclusion: Reactor appears to be safe even if filled to any height.

A sample Tr # 850158  
P = 23.14% by wt.  
NO<sub>2</sub> = 2.55%  
B. U = .03594 gm/gm sample Tr. 850159  
X = 23.20

3/29/50

Ex 419

= 49.54

McFalls  
McSudar  
Fox  
Crown

P:U u 50 N:U u 2.8  $\frac{1}{4} \times u 300 = 316$

with 9 tubes filled with  $H_3PO_4 + 5\% HNO_3$  by volume  
approx P:U of 100 (85%)

15" stainless steel Reactor no top temper

Instruments	Stand scale	Trips
#3	x100	85 x 100
4	<del>x10</del> x5	—
5	x1	—
6	x25	6.2 x 1000
7	—	—

Sources at 20 cm using outside Control Rod

MT@

Evolution	Inventary	#1	#2	#3	#4	#5	#6	#7	#8	#9
		12.05	12.05	12.05	12.05	12.05	12.05	12	10	DUT 2

60.5 #9 mesh 6.9 mesh 4.8 MT MT

Sample taken by adding to DV - approx 1 liter from each cyl and mixing.

Time	HT	#1	#2	co/c <sub>1</sub>	co/c <sub>2</sub>
2:20 PM	23.2 cm	6.0	1.5 } 1.5 } 6.0 } 6.0 } 1.25 } 1.75 } 2.0 }	1.0	1.0
2:32 PM	30.0	7.5	2.0	.80	.86
2:47	45.7	9.5, 10.5	4.75, 3.25	.63, .57	.32, .46
3:02	60.2	11.0	5.5	.545	.27
3:16	67.3	11.0	6.0	.545	.25

Conclusion: Reactor appears to be safe even if filled to any height. System if anything is less reactive than that of #48.

7 PM - Manf'd exp DV in #3; each other cylinder has 6 cm in empty 15 cm when react.

*(Handwritten flourish)*

8/29/50

Exp 420

Robt.  
Cathian  
Henry

To repeat some fails. for Robt at steady  
flux for an extended time

15" reactor, H<sub>2</sub>OAC filled tubes removed,  
untamped. same solution as in 419.

- TRIP rods # 3 - 90 x 100  
# 6 - 6.5 x 100  
# 7 - 0.5  
Rest scales # 3 x 100  
# 4 x 5  
# 5 x 1  
# 6 x 25

Source 14 cm above reactor bottom = 22.5 on scale  
using 3/4" Cd rod in platform for control.

Time	H	C <sub>1</sub>	C <sub>2</sub>	M <sup>+</sup>	M <sup>-</sup>	Notes
8:05P						Reactor filled from # 3.
10						#3 3' empty at 4.0 cm, Filling for #1.
18						#1 " " 9.7" Filling for #9.
1:35	16.7 cm	18.5 18.0	17.07			#9 empty, Filling for #8
50	23.3	30.5	17.0	0.61	[0.61 → C <sub>20</sub> = 10.3]	#8 empty, Filling for #7
9:07	29.4	38.0	44.5	0.32	0.38	#7 empty, Filling for #6
22	35.2	103	96.0	0.18	0.16 0.18	#6 empty, Filling for #5
37	41.1 41.0	274	298	0.07	0.06	#5 " " - 2
	45.2					Slightly sub-critical
	45.7					Critical with rod at 28.0
10:11	—					Foils placed with safety & control rods in and with source out — no sign of a change in levels due to tamper of personnel
10:18	—					Radiation level (neutron) brought to 60 <sup>x100</sup> on #3 meter and maintained constant. (6 x 1000 on #6)
11:20	—					Radiation at rate of 8 m/hr at end of tamper tank nearest control room
11:59	—					Control rod & safety rod in; foils removed;
12:23	—					New foils placed and reactor started toward critical
12:34	—					Radiation level (neutron) brought to 80 x 100 on #3 and maintained; #6 is off-scale on 1000. Critical with rod at 29.5 cm.
1:20	—					Critical with rod at 30.0. Level still 80 x 100 on #3
2:20	45.7					Critical with rod at 30.5. Level as above

Drain back:

Into #2	to	46.0
Into #5	to	35.5
" #6	to	29.4
" #7	to	22.8
" #8	"	16.3
" #9	"	9.7
" #1	"	3.8
" #3	"	remainder

(Cms. in 15" reactor with framing for tubes)

Installed 30 tubes of  $H_2PO_4$  in lattice -

Out.

3/34/50

Exp # 421

H/x ~ 300  
= 316

P/u ~ 50  
= 49.56

Callahan

15" Reactor side & bottom Tamping only. 36 tubes filled

Crown

no pattern as per page 108.

with H<sub>3</sub>PO<sub>4</sub> + 5% HNO<sub>3</sub>

Fox

Maxlin

Mufeta

Instruments

Start @

Trips @

3

X100

92 x 100

4

X5

4 X 100 Pyrom.

5

X1

6

X25

6 1/2 x 1000

7

Trips

Source @ 12 cm.

T<sub>1</sub> mi  
8:45

Solu Hgt.  
14.5

#1  
any 5.0

#2  
2.0 any

1/M<sub>1</sub>  
1.0

1/M<sub>2</sub>  
1.0

9 MT @ 6  
8 MT

8:55

20.0

7.5

3.0

.66

.66

from #7  
#7 MT @ 21.2

9:15

28.2

11.0

4.5

.455

.445

from #6 <sup>6 mt @ 21.2</sup>

9:25

35.0

32.0

23.0

.156

.087

from #5

9:40

Rod in

30.0

.170

stopped #5

36.5

90.0

68.0

.055

.027

started #4

Rod in

58

.086

37.4

Super Crit. Rod at 40

37.3

Critical Rod out.

37.25

Sub. Critical Rod out.

Critical at ~~37.3~~ 37.3 ± 0.1 cm

zero in reactor gives + 1.1 cm on S.G. (Tamp tanks drained)

Drainbocks  
15" cm

1 2 3 4 5 6 7 8 9  
6.4 6.4 6.4 6.4 6.4 6.4 6.4 DU + 8 cm

Sight Glass crit Ht. 37.30  
Bot. + zero cor ~~total cor~~ - .50  
Bot. Plate cor ~~the~~ ~~36.80~~ - .99

99 37.30  
.50 - 1.44  
1.44 35.86

H<sub>c</sub> = 35.86

V<sub>c</sub> = 34.26

M<sub>c</sub> 2.03 Kg.  
1.89  
1.90

Area of tubes  
5066 x 36 = 182.37 cm<sup>2</sup>  
rods 2.14  
184.51

1190.0  
189.5  
955.5

4/3/50

Epp 422

H/A ~ 300  
= 316

P/U = 50139  
= 49.56

For  
Crown  
Machine

12" Stainless Reactor complete water reflector

Source at 12cm

Instrument	Start	Trip
3	x100	92 x100
4	x5	—
5	x1	—
6	x25	6 1/2 x1000
7	—	Trips

Sol's Inventory	#1	#2	#3	#4	#5	#6	#7	#8	#9
	10cm	10cm	10cm	10cm	10cm	10cm	10cm	18cm	DV
			○	○	○	○	○	○	○

Time	Sol's Ht	#1	#2	1/M1	1/M2	Notes
10:33	12.3 (28.3x)	5.5	1.0	1.0	1.0	3x Blown Back from 13.1
10:46	16.1					7 MT @ 16.1
10:50	22.3 (8.8)	9.5	2.0	0.58	0.50	small rises on #6 (25x)
11:02	26.2					#6 cyl empty
11:10	29.2 (29.3)	12.5	3.0	.44	0.33	#6 in at 50x
11:22	36.3					#5 MT #6 @ 100x
11:25	39.0 (38.9)	32.5	12.5	.17	.08	good rises #6 @ 200x
11:37	42.0	97.5	41.5	.056	.024	#6 @ 500x
11:44	42.0 (rod in)	45.0		.12		rod worth 1.7 cm
11:45	42.0 (rod in Temp rod)	30.0		.18		rod + temp worth 3.3 cm
11:48	43.5 (43.6)					feed from #3
11:54	43.8 (43.9)					

Very slightly subcritical (Rod out)  
Super in Rod > 36 cm from bottom

12" SS Reactor is at 0 when sight glass reads 1.0 cm (no H<sub>2</sub>O tank)  
Critical @ 43.65 ± 0.15 on Sight glass

Drain back approx as before

zero in cylinder reads 1 cm on sight-glass - no water in temp tank etc etc

-8 Bot gno  
+6.5  
-1.5

right sl. 43.45  
Total 43.50  
Hc = 43.50  
Vc = 31.74  
Mc = 1.75 ✓

H/A = 316.0  
P/U = 49.56



4/9/50

Epp 423

Fox

10" Al  $\frac{1}{4}$ " 300 P:U u 50 N:U u 2.8

Machlin  
Crown

completely water tamped

Analysis data:

Source at 20 cm

$\frac{H}{X} = 316.0$

$\frac{P}{U} = 49.56$

$\frac{N}{U} = 2.71$

Instrument	Start	Time
#3	x100	92 x 100
#4	x5	—
#5	x1	—
#6	x25	6.4 x 1000
#7	—	2"
#8	—	—

Solution  
Inventory

1	2	3	4	5	6	7	8	9
13.7	13.7	13.7	13.7	13.7	13.7	13.7	11.5	DV + 1 cm
			(MT)	(MT)	(MT)	(MT)	(MT)	(MT)

Time

Soln #	#1	#2	$\frac{1}{M_1}$	$\frac{1}{M_2}$	
9:10 DV	3.0	1.5			#9 MT
2	3.5 (2.5)	1.0 (1.5)			#8 MT at 12 cm
9:23 AM 22.5	4.0	1.5			from #7
9:40 AM 41.2	6.5	3.5	.54	.43	7 MT at 26.5
9:55 AM 55.3	8.0	7.0	.44	.21	#6 MT 41.2
10:05 AM 65.3	10.0	8.0	.35	.178	#5 MT 48.5
73.3	12.0	10.5	.28	.143	#4 MT 65.3

System sub-critical at 73.3 (maximum lid in cyl)  
 $\frac{1}{M}$  extrapolates to 105 cm as critical.

#1 counter = 105 cm

#2 counter = 104 cm

$1.035$   
 $+ .93$   
 $+ .1$

zero in cylinder is -0.1 cm on sight glass.

$H_c \sim 109.5$

$V_c \sim 52.9$

$M_c \sim \frac{3.44 \text{ kg}}{2.93}$

Sample from 830.169 8168

$\rightarrow U = .03553$

$ND_3 = 2.54 \% \approx .5736$

$P = 23.26\%$

Sample from cyl. F during inventory & shipping

$\frac{H}{X} = 316.0$

$\frac{P}{U} = 49.56$

4/11/50

Exp 424

Fox  
Machlin  
Crown

10" A1  $\frac{H}{K} = 80$  P:U = 7 N:U = 2.8  
contaminated (for wiping purposes)

Source at 7 cm

Instrument	Steps	Trip
#3	7100	92x100
4	x 5	—
5	x 1	—
6	x 25	7x1000
7	—	1"

Sal'n Inventory	(A)	(B)	(C)	(D)
	2	4	6	8
	348g	420g	142g	1531g
	4.8 cm	4.8 cm	9.2 cm	4.2 cm

10:10  
11:00  
11:30

Emptying #9  
#9 MTS  
#7 feeding  
valve on #2 position leaked. replaced with new valve

12:08  
12:15

#8	#1	#2	$\frac{1}{M_1}$	$\frac{1}{M_2}$
10.2 (3x blackback from 9:17)	32.0	11.0		

#7 stopped flow - added small amt H<sub>2</sub>O to clear line

1:15

23.4	48	20.5	.66	.54
------	----	------	-----	-----

2:05

#7+9 added more water to rinse out possibly clogged line after continued bleedback.  
28.6      54.5      24.5      .59      .45

$\frac{1}{M}$  curve extrapolated gives critical values: #1 = 61.0 cm } avg = 56.8 cm  
#2 = 52.5 cm }  $\pm 5$  cm

avg Sp. #1 = 150  
from first shipment

Hc  $\sim 56.8 \pm 5.0$   
Vc  $\sim 28.8$  liters  
M<sub>c</sub>  $\sim \frac{3.78}{3.24}$  kg

10.65% NO<sub>3</sub> - 830184  
15.69% P  
.0805 cm<sup>3</sup>/gm

$\frac{H}{X} = 156.7$   
 $\frac{N}{U} = 5.01$   
 $\frac{P}{U} = 14.77$

142 4/11/50

machlin

### Exp 425 A

Top 10" Al cyl  $H/K \approx 80-100$  P:U  $\approx 7$   $H/K = 156.07$

Crown Completely water tamped.  $P/U = 14.77$

Source at 7 cm  $M/U = 5.01$   
Instruments same as Exp 424

Background with T. Tamped up.	#1	#2
	5.5	3.0
	5.0	3.0

Time	Sol'n Ht	#1	#2	$1/M$	$1/M_2$	
2:30	10.0 cm	6.0	1.75			
2:35	19.7	13.5	5.0	.44	.24	
2:45	23.1	26.0	11.5	.23	.10	
		18.0	8.5	.33	.14	Top Tamped up 5cm
3:00	25.2	277.5	138.5	.021	.0085	
		44.0	20.0	.136	.06	Top Tamped up 5cm
		17.5				Control Rod in + tamped up.

3:05 25.5 Critical with Rod at 26 cm

Bot cor.	+ .95
zero.	+ .3
	<hr/>
	1.25

Critical at 25.35  $\pm 0.15$  cm on sight glass  
 $H_c = \frac{25.35 + 1.25}{26.60} \quad V_c = 13.47 \quad M_c = 1.52 V$

### Exp ~~425 A~~ 425 B

Time	Sol'n Ht	#1	#2	$1/M$	$1/M_2$	
3:15	26.9	47.5	26.5	.105	.11	Top. Removed
3:25	28.1	159.5	94.5	.031	.031	
3:32	22.7	15.0	7.5	.33	.40	

extrapolated to crit height 28.6 cm on sight glass  
 $H_c = \frac{27.85 + 1.25}{29.1} \quad V_c = 14.10$   
 Drainbocks  
 #2 10 cm    #5 10 cm    #7 8 cm    #9 D.V.     $M_c = 1.59 V$

St. Glen reads -1 mm at reactor zero

4/12/50

Expt 426 A

From  
Rohrer  
Fox

15" SS, cyl ~~80-120?~~ ~~filled with water~~ ~~tamped~~ ~~untamped~~ source at 5cm

Trap points: #7-2" ; #3-88 ; #6-6  
 Starting values: #5-1 ; #3-100 ; #6-25 ; #4-10

Background with  
 2nd Ht 9.0 approx tamped up

#1	22.5	#2	10.0
	20.5 (22.0)		10.5 (10.0)
	22.0		10.0

9, 8, 7 & 6 Empty - also 5 & 2

3:37	(col. H) 13.0	$C_1$ 31.0	$C_2$ 19.5	$C_4$ .71	$C_6$ .69	4 empty
		15.7	43.0	21.5	.51	4.6
3:57		17.7	57.0	32.5	.38	.31

426B

From  
Gross  
Cachin

Prior to above exp (426A) it was necessary to add water in order to put solids back into solution. Some mixing was done above after drain back air was bubbled through cylinder - this experiment will homogenize the sl & estimate untamped critical mass.

4:40P	H = 8.0cm = 8.8	$C_0 = 22.0$	#1 22.0	#2 10.0	$M^{-1}$ #1 #2	#2, 3, 4 empty #7 empty #5 empty #9 -
50	= 14.9 after blow back	36.5	16.5	0.61	0.61	
59	= 19.4	58.0	32.5	0.38	0.31	
	= 19.4	47.0	23.0	0.47	0.44	

Extrapolated critical height < 27.5 cm  
 724. ~ 255

Inventory -

#2 - 5cm in 15" meter  
 #5 - 5 - - - -

Sp. Gr. 1.52

Sightglass - 0.9 cm  
 24.6  
 bottom 7.41  
 Hc m 25.0 cm  
 Vc 28.5 liters  
 Mc 3.1 kg ✓

$H/\lambda = 180$

$P/w = 11.58 ; N/w = 5.13$   
 $N/H = 5.50$

144

4/12/50

Use 2

#427 A.

Fox  
CRONIN  
CALLIHAN

15" Stainless Reactor Tamped.

~~15" 150~~ Pt 10 = 87.

Dist. sh as in 426 - (Hot Warm water in (temp).)

		#1	#2		
Background:		6.0	1.5		
		6.0	1.5		
5:35P	H = 9.0 cm.	6.0	1.5	$\epsilon$	$m^2$
38	= 14.4	18.5	6.0	0.32	0.25
50	= 15.6	34.0	13.0	0.18	0.12
55	= 16.5	102	45	0.06	0.03
	= 17.0				
					Critical with red almost out in.
6:05	= 16.8				Subcritical red out.

#5 empty

CRITICAL WITH SIGHT GLASS = 16.9.

16.9	16.9
- 9	- 49
16.0	Hc 15.41
+ 1.41	Vc 17.56
16.4	Mc 1.89 ✓

427 B.

Removed top tamped -

6:07	H = 16.8	22	8	0.27	0.19
14	= 18.0	34	15	0.18	0.10
26	= 19.2	273	132	0.02	0.01

Out of solution

Extrapolated Critical Height - sight glass = 19.35 cm - (good extrapolation).

Inventory:	#	cm in 15" reactor.	sight glass
	2	6	19.35
	5	6	- .90
	7	6	18.45
	9	1	+ .41
			bottom
			Hc 18.86 9
			Vc 21.5 ✓
			Mc 2.31 ✓

Zero in 15" cyl reads 0.9 cm on sight glass.

DAC + JK7

Sample taken ~~4/13/50~~ 4/13/50 from manifold.

.0812 gm U/gm

830185

.0812 gm U/gm

Sp g (Calc) 1.42 g/cc  
g U/gm/cc .1075 =

NO<sub>3</sub> - 10.97%

P - 12.42%

4/13/50

Exp 428

Crown  
Top  
Modelin

15" Stainless Reactor with 10 tubes with 5% HNO<sub>3</sub> (250 cc per tube)

H/X 150 P/U " 7 N/U 22 6

Source at 9cm

Warm water in ampers 20-23°C

Instruments:	Trips	Start
3	92x100	x100
4	-	x10
5	-	x1
6	6.5x1000	x25
7	1" trip	+

Sol' & Density

	2	5	7	9
	11.4 cm	11.4	11.4	du + 1.9 cm

Time

Time	Sol' & Rod	#1	#2	1/M <sub>1</sub>	1/M <sub>2</sub>
12:20	8.9	6.0	1.5		
12:30	19.6	14.0	5.0	.43	.30
12:45	22.7	31.5	12.5	.19	.12
12:52	24.2	48.0	22.0	.125	.068
		68.0	32.0	.088	.047
1:00	25.5	Rod 21 cm out		Critical	
	25.3	Rod 40 cm out		Critical	
	25.2	Sub Critical			

stopped #5  
Control Rod in

Critical at 25.25 ± 0.5 cm  
sight glass - .90 zero L.H.

Cor. - .94 bot Plate  
+ 70 botton pipe

corr.	24.35
H <sub>c</sub>	- .24
V <sub>c</sub>	24.1
M <sub>c</sub>	14.6
	1.88 kg
	1.77

H<sub>1</sub> / H<sub>2</sub> =  
X  
H<sub>1</sub> / H<sub>2</sub> of sol'n only = 126

P/U = 14.74

N/U<sup>235</sup> = 6.97

4/13/50

Exp. 429

Corium

15" Stainless Reactor

Top  
Machine

Untamped with 106 tubes with  $5\% \text{H}_2\text{O}_3$   
same as Ex 428 other wise

$C_0 = 20$

$C_0 = 10$

Time	Sol'n H/H	#1	#2	$1/m_1$	$1/m_2$
1:25	25.5	108	57	.18	.17
1:40	27.4	130	72.5	.15	.138
1:50	30.3	195	121	.10	.08
2:00	32.5	303	204	.067	.05
2:05	34.3	sub critical rod out			
2:10	36.8	Critical Rod at 28.0			
	<del>36.50</del> 36.50	just critical rod out			

2:15

Critical at  $36.50 \pm 0.1 \text{ cm}$

$P/\mu = 14.74$

Drainback

$$\begin{array}{r} -1.90 \\ 35.40 \\ -0.24 \\ \hline \end{array}$$

$N/\mu^{2.35} = 6.97$

$H_c = 35.40 \text{ V}$

Sol'n  $H/H = 127.6$

$V_c = 21.3$

$MC = 2.58 \text{ kg } \checkmark$

4/13/50

Exp 430

Oronin  
Muddlin  
Fox

15" Stainless Reactor with 1/3 lattice with 5% HNO<sub>3</sub> in tube  
Tamped spaced for top

$\frac{H}{L} = 127.6$   
 $\frac{H}{U} = 14.74$   
 $\frac{H}{u_{235}} = 6.97$

Time	Sol'n H <sub>2</sub> O	C <sub>0</sub> = 7.5		C <sub>0</sub> = 3.5		1/m	1/m <sub>2</sub>	20.78
		#1	#2	#1	#2			
3:30	9.4							1.14
3:25	16.4	14.0	7.5	.53	.46		H <sub>c</sub> - 19.64	
3:45	20.2	95.5	50.5	.08	.07		V <sub>c</sub> - 18.8	
3:50	21.0	Critical Rod at 11.5						M <sub>c</sub> - 2.28 Kg
3:52	20.8	Critical Rod out (slightly super)						
	20.75	Sub critical rod out						

critical at 20.775 ± 0.05 cm

Exp 431

Same as above untamped

Time	Sol'n H <sub>2</sub> O	C <sub>0</sub> = 27		C <sub>0</sub> = 18		1/m	1/m <sub>2</sub>
		#1	#2	#1	#2		
3:55	20.9	100.5	55.5	.27	.32		
4:05	23.3	155.5	94.0	.174	.19		
4:10	16.4	55	25	.49	.72		

extrapolates to 26-28 cm away = 27.0 cm ± 1 cm

Drainbacks

2 5 7 9  
7cm 7cm 7cm DV + 2.4 cm (including SG zero & bottom plate error)

$$\begin{array}{r} 27.0 \\ - 1.14 \\ \hline H_c = 26.9 \\ V_c = 25.70 \\ M_c = 3.34 \end{array}$$

$26.9 = H_c$   
 $24.7$

$3.0$  HKF later



Untamped

4/14/50

Exp 432

Cronin

15" Stainless Reactor with  $\frac{1}{3}$  lattice with  $H_2PO_4$  in

Fox  
Rohrer

tubes (250 cc. per tube)  
~~Fumped except for top.~~  
Untamped.

Source at  $\frac{1}{4}$  cm.

$\frac{H}{X}$  of sol'n = ~~15.764~~  
24.21  
131.2  
 $\frac{P}{u}$  of sol'n = 14.74  
 $\frac{N}{u}$  of sol'n = ~~6.50~~  
 $\frac{N}{X}$  of sol'n = 6.97

Instruments:	trip	start
3	90x100	x100
4	—	x10
5	—	x1
6	6.5x1000	x25
7	2"	—

Solution Inventory

	2	5	7	9
	7 cm	7 cm	7 cm	DV + 2.4 cm

Time	Sol. Ht	#1	#2	$\frac{0}{M}$	$\frac{x}{M}$	Remarks
1021	9.5 cm	24.5 26.0) <sup>25</sup>	14.5 (14.0) 13.5			7 empty feed from 7
1024	9.7 cm					7 empty
1030	16.1	48.5	21.0	.51	.66	
1035	16.9					5 empty
1040	21.2	86.0	42.5	.29	.33	
1050	23.9	128.5	74.0	.19	.19	2 empty

Critical ht. extrapolated to be between 27.3 & 28.7 cm.  
Approx. avg. 28.0 cm.  $\pm$  0.7 cm.

Drain back:

	2	5	7	9
	23.9	16.9		
	16.9	9.5	empty	empty
	7 cm.	7.4 cm		

28.0  
1.14  
Hc 26.86 ✓  
Vc 25.6 ✓  
Mc 30.7

Exp 428  
429  
430  
431

Analysis. Complete.  
colorimet. .0884 gm/gm 830187  
precision .08535 gm/gm 830186  
.08535

4/14/50

Exp 433

Cronin  
Fox  
Rohrer

15" Stainless Reactor with  $\frac{1}{3}$  lattice with  $H_2PO_4 + 5\% HNO_3$  in tubes  
(250 cc. per tube)  
Tamped

Time	Sol Ht.	#1	#2	$\frac{1}{M_1}$	$\frac{1}{M_2}$
1105	9.5	7.5 } 7.0 } 7.0	2.5 } 2.5 } 2.5		
1115	16.9	13.5	5.0	.52	.5
1122	20.3	36.5	17.0	.192	.147
1129	21.1	64.0	30.0	.109	.083

Remarks  
- Bkg. & empty

empty

22.0 Critical with rod @  $\approx 20$  cm.  
21.9 Sub-critical rod out.

Critical  $21.95 \pm .05$  cm.

1145

Drainback:

#2	5	4	9
23.9	16.5	9.6	
<u>16.5</u>	<u>9.6</u>	<u>~2.0</u>	D.V. + $\approx 20$ cm.
7.4 cm.	6.9 cm	7.6 cm	

$21.95$   
1.14  
HC - 20.8+  
VC - 19.87 ✓  
MC - 2.38 ✓

4/14/50

Exp 434

Crosin

15" Stainless Reactor with 106 tubes with

Fox

$H_2PO_4 + 5\% HNO_3$  in tubes  
(250 cc. per tube)

Henry  
Rohrer

Tamped.  
Instruments as in Exp 432  
Source

Sol. Lev.

#2    #5    #7    #9  
7.4 cm    6.9 cm    7.6 cm    DV + 20 cm.

Lucia  
1257

Sol. Ht.	#1	#2	$\frac{1}{m_1}$	$\frac{1}{m_2}$
10.6 (blk)	6.0 } 6.0	2.5 } 2.5		
	6.0 }	2.5 }		

Remarks  
9 empty

1313

15.0 cm    —    —    —    —

7 empty

1318

20.5    11.0    9.0    .545    .625

1322

25.1    23.0    8.5    .261    .294

1325

26.0    —    —    —    —

5 empty

1334

28.1    53.0    24.0    .113    .104

50    20    .12    .125 } rod worth  
40    .15    .15 } v/cm.

29.9 Sub-critical rod out  
30.2 Critical with rod @ 26 cm.

1338

30.1 Sub-critical rod out.

Critical height on sight glass at  $30.15 \pm .05$  cm.

— 1.14  
Hc - 29.07  
Vc - 17.43  
Mc - 2.07

4/14/50

Exp 435

Cronin  
Fox  
Henry  
Rohrer

15" Stainless Reactor 10.6 tubes with  $H_2 PO_4 + 5\% HNO_3$   
in tubes (250 cc per tube)

Untamped

Other wise same as 434

Qty as on Exp 432 #1 25 #2 14 @ 9.5 cm.

Time	Sol. Wt.	#1	#2	$\frac{1}{M_1}$	$\frac{1}{M_2}$	Remarks
30.2		93.0	50.0	.27	.28	
33.1		112.0	63.0	.223	.222	
36.						
37.1		151.0	94.5	.165	.148	

Critical extrapolated to be between 45.5 & 48.2 cm.

Avg = 46.8 ± 1.3 cm.

Drain Back -

#2	#5	#7	#9
37.1	26.0	14.5	
26.0	14.5	3.5	
11.1 cm	11.5 cm	11.0 cm	3.5 cm + D.V.

46.8  
1.14  
H<sub>c</sub> = 45.66  
V<sub>c</sub> = 27.39  
M<sub>c</sub> = 3.29 ✓

1140  
539  
601 net area

H/x = 144

# Check List

## Instruments

### 1. Personell

- dosimeters and film badges
- survey meter in control Rm.
- Process Monitor checked
- Catastrophe badge

### 2. Reactor System.

- Trip points recorded
- Starting scales recorded
- Instruments respond to source
- Source in Operating position
- All SOURCES Accounted for
- Exp. No's on charts
- Attic Fan

## Reactor

- Water in Tamper tank
- Top Tamper
- Smooth Action Tamper Limit Switches Set.
- Safety Rod Set
- Control Rod zeroed
- Dump Valve Set
- Dump Pan taped up.
- Check all Pulleys and wires

## Solution

- Solution Inventory in Reactor Ht.
- All valves inc. Dump Valve
- Pins in Cyl Valves
- Air Pressure
- Light on Feed Line
- Set Dump Spring

## Final Check

- Key to Rear Gate, Rear Gate Open.
- Notify Guards, Check Personnel Red Light.
- Check for Leaks

	317	318	319	320	320A	321	322 A	322 B	323	324	325	327	328	329	330	331	332	333
JF JM	DC	HH	HH	FC	FC	FC	JF	FC	FC	HH	✓	JF	JF	L	L	FC	FC	FC
JF JM	FC	HH	FC	JF	DC	HH	✓	FC	FC	✓	RM	✓	L	L	FC	FC	FC	FC
RM JF	FC	HH	RM	DC	FC	FC	JF	JF	✓	FC	✓	RM	FC	L	L	FC	RM	RM
FC JM	DC	HH	JF	JF	FC	DC	JM	JM	JF	FC	✓	FC	FC	L	L	FC	FC	FC
FC FC	FC	HH	FC	FC	DC	DC	JM	DC	HH	✓	FC	JM	L	L	FC	FC	FC	FC
FC FC	FC	HH	FC	FC	DC	DC	JM	DC	HH	✓	FC	JM	L	L	FC	FC	FC	FC
RM JM	FC	FC	RM	DC	FC	FC	JF	✓	FC	✓	RM	FC	L	L	FC	FC	FC	FC
JF JM	FC	FC	FC	FC	FC	FC	JF	JM	FC	✓	✓	RM	FC	L	L	FC	FC	FC
DM JM	FC	FC	RM	DC	RM	HH	JF	✓	FC	✓	RM	FC	L	L	FC	FC	FC	FC
JF JM	JM	FC	FC	FC	FC	HH	FC	✓	FC	✓	FC	JF	L	L	FC	FC	FC	FC
- FC	JF	FC	RM	JF	FC	HH	-	-	JF	✓	✓	FC	FC	L	L	JF	RM	RM
- JF	FC	FC	JF	JF	FC	FC	-	-	FC	✓	✓	FC	FC	L	L	JF	FC	FC
- JM	FC	FC	FC	JF	FC	FC	-	-	✓	✓	✓	FC	FC	L	L	JF	FC	FC
JF JM	FC	FC	FC	JM	FC	HH	JM	JF	JF	✓	RM	FC	L	L	JF	FC	FC	FC
JF JM	FC	FC	JF	JM	FC	FC	JM	FC	JF	✓	RM	JF	L	L	JF	FC	FC	FC
JF FC	FC	FC	FC	FC	FC	FC	FC	✓	✓	✓	JF	JF	L	L	JF	FC	FC	FC
JF JF	JF	FC	JF	FC	FC	✓	JF	✓	✓	✓	JF	✓	L	L	JF	FC	FC	FC
JF JF	JF	JF	JF	JF	FC	✓	JM	JF	✓	✓	JF	FC	L	L	JF	FC	FC	FC
FC JM	JM	FC	FC	FC	FC	✓	JM	✓	✓	✓	FC	FC	L	L	FC	FC	FC	FC
JF FC	FC	FC	FC	JF	FC	FC	JF	✓	✓	✓	FC	✓	✓	JF	L	L	JF	FC
FC FC	FC	FC	FC	JF	FC	FC	JM	JF	FC	✓	✓	JM	L	L	JF	FC	FC	FC
FC JM	FC	FC	FC	JM	FC	FC	JF	JF	✓	✓	FC	JF	L	L	JF	FC	FC	FC
JF JM	JF	FC	FC	JM	FC	FC	JF	JM	✓	✓	JF	JF	L	L	JF	FC	FC	FC
JF FC	FC	FC	FC	FC	FC	FC	FC	FC	FC	FC	FC	JF	FC	L	L	JF	FC	FC
JF FC	DC	FC	RM	FC	RM	FC	FC	✓	✓	✓	JF	JF	L	L	FC	FC	FC	FC
JF FC	FC	JF	FC	DC	RM	DC	JF	✓	✓	✓	JF	JM	L	L	FC	FC	FC	FC
JF JF	FC	JF	JF	FC	FC	FC	FC	✓	✓	✓	JF	JF	L	L	FC	FC	FC	FC

33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92

FC FL JM FC	FC JFL JM JM ✓	✓ HH JM JM JM ✓	JML ✓ HH ✓ ✓	JML ✓ FC ✓ JM ✓	FC FC JM FC FC	FC FC JM
FC DL JM FC	JM JM JM JM ✓	✓ HH JM JM JM ✓	JML ✓ HH ✓ ✓	JM ✓ JML ✓ JM ✓	JM JM JM FC FC JM JM JM	
RM RM FC OF	JF JF JF JM ✓	✓ HF FC FC FC ✓	JML ✓ RM ✓ ✓	JML ✓ JML ✓ FC ✓	JM JML FC FC JM ✓	JF JF JF
FC DL JM JM	JM JM JM JM ✓	✓ JM FC FC JM ✓	JM ✓ JM ✓ ✓	JM ✓ JM ✓ JM ✓	JM JM JM RM JM ✓	JM JM JM

RM - JM JF JF	JFL No - No 2nd -	→ JFL FC JML ✓
R - JM FC JF	JF No - No 20 -	JM FC JML ✓
FC - JM FC JF	FC - No 20 -	JM JM JML ✓
FL FC JM JM JF	JM JM JM FC JF ✓	JF FC FC JML ✓
FL RM JM JM JF	FC JM JM FC ✓	✓ HH JM FC JM ✓
FL FC JM JF JF	JM JM JF JF ✓	✓ JF FC JML ✓
FL FC FC ✓ JF	JF JM JF JF ✓	✓ JF FC JML ✓
FL FC JM JF JF	JM JF JF JF ✓	✓ JF JM FC JML ✓

FC FC JM - FC	JF ✓ JF JM ✓
HH ✓ RM - JM	JF JM ✓
JML ✓ RM - JM	JM JF ✓
HH ✓ JM ✓ JML ✓	FC JM JM FC JM ✓
JM ✓ JM ✓ JML ✓	JM JM JM FC JM ✓
✓ ✓ ✓ JM ✓ FC ✓	JM JM JM JF JM ✓
✓ ✓ ✓ JM ✓ ✓	JF JM ✓ JM ✓
JM ✓ ✓ JML ✓ JML ✓	HH ✓ RM JM JM FC JM ✓

FC ✓ JM FC	JM JM JM JM ✓	✓ JF FC JM JM ✓	JM ✓ ✓ ✓ JM ✓	✓ FC JM JM	✓ JM JM
FC RM JM JM JM	JM JM JM JF JM ✓	✓ JF JM JM JM ✓	JM ✓ ✓ JM ✓	FC ✓ JM ✓	JM JM JM JM JM ✓
RM FC FC JM JM	JF JF JM JM ✓	✓ HH JM JM FC ✓	JML ✓	JM ✓ JM ✓	FC JM JM JM JM ✓
RM FC JM FC JM	JF JF JF JM ✓	✓ HF FC JM JM ✓	JM ✓	JM ✓ JM ✓	JM JM JM JM JM ✓
RM JM JM JM JM	JF JM JM JF ✓	✓ JF JM JM JM ✓	JML ✓	JM ✓ JM ✓	JM JM JM JM JM ✓
FC JM FC	JM JM JF JM JM ✓	JF JM JM FC ✓	JML ✓	JM ✓ JM ✓	HH ✓ RM JM JM ✓

RM FC FC	FC JM JM JF ✓	✓ FC FC FC JM ✓	FC ✓	JM ✓ ✓ JML ✓ JM ✓	FC ✓ RM JM JM FC FC ✓	FC JM FC
FC FC JF	JM JF JF FC ✓	✓ FC JM JM FC ✓	JML ✓	JM ✓ ✓ FC ✓	FC ✓ JM ✓	FC JM FC
FC JM	JF JF JF ✓	✓ JF JM JM JM ✓	JM ✓	JM ✓ JML ✓	FC ✓ JM JM JM	JF JM ✓ JM JM JF

393 394 395 396 397 398 399 400 401 402 403 404 405 406 408 409 410 411

413 414 415 416 418 419 421 422 423 424 425 426 428 432 434

✓ JF RA RA ✓ JM	✓ JM JM ✓ JA ✓ JM J.F.N.H.RM. FC	JF ✓ ✓ FC JM JFC DC JFC JF RM FC ✓ RM ✓ ✓
✓ JM JM JA ✓ JM	✓ JM ✓ AR ✓ H.H.C.S. JM JM JM	JM ✓ ✓ FC FC DC JM JF FC FC ✓ ✓ JF ✓ ✓
✓ FC JM RA ✓ JF	✓ JF ✓ JF ✓ RM C.S. RM JM RM	JM ✓ ✓ JF FC DC JM FC FC RM ✓ ✓ FC ✓ ✓
✓ JM JA JA ✓ JM	✓ JM ✓ JF ✓ JM JM N.H. JM FC	JM ✓ ✓ FC FC DC FC JF JF FC ✓ FC ✓ ✓
✓ JM JM JA ✓ JM	✓ JM ✓ JM ✓ JM ✓ H.H.C.	JM ✓ ✓ FC RA FC DC JM FC FC FC ✓ JF FC ✓ ✓
✓ FC JM JA ✓ JM	✓ JM ✓ JM ✓ JM JM DC	JM ✓ ✓ FC RA FC DC JM FC FC FC ✓ JF FC ✓ ✓
✓ FC JM RA ✓ JF	✓ JF ✓ JF ✓ RM C.S. JM RA RM	JM ✓ ✓ FC RA FC DC JM FC FC RM ✓ ✓ FC ✓ ✓
✓ FC JM RA ✓ JA	✓ JF ✓ JM ✓ JM ✓ JF JM	JM ✓ ✓ JF RA FC DC FC FC RM FC ✓ ✓ FC ✓ ✓
✓ FC JM RA ✓ JF	✓ JF ✓ JF ✓ RM ✓ RM RM FC	JM ✓ ✓ JF FC JF DC JM FC FC RM ✓ ✓ FC ✓ ✓
✓ JF JM ✓ JF	✓ JM ✓ JM ✓ JM JM JF RM. FC	JM ✓ ✓ FC ✓ JM DC JM JF FC FC ✓ ✓ ✓ ✓
✓ on -	✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓	✓ ✓ ✓ FC ✓ - - FC FC FC ✓ ✓ ✓ ✓

✓ JF H.H. JF ✓ JF	✓ JM ✓ JF - N.H. ✓ JF - JF	JM - - RR RR JM - - FC FC - JF JF ✓ ✓
✓ - - - -	✓ - - - JF - JM ✓ JF - RM	JM - - FC FC - - - JF JF - JF ✓ ✓
✓ - - - -	✓ - - - JF - ✓ JM - RM	JF - - FC ✓ - - - FC JF - ✓ ✓ ✓
✓ FC RA ✓ JA	✓ JF ✓ RM - JM ✓ JM JM JF	JM ✓ ✓ FC FC JM DC FC JF RM FC ✓ ✓ FC ✓ ✓
✓ JF RA ✓ JF	✓ JM ✓ ✓ JM ✓ JF JM JM	JF ✓ ✓ FC JF JM DC JM FC FC FC ✓ ✓ ✓ ✓
✓ JF JM ✓ JF	✓ JM ✓ ✓ JM ✓ JF - -	JF ✓ ✓ ✓ JM ✓ ✓ ✓ JF ✓ ✓ ✓ ✓ ✓ ✓
✓ JF ✓ ✓ ✓	✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓	JM ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ JF ✓ ✓ ✓ ✓ ✓ ✓
✓ JF JM ✓ JF	✓ JM ✓ JM ✓ JM ✓ JF JM JF	JM ✓ ✓ FC JM ✓ - FC JF ✓ JF ✓ ✓ ✓ ✓

✓ DE RA ✓ JM	✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓	JM ✓ ✓ FC FC FC DC ✓ FC FC - FC FC FC ✓ ✓
✓ JF JF ✓ JF	✓ JF ✓ ✓ JM ✓ JF - JF	JM ✓ ✓ JF FC ✓ DC JM JF FC RM ✓ ✓ FC ✓ ✓
✓ JM JF RM ✓ JF	✓ JF ✓ RM ✓ RM ✓ JM -	JF ✓ ✓ JF FC ✓ DC RM JF FC JF ✓ ✓ ME FC ✓ ✓
✓ JF JF JM ✓ JF	✓ JM ✓ JF ✓ RM ✓ JF - RM	JM ✓ ✓ FC FC ✓ DC FC FC FC FC ✓ ✓ ME FC ✓ ✓
✓ JF JF JM ✓ JF	✓ JF ✓ JF ✓ JM ✓ JM - JF	JF ✓ ✓ JF FC ✓ DC FC FC RM JF ✓ ✓ JF JF ✓ ✓
✓ JF JM ✓ JA	✓ JM ✓ JM ✓ N.H. ✓ JF - JF	JM ✓ ✓ FC JM ✓ ✓ ✓ FC FC ✓ ✓ ✓ ✓

✓ JF JM JM ✓ JM	✓ JM ✓ JM ✓ RM ✓ RM FC	JM ✓ ✓ JF FC ✓ JM DC JM FC RM FC ✓ ✓ FC RM ✓ ✓
✓ JM JM JM ✓ JM	✓ JM ✓ JM ✓ JM ✓ RM FC	JM ✓ ✓ FC FC ✓ JM RM FC FC ✓ ✓ FC ✓ ✓
✓ JF JM ✓ JF	✓ JF ✓ JF ✓ RM ✓ JM -	JF ✓ ✓ JF JF JM DC JM JF FC JF ✓ ✓ ✓ ✓

Mr. Raymond  
4-7019

SECRET

3-S AL.

1.500" O.D.

.035" wall

.049

.058



SECRET